

National Flood Insurance Program

Elevation Certificate

and Instructions

2023 EDITION



FEMA

ELEVATION CERTIFICATE AND INSTRUCTIONS

PAPERWORK REDUCTION ACT NOTICE

Public reporting burden for this data collection is estimated to average 3.75 hours per response. The burden estimate includes the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and submitting this form. You are not required to respond to this collection of information unless a valid OMB control number is displayed on this form. Send comments regarding the accuracy of the burden estimate and any suggestions for reducing the burden to: Information Collections Management, Department of Homeland Security, Federal Emergency Management Agency, 500 C Street SW, Washington, DC 20742, Paperwork Reduction Project (1660-0008). **NOTE: Do not send your completed form to this address.**

PRIVACY ACT STATEMENT

Authority: Title 44 CFR § 61.7 and 61.8.

Principal Purpose(s): This information is being collected for the primary purpose of documenting compliance with National Flood Insurance Program (NFIP) floodplain management ordinances for new or substantially improved structures in designated Special Flood Hazard Areas. This form may also be used as an optional tool for a Letter of Map Amendment (LOMA), Conditional LOMA (CLOMA), Letter of Map Revision Based on Fill (LOMR-F), or Conditional LOMR-F (CLOMR-F), or for flood insurance rating purposes in any flood zone.

Routine Use(s): The information on this form may be disclosed as generally permitted under 5 U.S.C. § 552a(b) of the Privacy Act of 1974, as amended. This includes using this information as necessary and authorized by the routine uses published in DHS/ FEMA-003 – *National Flood Insurance Program Files System of Records Notice 79 Fed. Reg. 28747 (May 19, 2014)* and upon written request, written consent, by agreement, or as required by law.

Disclosure: The disclosure of information on this form is voluntary; however, failure to provide the information requested may impact the flood insurance premium through the NFIP. Information will only be released as permitted by law.

PURPOSE OF THE ELEVATION CERTIFICATE

The Elevation Certificate is an important administrative tool of the NFIP. It can be used to provide elevation information necessary to ensure compliance with community floodplain management ordinances, to inform the proper insurance premium, and to support a request for a LOMA, CLOMA, LOMR-F, or CLOMR-F.

The Elevation Certificate is used to document floodplain management compliance for Post-Flood Insurance Rate Map (FIRM) buildings, which are buildings constructed after publication of the FIRM, located in flood Zones A1–A30, AE, AH, AO, A (with Base Flood Elevation (BFE)), VE, V1–V30, V (with BFE), AR, AR/A, AR/AE, AR/A1–A30, AR/AH, AR/AO, and A99. It may also be used to provide elevation information for Pre-FIRM buildings or buildings in any flood zone.

As part of the agreement for making flood insurance available in a community, the NFIP requires the community to adopt floodplain management regulations that specify minimum requirements for reducing flood losses. One such requirement is for the community to obtain the elevation of the lowest floor (including basement) of all new and substantially improved buildings, and maintain a record of such information. The Elevation Certificate provides a way for a community to document compliance with the community's floodplain management ordinance.

Use of this certificate does not provide a waiver of the flood insurance purchase requirement. Only a LOMA or LOMR-F from the Federal Emergency Management Agency (FEMA) can amend the FIRM and remove the federal mandate for a lending institution to require the purchase of flood insurance. However, the lending institution has the option of requiring flood insurance even if a LOMA/LOMR-F has been issued by FEMA. The Elevation Certificate may be used to support a LOMA, CLOMA, LOMR-F, or CLOMR-F request. Lowest Adjacent Grade (LAG) elevations certified by a land surveyor, engineer, or architect, as authorized by state law, will be required if the certificate is used to support a LOMA, CLOMA, LOMR-F, or CLOMR-F request. A LOMA, CLOMA, LOMR-F, or CLOMR-F request must be submitted with either a completed FEMA MT-EZ or MT-1 application package, whichever is appropriate. If the certificate will only be completed to support a LOMA, CLOMA, LOMR-F, or CLOMR-F request, there is an option to document the certified LAG elevation on the Elevation Form included in the MT-EZ and MT-1 application.

This certificate is used only to certify building elevations. A separate certificate is required for floodproofing. Under the NFIP, non-residential buildings can be floodproofed up to or above the BFE. A floodproofed building is a building that has been designed and constructed to be watertight (substantially impermeable to floodwaters) below the BFE. Floodproofing of residential buildings is not permitted under the NFIP unless FEMA has granted the community an exception for residential floodproofed basements. The community must adopt standards for design and construction of floodproofed basements before FEMA will grant a basement exception. For both floodproofed non-residential buildings and residential floodproofed basements in communities that have been granted an exception by FEMA, a floodproofing certificate is required.

The expiration date on the form herein does not apply to certified and completed Elevation Certificates, as a completed Elevation Certificate does not expire, unless there is a physical change to the building that invalidates information in Section A Items A8 or A9, Section C, Section E, or Section H. In addition, this form is intended for the specific building referenced in Section A and is not invalidated by the transfer of building ownership.

Additional guidance can be found in FEMA Publication 467-1, *Floodplain Management Bulletin: Elevation Certificate*.

ELEVATION CERTIFICATE

IMPORTANT: MUST FOLLOW THE INSTRUCTIONS ON INSTRUCTION PAGES 1-11

Copy all pages of this Elevation Certificate and all attachments for (1) community official, (2) insurance agent/company, and (3) building owner.

SECTION A – PROPERTY INFORMATION	FOR INSURANCE COMPANY USE
A1. Building Owner's Name: <u>TPI-FMB I, LLC</u>	Policy Number: _____
A2. Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No.: <u>1180 Estero Blvd</u>	Company NAIC Number: _____
City: <u>Fort Myers Beach</u> State: <u>FL</u> ZIP Code: <u>33931</u>	
A3. Property Description (e.g., Lot and Block Numbers or Legal Description) and/or Tax Parcel Number: <u>LOTS 31 THRU 6, BLOCK "B", CRESCENT PARK, STRAP 19-46-24-W4-W0494.2609</u>	
A4. Building Use (e.g., Residential, Non-Residential, Addition, Accessory, etc.): <u>Non-Residential</u>	
A5. Latitude/Longitude: Lat. <u>26°27'08"N</u> Long. <u>81°57'13"W</u> Horiz. Datum: <input type="checkbox"/> NAD 1927 <input checked="" type="checkbox"/> NAD 1983 <input type="checkbox"/> WGS 84	
A6. Attach at least two and when possible four clear color photographs (one for each side) of the building (see Form pages 7 and 8).	
A7. Building Diagram Number: <u>1B</u>	
A8. For a building with a crawlspace or enclosure(s):	
a) Square footage of crawlspace or enclosure(s): <u>1770.00</u> sq. ft.	
b) Is there at least one permanent flood opening on two different sides of each enclosed area? <input type="checkbox"/> Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> N/A	
c) Enter number of permanent flood openings in the crawlspace or enclosure(s) within 1.0 foot above adjacent grade: Non-engineered flood openings: <u>N/A</u> Engineered flood openings: <u>N/A</u>	
d) Total net open area of non-engineered flood openings in A8.c: <u>N/A</u> sq. in.	
e) Total rated area of engineered flood openings in A8.c (attach documentation – see Instructions): <u>N/A</u> sq. ft.	
f) Sum of A8.d and A8.e rated area (if applicable – see Instructions): <u>N/A</u> sq. ft.	
A9. For a building with an attached garage:	
a) Square footage of attached garage: <u>N/A</u> sq. ft.	
b) Is there at least one permanent flood opening on two different sides of the attached garage? <input type="checkbox"/> Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> N/A	
c) Enter number of permanent flood openings in the attached garage within 1.0 foot above adjacent grade: Non-engineered flood openings: <u>N/A</u> Engineered flood openings: <u>N/A</u>	
d) Total net open area of non-engineered flood openings in A9.c: <u>N/A</u> sq. in.	
e) Total rated area of engineered flood openings in A9.c (attach documentation – see Instructions): <u>N/A</u> sq. ft.	
f) Sum of A9.d and A9.e rated area (if applicable – see Instructions): <u>N/A</u> sq. ft.	

SECTION B – FLOOD INSURANCE RATE MAP (FIRM) INFORMATION

B1.a. NFIP Community Name: <u>Town of Ft. Myers Beach</u>	B1.b. NFIP Community Identification Number: <u>120673</u>
B2. County Name: <u>LEE</u>	B3. State: <u>FL</u> B4. Map /Panel No.: <u>12071C0554</u> B5. Suffix: <u>F</u>
B6. FIRM Index Date: <u>11/17/22</u>	B7. FIRM Panel Effective/Revised Date: <u>11/17/22</u>
B8. Flood Zone(s): <u>AE</u>	B9. Base Flood Elevation(s) (BFE) (Zone AO, use Base Flood Depth): <u>12</u>
B10. Indicate the source of the BFE data or Base Flood Depth entered in Item B9: <input type="checkbox"/> FIS <input checked="" type="checkbox"/> FIRM <input type="checkbox"/> Community Determined <input type="checkbox"/> Other: _____	
B11. Indicate elevation datum used for BFE in Item B9: <input type="checkbox"/> NGVD 1929 <input checked="" type="checkbox"/> NAVD 1988 <input type="checkbox"/> Other/Source: _____	
B12. Is the building located in a Coastal Barrier Resources System (CBRS) area or Otherwise Protected Area (OPA)? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No Designation Date: _____ <input type="checkbox"/> CBRS <input type="checkbox"/> OPA	
B13. Is the building located seaward of the Limit of Moderate Wave Action (LiMWA)? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	

ELEVATION CERTIFICATE

IMPORTANT: MUST FOLLOW THE INSTRUCTIONS ON INSTRUCTION PAGES 1-11

Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No.: 1180 Estero Blvd	FOR INSURANCE COMPANY USE
City: <u>Fort Myers Beach</u> State: <u>FL</u> ZIP Code: <u>33931</u>	Policy Number: _____ Company NAIC Number: _____

SECTION C – BUILDING ELEVATION INFORMATION (SURVEY REQUIRED)

- C1. Building elevations are based on: Construction Drawings* Building Under Construction* Finished Construction
 *A new Elevation Certificate will be required when construction of the building is complete.
- C2. Elevations – Zones A1–A30, AE, AH, AO, A (with BFE), VE, V1–V30, V (with BFE), AR, AR/A, AR/AE, AR/A1–A30, AR/AH, AR/AO, A99. Complete Items C2.a–h below according to the Building Diagram specified in Item A7. In Puerto Rico only, enter meters.
 Benchmark Utilized: NGS BM A25-2 Vertical Datum: NAVD88

Indicate elevation datum used for the elevations in items a) through h) below.

NGVD 1929 NAVD 1988 Other: _____

Datum used for building elevations must be the same as that used for the BFE. Conversion factor used? Yes No

If Yes, describe the source of the conversion factor in the Section D Comments area.

Check the measurement used:

- | | | | |
|---|------------|--|---------------------------------|
| a) Top of bottom floor (including basement, crawlspace, or enclosure floor): | <u>6.0</u> | <input checked="" type="checkbox"/> feet | <input type="checkbox"/> meters |
| b) Top of the next higher floor (see Instructions): | <u>N/A</u> | <input type="checkbox"/> feet | <input type="checkbox"/> meters |
| c) Bottom of the lowest horizontal structural member (see Instructions): | <u>5.5</u> | <input checked="" type="checkbox"/> feet | <input type="checkbox"/> meters |
| d) Attached garage (top of slab): | <u>N/A</u> | <input type="checkbox"/> feet | <input type="checkbox"/> meters |
| e) Lowest elevation of Machinery and Equipment (M&E) servicing the building (describe type of M&E and location in Section D Comments area): | <u>6.0</u> | <input checked="" type="checkbox"/> feet | <input type="checkbox"/> meters |
| f) Lowest Adjacent Grade (LAG) next to building: <input type="checkbox"/> Natural <input checked="" type="checkbox"/> Finished | <u>5.4</u> | <input checked="" type="checkbox"/> feet | <input type="checkbox"/> meters |
| g) Highest Adjacent Grade (HAG) next to building: <input type="checkbox"/> Natural <input checked="" type="checkbox"/> Finished | <u>5.8</u> | <input checked="" type="checkbox"/> feet | <input type="checkbox"/> meters |
| h) Finished LAG at lowest elevation of attached deck or stairs, including structural support: | <u>6.0</u> | <input checked="" type="checkbox"/> feet | <input type="checkbox"/> meters |

SECTION D – SURVEYOR, ENGINEER, OR ARCHITECT CERTIFICATION

This certification is to be signed and sealed by a land surveyor, engineer, or architect authorized by state law to certify elevation information. *I certify that the information on this Certificate represents my best efforts to interpret the data available. I understand that any false statement may be punishable by fine or imprisonment under 18 U.S. Code, Section 1001.*

Were latitude and longitude in Section A provided by a licensed land surveyor? Yes No

Check here if attachments and describe in the Comments area.

Certifier's Name: Thomas Michael Rooks JR., PSM License Number: 6347

Title: Director of Surveying

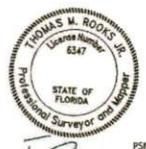
Company Name: Morris-Depew Associates, Inc.

Address: 2914 Cleveland Avenue

City: Fort Myers State: FL ZIP Code: 33901

Telephone: (239) 337-3993 Ext.: 350 Email: Mrooks@m-da.com

Signature:  _____ Date: 2024.01.25 09:55:40 -05'00'



Digitally signed by
 Thomas M. Rooks Jr.
 Date: 2024.01.25
 09:56:01 -05'00'

PSM 6347

Place Seal Here

Copy all pages of this Elevation Certificate and all attachments for (1) community official, (2) insurance agent/company, and (3) building owner.

Comments (including source of conversion factor in C2; type of equipment and location per C2.e; and description of any attachments):

A8(b&c) Plans indicate dry flood proofing Spec sheet 4-A201 Sections
 A5) Latitude and longitude were obtained by handheld GPS device.
 Lowest elevation of equipment referenced by item C2(e) refers to hot water heater

ELEVATION CERTIFICATE

IMPORTANT: MUST FOLLOW THE INSTRUCTIONS ON INSTRUCTION PAGES 1-11

Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No.: 1180 Estero Blvd	FOR INSURANCE COMPANY USE
City: <u>Fort Myers Beach</u> State: <u>FL</u> ZIP Code: <u>33931</u>	Policy Number: _____ Company NAIC Number: _____

SECTION E – BUILDING MEASUREMENT INFORMATION (SURVEY NOT REQUIRED) FOR ZONE AO, ZONE AR/AO, AND ZONE A (WITHOUT BFE)

For Zones AO, AR/AO, and A (without BFE), complete Items E1–E5. For Items E1–E4, use natural grade, if available. If the Certificate is intended to support a Letter of Map Change request, complete Sections A, B, and C. Check the measurement used. In Puerto Rico only, enter meters.

Building measurements are based on: Construction Drawings* Building Under Construction* Finished Construction
 *A new Elevation Certificate will be required when construction of the building is complete.

E1. Provide measurements (C.2.a in applicable Building Diagram) for the following and check the appropriate boxes to show whether the measurement is above or below the natural HAG and the LAG.

a) Top of bottom floor (including basement, crawlspace, or enclosure) is: _____ feet meters above or below the HAG.

b) Top of bottom floor (including basement, crawlspace, or enclosure) is: _____ feet meters above or below the LAG.

E2. For Building Diagrams 6–9 with permanent flood openings provided in Section A Items 8 and/or 9 (see pages 1–2 of Instructions), the next higher floor (C2.b in applicable Building Diagram) of the building is: _____ feet meters above or below the HAG.

E3. Attached garage (top of slab) is: _____ feet meters above or below the HAG.

E4. Top of platform of machinery and/or equipment servicing the building is: _____ feet meters above or below the HAG.

E5. Zone AO only: If no flood depth number is available, is the top of the bottom floor elevated in accordance with the community's floodplain management ordinance? Yes No Unknown The local official must certify this information in Section G.

SECTION F – PROPERTY OWNER (OR OWNER'S AUTHORIZED REPRESENTATIVE) CERTIFICATION

The property owner or owner's authorized representative who completes Sections A, B, and E for Zone A (without BFE) or Zone AO must sign here. *The statements in Sections A, B, and E are correct to the best of my knowledge*

Check here if attachments and describe in the Comments area.

Property Owner or Owner's Authorized Representative Name: _____

Address: 1180 Estero Blvd

City: _____ State: _____ ZIP Code: _____

Telephone: _____ Ext.: _____ Email: _____

Signature: _____ Date: _____

Comments: _____

ELEVATION CERTIFICATE

IMPORTANT: MUST FOLLOW THE INSTRUCTIONS ON INSTRUCTION PAGES 1-11

Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No.: 1180 Estero Blvd	FOR INSURANCE COMPANY USE
City: <u>Fort Myers Beach</u> State: <u>FL</u> ZIP Code: <u>33931</u>	Policy Number: _____ Company NAIC Number: _____

SECTION G – COMMUNITY INFORMATION (RECOMMENDED FOR COMMUNITY OFFICIAL COMPLETION)

The local official who is authorized by law or ordinance to administer the community's floodplain management ordinance can complete Section A, B, C, E, G, or H of this Elevation Certificate. Complete the applicable item(s) and sign below when:

- G1. The information in Section C was taken from other documentation that has been signed and sealed by a licensed surveyor, engineer, or architect who is authorized by state law to certify elevation information. (Indicate the source and date of the elevation data in the Comments area below.)
- G2.a. A local official completed Section E for a building located in Zone A (without a BFE), Zone AO, or Zone AR/AO, or when item E5 is completed for a building located in Zone AO.
- G2.b. A local official completed Section H for insurance purposes.
- G3. In the Comments area of Section G, the local official describes specific corrections to the information in Sections A, B, E and H.
- G4. The following information (Items G5–G11) is provided for community floodplain management purposes.
- G5. Permit Number: 231393 G6. Date Permit Issued: 6/12/23
- G7. Date Certificate of Compliance/Occupancy Issued: _____
- G8. This permit has been issued for: New Construction Substantial Improvement
- G9.a. Elevation of as-built lowest floor (including basement) of the building: _____ feet meters Datum: _____
- G9.b. Elevation of bottom of as-built lowest horizontal structural member: _____ feet meters Datum: _____
- G10.a. BFE (or depth in Zone AO) of flooding at the building site: CAZ 12 feet meters Datum: NAVD
- G10.b. Community's minimum elevation (or depth in Zone AO) requirement for the lowest floor or lowest horizontal structural member: 13 feet meters Datum: NAVD
- G11. Variance issued? Yes No If yes, attach documentation and describe in the Comments area.

The local official who provides information in Section G must sign here. *I have completed the information in Section G and certify that it is correct to the best of my knowledge. If applicable, I have also provided specific corrections in the Comments area of this section.*

Local Official's Name: Kristin Schumacher Title: Floodplain Manager
 NFIP Community Name: T. Fort Myers Beach
 Telephone: 239-765-0202 Ext.: _____ Email: kristin.schumacher@fmbgov.com
 Address: 2525 Estero Blvd
 City: Fort Myers Beach State: FL ZIP Code: 33931

Signature: [Signature] Date: 1/26/24

Comments (including type of equipment and location, per C2.e; description of any attachments; and corrections to specific information in Sections A, B, D, E, or H):

*EC OK
 Dry floodproofing
 certificate
 attached*

ELEVATION CERTIFICATE

IMPORTANT: MUST FOLLOW THE INSTRUCTIONS ON INSTRUCTION PAGES 1-11

Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No.: 1180 Estero Blvd	FOR INSURANCE COMPANY USE
City: <u>Fort Myers Beach</u> State: <u>FL</u> ZIP Code: <u>33931</u>	Policy Number: _____ Company NAIC Number: _____

**SECTION H – BUILDING'S FIRST FLOOR HEIGHT INFORMATION FOR ALL ZONES
(SURVEY NOT REQUIRED) (FOR INSURANCE PURPOSES ONLY)**

The property owner, owner's authorized representative, or local floodplain management official may complete Section H for all flood zones to determine the building's first floor height for insurance purposes. Sections A, B, and I must also be completed. Enter heights to the nearest tenth of a foot (nearest tenth of a meter in Puerto Rico). **Reference the Foundation Type Diagrams (at the end of Section H Instructions) and the appropriate Building Diagrams (at the end of Section I Instructions) to complete this section.**

H1. Provide the height of the top of the floor (as indicated in Foundation Type Diagrams) above the Lowest Adjacent Grade (LAG):

a) **For Building Diagrams 1A, 1B, 3, and 5–8.** Top of bottom _____ feet meters above the LAG floor (include above-grade floors only for buildings with crawlspaces or enclosure floors) is:

b) **For Building Diagrams 2A, 2B, 4, and 6–9.** Top of next _____ feet meters above the LAG higher floor (i.e., the floor above basement, crawlspace, or enclosure floor) is:

H2. Is **all** Machinery and Equipment servicing the building (as listed in Item H2 instructions) elevated to or above the floor indicated by the H2 arrow (shown in the Foundation Type Diagrams at end of Section H instructions) for the appropriate Building Diagram?
 Yes No

SECTION I – PROPERTY OWNER (OR OWNER'S AUTHORIZED REPRESENTATIVE) CERTIFICATION

The property owner or owner's authorized representative who completes Sections A, B, and H must sign here. *The statements in Sections A, B, and H are correct to the best of my knowledge.* **Note:** If the local floodplain management official completed Section H, they should indicate in Item G2.b and sign Section G.

Check here if attachments are provided (including required photos) and describe each attachment in the Comments area.

Property Owner or Owner's Authorized Representative Name: _____

Address: _____

City: _____ State: _____ ZIP Code: _____

Telephone: _____ Ext.: _____ Email: _____

Signature: _____ Date: _____

Comments: _____

ELEVATION CERTIFICATE

IMPORTANT: MUST FOLLOW THE INSTRUCTIONS ON INSTRUCTION PAGES 1-11 BUILDING PHOTOGRAPHS

See Instructions for Item A6.

Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No.:
1180 Estero Blvd

City: Fort Myers Beach State: FL ZIP Code: 33931

FOR INSURANCE COMPANY USE

Policy Number: _____

Company NAIC Number: _____

Instructions: Insert below at least two and when possible four photographs showing each side of the building (for example, may only be able to take front and back pictures of townhouses/rowhouses). Identify all photographs with the date taken and "Front View," "Rear View," "Right Side View," or "Left Side View." Photographs must show the foundation. When flood openings are present, include at least one close-up photograph of representative flood openings or vents, as indicated in Sections A8 and A9.



Photo One

Photo One Caption: WEST SIDE OF BUILDING

Clear Photo One



Photo Two

Photo Two Caption: SOUTH SIDE OF BUILDING

Clear Photo Two

ELEVATION CERTIFICATE

IMPORTANT: MUST FOLLOW THE INSTRUCTIONS ON INSTRUCTION PAGES 1-11

BUILDING PHOTOGRAPHS

Continuation Page

Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No.:
1180 Estero Blvd

City: Fort Myers Beach State: FL ZIP Code: 33931

FOR INSURANCE COMPANY USE

Policy Number: _____

Company NAIC Number: _____

Insert the third and fourth photographs below. Identify all photographs with the date taken and "Front View," "Rear View," "Right Side View," or "Left Side View." When flood openings are present, include at least one close-up photograph of representative flood openings or vents, as indicated in Sections A8 and A9.



Photo Three

Photo Three Caption: NORTHWEST SIDE OF BUILDING

Clear Photo Three



Photo Four

Photo Four Caption: NORTHEAST SIDE OF BUILDING

Clear Photo Four

DRY FLOODPROOFING CERTIFICATE FOR NON-RESIDENTIAL STRUCTURES

PAPERWORK BURDEN DISCLOSURE NOTICE

Public reporting burden for this data collection is estimated to average 3.25 hours per response. The burden estimate includes the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and submitting this form. You are not required to respond to this collection of information unless a valid OMB control number is displayed on this form. Send comments regarding the accuracy of the burden estimate and any suggestions for reducing the burden to: Information Collections Management, Department of Homeland Security, Federal Emergency Management Agency, 500 C Street SW, Washington, DC 20742, Paperwork Reduction Project (1660-0008). **NOTE: Do not send your completed form to this address.**

General: This information is provided pursuant to Public Law 96-511 (the Paperwork Reduction Act of 1980, as amended), dated December 11, 1980, to allow the public to participate more fully and meaningfully in the Federal paperwork review process.

Authority: Public Law 96-511, amended; 44 U.S.C. 3507; and 5 CFR 1320.

PRIVACY ACT STATEMENT

Authority: Title 44 CFR § 60.3, 61.7 and 61.8.

Principal Purpose(s): This information is being collected for the primary purpose of estimating the risk premium rates necessary to provide flood insurance for new or substantially improved structures in designated Special Flood Hazard Areas.

Routine Use(s): The information on this form may be disclosed as generally permitted under 5 U.S.C. § 552a(b) of the Privacy Act of 1974, as amended. This includes using this information as necessary and authorized by the routine uses published in DHS/FEMA-003 – National Flood Insurance Program Files System or Records Notice 79 Fed. Reg. 28747 (May 19, 2014), and upon written request, written consent, by agreement, or as required by law.

Disclosure: The disclosure of information on this form is voluntary; however, failure to provide the information requested may result in the inability to obtain flood insurance through the National Flood Insurance Program or being subject to higher premium rates for flood insurance. Information will only be released as permitted by law.

PURPOSE OF THE DRY FLOODPROOFING CERTIFICATE FOR NON-RESIDENTIAL STRUCTURES

Under the National Flood Insurance Program (NFIP), the dry floodproofing of non-residential buildings may be permitted as an alternative to elevating to or above the Base Flood Elevation (BFE) or for certain flood zones, the natural Highest Adjacent Grade (HAG). A dry floodproofing design certification is required for non-residential structures that are dry floodproofed and the dry floodproofed non-residential portions of mixed-use buildings. This form is to be used for that certification. FEMA Form 206-FY-21-122 NFIP Residential Basement Floodproofing Certificate is required for the residential portions of mixed-use buildings.

A dry floodproofed building is a building that has been designed and constructed to be watertight (substantially impermeable to floodwaters) below the BFE and with structural components having the capability of resisting hydrostatic and hydrodynamic loads and effects of buoyancy. Before a dry floodproofed building is designed, numerous planning considerations, including flood warning time, uses of the building, mode of entry to and exit from the building and the site in general, floodwater velocities, flood depths, debris impact potential, flood frequency, and any other State and local requirements must be addressed to ensure that dry floodproofing will be a viable floodplain management measure.

The minimum NFIP requirement is to dry floodproof a building to the BFE. However, to be in compliance with the requirements of American Society of Civil Engineers (ASCE) 24, *Flood Resistant Design and Construction*, one foot is subtracted from the dry floodproofed elevation. Therefore, a building must be dry floodproofed to one foot above the BFE to be considered for floodproofing credit. For B, C, D, or X flood zones, the building's dry floodproofed design elevation must be at least two feet above the natural HAG to be considered for floodproofing credit.

Additional guidance can be found in FEMA Publication 936, *Floodproofing Non-Residential Buildings* (2013), and NFIP Technical Bulletin 3, *Requirements for the Design and Certification of Dry Floodproofed Non-Residential and Mixed-Use Buildings* (2021), available on FEMA's Building Science Resource Library website at www.fema.gov/ar/emergency-managers/risk-management/building-science/publications.

Copy all pages of this Dry Floodproofing Certificate and all attachments for 1) community official, 2) insurance agent/company, and 3) building owner. The dry floodproofing of non-residential buildings and the non-residential portions of mixed-use buildings may be permitted as an alternative to elevating to or above the Base Flood Elevation (BFE); however, a dry floodproofing design certification is required. This form is to be used for that certification. Dry floodproofing of a residential building does not alter a community's floodplain management elevation requirements or affect the insurance rating unless the community has been issued an exception by FEMA to allow dry floodproofed residential basements. The permitting of a dry floodproofed residential basement requires a separate certification specifying that the design complies with the local floodplain management ordinance.

PROPERTY INFORMATION

Building Owner's Name: <u>TPI-FMB I, LLC</u> Building Street Address (Including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No.: <u>1180 Estero Blvd</u> City: <u>Fort Myers Beach</u> State: <u>FL</u> ZIP Code: <u>33931</u> Property Description (e.g., Lot and Block Numbers, or Legal Description) and/or Tax Parcel Number: <u>Building #4 LOTS 31 THRU 6. BLOCK "B". CRESENT PARK. STRAP 19-46-24-W4-W0494.2609</u> Building Use (e.g., Non-Residential, Mixed Use, Addition, Accessory, etc.): <u>Non-Residential</u> Latitude/Longitude: Lat. <u>26°27'08"N</u> Long. <u>81°57'13"W</u> Horizontal Datum: <input type="checkbox"/> NAD 1927 <input checked="" type="checkbox"/> NAD 1983 <input type="checkbox"/> WGS 84	FOR INSURANCE COMPANY USE Policy Number: _____ Company NAIC Number: _____
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SECTION I – FLOOD INSURANCE RATE MAP (FIRM) INFORMATION

NFIP Community Name: Town of Fort Myers Beach NFIP Community Identification Number: 120673
 County Name: Lee State: FL Map/Panel Number: 12071C0554 Suffix: G
 FIRM Index Date: 11/17/2022 FIRM Panel Effective/Revised Date: 11/17/2022 Flood Zone(s): AE
 BFE(s) (Zone AO, use Base Flood Depth (BFD)): 12
 Indicate the source of the BFE data or BFD entered above: Flood Insurance Study (FIS) FIRM
 Community Determined Other: _____
 Indicate elevation datum used for BFE shown above: NGVD 1929 NAVD 1988 Other/Source: _____
 Is a Limit of Moderate Wave Action (LiMWA) shown on the FIRM? Yes No
 If Yes, is the property located in the Coastal A Zone [area between the LiMWA and Zone V boundary (or shoreline)]? Yes No
 Is the property located in a floodway? Yes No If Yes, provide the velocity at the building location: _____
 Is the property located in an alluvial fan? Yes No
 If Yes, provide the depth at the building location: _____ and velocity: _____

SECTION II – DRY FLOODPROOFED DESIGN CERTIFICATION

(By a Registered Professional Engineer or Architect licensed in the State where the building is located)

(Note: For insurance rating purposes in all zones except for B, C, D, or X, the building's dry floodproofed design elevation must be at least one foot above the BFE to be considered for floodproofing credit. For B, C, D, or X Zones, the building's dry floodproofed design elevation must be at least two feet above the natural HAG to be considered for floodproofing credit. If the building is not dry floodproofed to the above-mentioned standards, then the building will be ineligible for floodproofing credit. See the Instructions section for information on documentation that must accompany this certificate if being submitted for flood insurance rating purposes.)

Briefly list measures incorporated into the design to meet the performance criteria for dry floodproofing and attach calculations showing the structure is designed with structural components that have the capability of resisting hydrostatic and hydrodynamic loads and the effects of buoyancy and will be watertight and substantially impermeable to the passage of water.

1. Engineered flood panels for all large exterior openings.
2. Sump pump provided per ASCE 24-14 Section 6.2.
3. All exterior walls designed to meet requirements of ASCE 24-14 Section 6.2.2.
4. The piles, grade beams, 16 inch thick slab, and 14 inch thick concrete walls were design to resist the forces associated with flood loading. See attached structural calculations.

Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No.: <u>1180 Estero Blvd</u>	FOR INSURANCE COMPANY USE
City: <u>Fort Myers Beach</u> State: <u>FL</u> ZIP Code: <u>33931</u>	Policy Number: _____ Company NAIC Number: _____

SECTION II – DRY FLOODPROOFED DESIGN CERTIFICATION (Continued)
 (By a Registered Professional Engineer or Architect licensed in the State where the building is located)

Provide elevations used in design, specifications and construction drawings. In Puerto Rico only, enter meters.

Indicate elevation datum used for the elevations in this section. NGVD 1929 NAVD 1988 Other/Source: _____

Elevation datum used for building elevations must be the same as that used for the BFE. Conversion factor used? Yes No
 If Yes, describe the source of the conversion factor in the Comments area of this Section.

A. Dry Floodproofed Design Elevation: _____ 13 feet meters

B. Lowest Adjacent Grade (LAG) next to the building: Natural Finished _____ 5.6 feet meters

C. Highest Adjacent Grade (HAG) next to the building: Natural Finished _____ 5.95 feet meters

Non-Residential Dry Floodproofed Design Certification:

I certify the structure, based upon development and/or review of the design and specifications for construction, has been designed in accordance with the accepted standards of practice (ASCE 24-05, ASCE 24-14 or their equivalent) and the following provisions.

- *The structure, together with attendant utilities and sanitary facilities will be watertight to the dry floodproofed design elevation indicated above, will be substantially impermeable to the passage of water, and shall perform in accordance with the 44 Code of Federal Regulations (44 CFR 60.3(c)(3)).*
- *All structural components are capable of resisting hydrostatic and hydrodynamic flood forces, including the effects of buoyancy, and anticipated debris impact forces up to the dry floodproofed design elevation. Flood damage-resistant materials are used for all areas where seepage is intended to collect inside the dry floodproofed areas up to at least 4 inches above the floor.*

I certify that the information in Section II on this certificate represents a true and accurate determination by the undersigned using the available information and data. I understand that any false statement may be punishable by fine or imprisonment under 18 U.S. Code, Section 1001.

Certifier's Name: Jeffrey H. Zander License Number (or Affix Seal): 17043

Title: Senior Structural Engineer Company Name: Ramaker Professional Services

Mailing Address: 855 Community Drive

City: Sauk City State: WI ZIP Code: 53583

Phone #1: (608) 643-4100 Ext.: _____ Phone #2: _____ Ext.: _____

Email: jzander@ramaker.com



Signature:  Digitally signed by Jeffrey H Zander
 Date: 2024.02.15 12:23:27-06'00' Date: 02/15/2024

Comments (including source of conversion factor and description of any attachments):

1. Shop drawing package of engineered flood panels.
2. Cut sheet of sump pump installed including battery backup power.
3. Structural calculations showing compliance with ASCE 24-14 Section 6.2.2.

Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No.: <u>1180 Estero Blvd</u>	FOR INSURANCE COMPANY USE
City: <u>Fort Myers Beach</u> State: <u>FL</u> ZIP Code: <u>33931</u>	Policy Number: _____ Company NAIC Number: _____

SECTION III – DRY FLOODPROOFED ELEVATION CERTIFICATION
 (By a Registered Professional Land Surveyor, Engineer or Architect licensed in the State where the building is located)

Benchmark Utilized: NGS BM A25-2 Vertical Datum: NAVD 88

Indicate elevation datum used for the elevations provided in this section:
 NGVD 1929 NAVD 1988 Other/Source: _____

Elevation datum used for building elevations must be the same as that used for the BFE. Conversion factor used? Yes No
 If Yes, describe the source of the conversion factor in the Comments area of this section.

A. Dry floodproofed elevation (must be based on finished construction): _____ 13.3 feet meters

B. Lowest Adjacent Grade (LAG) next to the building: Natural Finished _____ 5.4 feet meters

C. Natural Highest Adjacent Grade (HAG) next to the building: _____ 5.8 feet meters

Height of floodproofing on the building above the natural or finished LAG is _____ 7.9 feet.
 (In Puerto Rico only: _____ meters.)

(Note: For insurance rating purposes in all eligible zones inside the SFHA, the building's dry floodproofed design elevation must be at least one foot above the BFE to be considered for floodproofing credit. For B, C, D, or X Zones, the building's dry floodproofed design elevation must be at least two feet above the natural HAG. If the building is not dry floodproofed to the above-mentioned standards, then the building will not be considered for floodproofing credit. See the Instructions section for information on documentation that must accompany this certificate if being submitted for flood insurance rating purposes.)

Non-Residential Dry Floodproofed Elevation Information Certification:

Section III certification is to be signed and sealed by a land surveyor, engineer, or architect authorized by law to certify elevation information.

I certify that the information in Section III on this Certificate represents a true and accurate interpretation and determination by the undersigned using the available information and data. I understand that any false statement may be punishable by fine or imprisonment under 18 U.S. Code, Section 1001.

Certifier's Name: <u>Thomas Michael Rooks JR., PSM</u> License Number (or Affix Seal): <u>6347</u>	<div style="border: 1px solid black; height: 100%; width: 100%; display: flex; align-items: center; justify-content: center;"> <div style="border: 1px solid black; width: 80%; height: 80%; margin: 10px;"></div> </div> <p style="margin-top: 10px;">Place Seal Here</p>
Title: <u>Director of Surveying</u> Company Name: <u>Morris-Depew Associates, Inc.</u>	
Mailing Address: <u>2914 Cleveland Avenue, Inc.</u>	
City: <u>Fort Myers</u> State: <u>FL</u> ZIP Code: <u>33901</u>	
Phone #1: <u>(239) 337-3993</u> Ext.: _____ Phone #2: _____ Ext.: _____	
Email: <u>Mrooks@m-da.com</u>	

Signature: _____ Date: 02/15/2024

Comments (including source of conversion factor and description of any attachments):

Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No.: <u>1180 Estero Blvd</u>	FOR INSURANCE COMPANY USE
City: <u>Fort Myers Beach</u> State: <u>FL</u> ZIP Code: <u>33931</u>	Policy Number: _____
	Company NAIC Number: _____

SECTION IV – DRY FLOODPROOFED CONSTRUCTION CERTIFICATION
(By a Registered Professional Engineer or Architect licensed in the State where the building is located)

Non-Residential Dry Floodproofed Construction Certification:

I certify the structure, based upon development and/or review of the design, specifications, as-built drawings for construction and physical inspection, has been designed and constructed in accordance with the accepted standards of practice (ASCE 24-05, ASCE 24-14 or their equivalent) and any alterations also meet those standards and the following provisions.

- *The structure, together with attendant utilities and sanitary facilities is watertight to the dry floodproofed design elevation indicated above, is substantially impermeable to the passage of water, and shall perform in accordance with the 44 Code of Federal Regulations (44 CFR 60.3(c)(3)).*
- *All structural components are capable of resisting hydrostatic and hydrodynamic flood forces, including the effects of buoyancy, and anticipated debris impact forces up to the dry floodproofed design elevation.*
- *The floodproofed elevation is in accordance with the design and any alteration(s) to the design.*
- *Flood damage-resistant materials have been incorporated/used in all areas where seepage would collect inside the dry floodproofed areas up to at least 4 inches above the floor.*

I certify that the information in Section IV on this certificate represents a true and accurate determination by the undersigned using the available information and data. I understand that any false statement may be punishable by fine or imprisonment under 18 U.S. Code, Section 1001.

Certifier's Name: Jeffrey H. Zander License Number (or Affix Seal): 17043

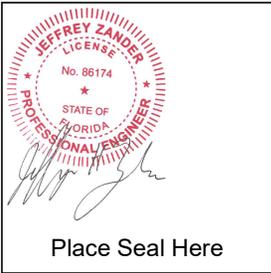
Title: Senior Structural Engineer Company Name: Ramaker Professional Services

Mailing Address: 855 Community Drive

City: Sauk City State: WI ZIP Code: 53583

Phone #1: (608) 643-4100 Ext.: _____ Phone #2: _____ Ext.: _____

Email: izander@ramaker.com



Signature:  Digitally signed by Jeffrey H Zander
Date: 2024.02.15 12:26:51-06'00' Date: 02/15/2024

**Copy all pages of this Dry Floodproofing Certificate and all attachments for:
1) community official, 2) insurance agent/company, and 3) building owner.**

REQUIRED DOCUMENTATION

In order to ensure compliance and provide reasonable assurance that due diligence had been applied in designing and constructing dry floodproofing measures, the following information must be provided with the completed Dry Floodproofing Certificate:

- 1. Photographs.** All photographs must be clear and in color, identified and include the date taken. Where the building is in the course of construction, provide clear descriptions of any other dry floodproofed components and attachments to be incorporated.
 - a. Photographs of all sides and aspects of the floodproofed building.
 - b. Photographs of all components used to provide dry floodproofing protections (shields, gates, barriers, sump pumps, backflow (non-return) valves or shutoff valves, etc.).
 - c. Photographs of the installed barriers/shields and corresponding clear photographs of openings areas where barriers and shields are deployed without the barriers/shields installed (doors, windows, ventilation intakes, etc.).
 - d. Photographs of penetrations through dry floodproofed envelopes (utilities, mechanical).
 - e. Photographs of backup power source for sump pumps.

- 2. Comprehensive Flood Emergency Operations Plan** for the entire structure to include but not limited to:
 - a. The personnel, equipment, tools, and supplies needed to deploy all dry floodproofing system components with sufficient time prior to the onset of flooding or conditions such as high winds that could interfere with efficient deployment of measures.
 - b. Clearly defined chain of command and assigned responsibilities for personnel involved in the installation of dry floodproofing measures.
 - c. Procedure for notifying personnel responsible for installing dry floodproofing measures, along with a list of duty requirements.
 - d. Decision tree that identifies the sequence, timeline, and responsible parties for installing the dry floodproofing components, including the triggers or benchmarks that will initiate procedures.
 - e. Written description and map of the storage locations and types of dry floodproofing measures to be installed or deployed (shields, gates, barriers, and components as well as all associated hardware), along with any equipment, tools, and materials required for installation.
 - f. Conditions that require the deployment of active dry floodproofing measures (e.g., installation of flood shields, closing of flood doors, closing of manual valves, staging of pumps).
 - g. Instructions for installing or deploying each dry floodproofing measure and the order of installation if important for effectiveness.
 - h. Instructions for connecting standby (emergency) power source (e.g., generator) for critical equipment such as sump pumps and egress lighting
 - i. Contact information for the manufacturer and designer to expedite obtaining replacement parts and support as needed
 - j. Evacuation plans for all personnel
 - k. Requirements for installation and deployment drills and training program (at least once a year)
 - l. Requirement for regular review and update of the plan procedures

- 3. Comprehensive Inspection and Maintenance Plan** for the entire structure to include but not limited to:
 - a. Exterior envelope of the structure, such as wall and foundation systems, to identify possible structural and waterproofing deficiencies such as cracks, water staining, and penetrations.
 - b. All penetrations to the exterior of the structure.
 - c. Slabs and wall/slab joints, including structural and drainage deficiencies.
 - d. Flood shields, gates, panels, doors, glazing, barriers, and other components designed to provide dry floodproofing protection, including all seals, gaskets, fasteners, and mounting hardware and tools.
 - e. Sump pumps (or self-priming pumps) and interior drain system.
 - f. Emergency power systems.
 - g. Testing of emergency generators, sump pumps, and other drainage measures.
 - h. Backflow (non-return) valves or shutoff valves.
 - i. Location of all flood shields, gates, panels, and other components including all hardware along with any materials or tools needed to seal the dry floodproofed area.
 - j. Contact information for the manufacturer of the shields and other components to determine the availability of replacement gaskets, seals, and other parts and to ask questions.
 - k. Cadence of inspection and maintenance plan.

- 4. Building owner** acknowledgment that verifies that the owner is aware of the criteria for when the dry floodproofing measures must be installed and that they know how to install all the measures. This would be signed by the owner. Additionally, if the measures are to be installed by a third-party, then the third-party contractor must sign that they know how to install the measures.

DEPARTMENT OF HOMELAND SECURITY
Federal Emergency Management Agency

**INSTRUCTIONS FOR COMPLETING THE DRY FLOODPROOFING CERTIFICATE
FOR NON-RESIDENTIAL STRUCTURES**

To receive credit for dry floodproofing, a completed Dry Floodproofing Certificate for Non-Residential Structures is required for non-residential buildings and the non-residential portions of mixed-use buildings in the Regular Program communities, located in all flood zones, including Zone X. For certification of finished construction, this form is invalid without Sections I through IV.

PROPERTY INFORMATION

This section identifies the building, its location, and its owner. Enter the name(s) of the building owner(s), the building's complete street address, and/or property description. If the building's address is different from the owner's address, enter the address of the building being certified. If the address is a rural route or a Post Office box number, enter the lot and block numbers, the tax parcel number, the legal description, or an abbreviated location description based on distance and direction from a fixed point of reference.

A map may be attached to this certificate to show the location of the building on the property. A tax map, FIRM, or detailed community map is appropriate. If no map is available, provide a sketch of the property location, and the location of the building on the property. Include appropriate landmarks such as nearby roads, intersections, and bodies of water. For building use, indicate whether the building is residential, non-residential, an addition to an existing residential or non-residential building, an accessory building (e.g., garage), or other type of structure. Use the Comments area of the appropriate section if needed or attach additional comments.

Provide latitude and longitude coordinates for the center of the front of the building. Use either decimal degrees (e.g., 39.504322°, -110.758522°) or degrees, minutes, seconds (e.g., 39° 30' 15.52", -110° 45' 30.72") format. If decimal degrees are used, provide coordinates to at least 6 decimal places or better. When using degrees, minutes, seconds, provide seconds to at least 2 decimal places or better. Provide the datum of the latitude and longitude coordinates (FEMA prefers the use of NAD 1983). Indicate the method or source used to determine the latitude and longitude in the Comments area.

SECTION I – FLOOD INSURANCE RATE MAP (FIRM) INFORMATION

Complete the Dry Floodproofing Certificate using the Flood Insurance Study (FIS) and FIRM in effect at the time of the certification.

The information for Section I is obtained by reviewing the FIS and the FIRM panel that includes the building's location. Information about the current FIS and FIRM is available from FEMA by visiting msc.fema.gov or contacting the local floodplain administrator. If a Letter of Map Amendment (LOMA), Letter of Map Revision (LOMR), or LOMR Based on Fill (LOMR-F) has been issued by FEMA, please provide the letter date and case number in the Comments area, as appropriate.

For a building in an area that was mapped in one community but is now in another community due to annexation or dissolution, enter the community name and 6-digit number of the community in which the building is now located in the name of the county or new county, if necessary; and the FIRM index date for the community the building is now located in. Enter information from the actual FIRM panel that shows the building location, even if it is the FIRM for the previous jurisdiction. If the map in effect at the time of the building's construction was other than the current FIRM, and you have the past map information pertaining to the building, provide the information in the Comments area.

Note: Indicate in the Comments Section, if using information based on best available data, such as base-level engineering or advisory flood hazard data (contact the local floodplain administrator to confirm).

NFIP Community Name & Community Identification Number. Enter the complete name of the community in which the building is located, and the associated 6-digit Community Identification Number. For a newly incorporated community, use the name and 6-digit number of the new community. Under the NFIP, a "community" is any State or area or political subdivision thereof, or any Indian tribe or authorized native organization which has authority to adopt and enforce floodplain management regulations for the areas within its jurisdiction. To determine the current community number, see the NFIP *Community Status Book*, available on FEMA's web site at www.fema.gov/national-flood-insurance-program-community-status-book.

County Name. Enter the name of the county or counties in which the community is located. For an unincorporated area of a county, enter the county name and "unincorporated area." For an independent city, enter "independent city."

State. Enter the 2-letter state abbreviation (for example, VA, TX, CA).

Map/Panel Number and Suffix. Enter the 10-character "Map Number" or "Community Panel Number" shown on the FIRM where the building or manufactured (mobile) home is located. For maps in a county-wide format, the sixth character of the "Map Number" is the letter "C" followed by a 4-digit map number. For maps not in a county-wide format, enter the "Community Panel Number" shown on the FIRM.

FIRM Index Date. Enter the effective date or the map revised date shown on the FIRM Index.

FIRM Panel Effective/Revised Date. Enter the effective date shown on the current FIRM panel. The current FIRM panel effective date can be determined by visiting msc.fema.gov or contacting the local floodplain administrator. In addition, if the area where the building is located was revised by a LOMR, include the LOMR effective date.

Flood Zone(s). Enter the flood zone, or flood zones, in which the building is located. All flood zones containing the letter "A" or "V" are considered Special Flood Hazard Areas. The flood zones are A, AE, A1–A30, V, VE, V1–V30, AH, AO, AR, AR/A, AR/AE, AR/A1–A30, AR/AH, AR/AO. Each flood zone is defined in the legend of the FIRM panel on which it appears.

BFE(s). Using the appropriate Flood Insurance Study (FIS) Profile, FIS Data Table (e.g., Transect, Floodway, etc.), or FIRM panel, locate the property and enter the BFE (or base flood depth) of the building site to the nearest tenth of a foot (nearest tenth of a meter, in Puerto Rico). If the building is located in more than one flood zone, list all appropriate BFEs.

BFEs are shown in the FIS or on a FIRM for Zones A1–A30, AE, AH, V1–V30, VE, AR, AR/A, AR/AE, AR/A1–A30, AR/AH, and AR/AO; flood depth numbers are shown for Zone AO. Use the AR BFE if the building is located in any of Zones AR/A, AR/AE, AR/A1–A30, AR/AH, or AR/AO.

In unnumbered A or V zones where BFEs are not provided in the FIS or on the FIRM, BFEs may be available from another source. For example, the community may have established BFEs or obtained BFE data from other sources (e.g., Base Level Engineering) for the building site. For subdivisions and other developments of more than 50 lots or 5 acres in Zone A, establishment of BFEs is required per Floodplain Management requirements 44 CFR 60.3(b)(3). If a BFE is obtained from another source, enter the BFE. The BFE entered must be based on hydrologic and hydraulic analyses. In an unnumbered A Zone where BFEs are not obtained from another source, enter N/A.

For areas in which BFEs have not been established, designers can refer to FEMA 265 *Zone A Manual: Managing Floodplain Development in Approximate Zone A Areas* (FEMA 1995), https://www.fema.gov/sites/default/files/documents/fema_approx-zone-a-guide.pdf?id=2215. This guide provides information on obtaining and developing BFEs.

Source of BFE. Indicate the source of the BFE or flood depth that you entered. If the BFE is from a source other than FIS Profile, FIRM, or community, include the name of the study, the agency or company that produced it, and the date when the study was completed. Visit msc.fema.gov or contact the local floodplain administrator to access the current FIS and FIRM.

Elevation Datum. Indicate the elevation datum to which the elevations on the applicable FIRM are referenced as shown on the map legend. The vertical datum is shown in the Map Legend and/or the Notes to Users on the FIRM.

Limit of Moderate Wave Action (LiMWA). Indicate if a LiMWA is shown on the FIRM and the location of the building in relation to the LiMWA.

Floodway. Indicate if building is in a floodway and if applicable, the velocity in the area of the building. See FEMA P-936, *Floodproofing Nonresidential Buildings* for more information on determining the velocity.

Alluvial Fan. Indicate if building is in an alluvial fan and if applicable, the depth and velocity in the area of the building.

SECTION II – DRY FLOODPROOFED DESIGN CERTIFICATION

Section II is to be completed by a Registered Professional Engineer or Architect licensed in the State where the building is located to certify the design of the dry floodproofing measures as required by 44 CFR 60.3(c)(4).

SECTION III – DRY FLOODPROOFED ELEVATION CERTIFICATION

Section III is to be completed by a Registered Professional Land Surveyor, Engineer, or Architect licensed in the State where the building is located to provide the surveyed elevations of the as-built construction. To ensure that all required elevations are obtained, it will be necessary to physically enter the building.

SECTION IV – DRY FLOODPROOFED CONSTRUCTION CERTIFICATION

Section IV is to be completed by a Registered Professional Engineer or Architect licensed in the state where the building is located to certify the structure, based upon development and/or review of the design, specifications, as-built drawings for construction and physical inspection, has been designed and constructed in accordance with the accepted standards of practice (ASCE 24-05, ASCE 24-14 or their equivalent) and any alterations also meet those standards and the provisions listed in Section IV.

BUILDING 4 DRY FLOODPROOFING PHOTOS

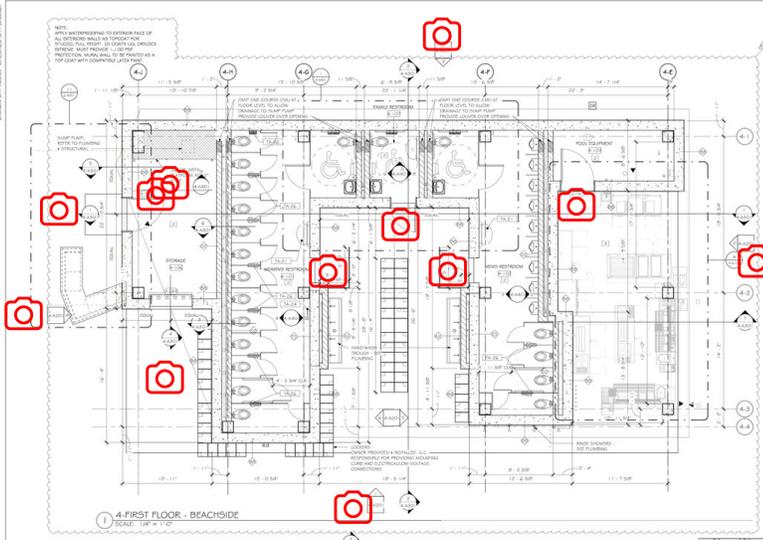
Prepared by : Tablet1 Ramaker & Associates

Jan 24, 2024

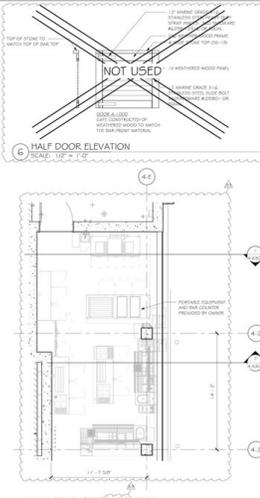
Description

Issued by tablet1@ramaker.com

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1 4-FIRST FLOOR - BEACHSIDE SCALE: 1/8" = 1'-0"



6 HALF DOOR ELEVATION SCALE: 1/2" = 1'-0"

4 4-BEACHSIDE PATIO AREA SCALE: 1/8" = 1'-0"

- KEY NOTES**
- 1. THIS PLAN SHOWS THE LOCATION OF FINISH THAT ARE ARCHITECTURALLY DIFFERENT FROM PLUMBING, MECHANICAL, AND ELECTRICAL FINISH INDICATED BY OTHER NOTES.
 - 2. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 3. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 4. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 5. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 6. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 7. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 8. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 9. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
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 - 11. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 12. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 13. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 14. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
- RCP SHEET KEY NOTES**
- 1. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 2. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
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 - 8. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 9. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 10. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 11. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 12. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 13. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 14. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
- RCP LEGEND**
- 1. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 2. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 3. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 4. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 5. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 6. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 7. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
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 - 11. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 12. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 13. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
 - 14. SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.

RAMAKER & ASSOCIATES, INC.
 815 Community Dr. Suite 200 Ft. Myers, FL 33904
 (888) 444-4444 ramaker.com
 815 Community Dr. Suite 200 Ft. Myers, FL 33904
 (888) 444-4444 ramaker.com

PROJECT LOCATION

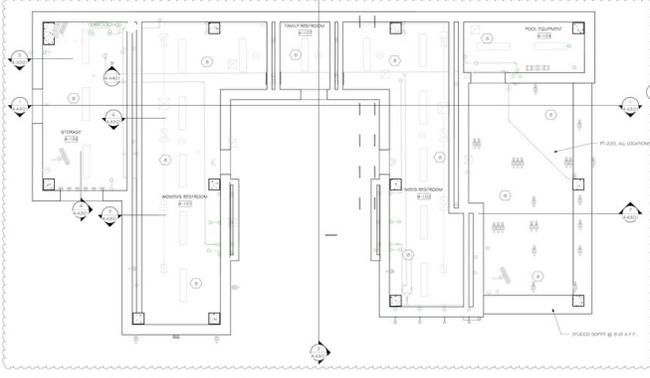
PROJECT NAME
TPI-FMB

PROJECT ADDRESS
FT. MYERS BEACH, FL

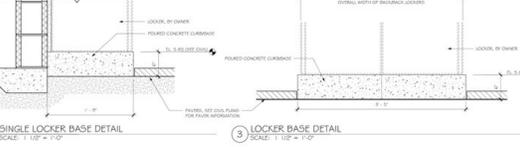
PROJECT FLOOR
FLOOR 4 CEILING PLANS

PROJECT NUMBER
30479

PROJECT DATE
4-A101



2 4-FIRST FLOOR REFLECTED CEILING PLAN - BEACHSIDE SCALE: 1/8" = 1'-0"



5 SINGLE LOCKER BASE DETAIL SCALE: 1/2" = 1'-0"

3 LOCKER BASE DETAIL SCALE: 1/2" = 1'-0"

TOILET ACCESSORY LEGEND

ACCESSORY TAG	DESCRIPTION	MANUFACTURER MODEL	FINISH	LOCATION	NOTES
PL-1	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-2	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-3	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-4	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-5	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-6	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-7	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-8	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-9	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-10	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-11	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-12	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-13	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-14	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-15	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-16	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-17	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-18	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-19	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-20	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-21	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-22	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-23	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-24	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-25	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
PL-26	TOILET	AMERICAN STANDARD	WHITE	RESTROOM	RESTROOM
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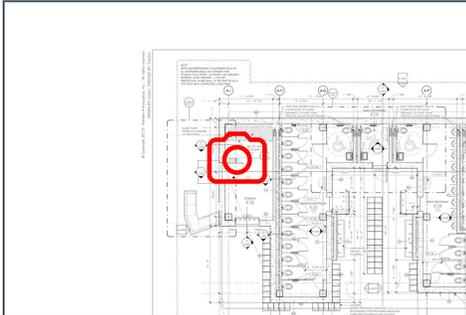
DOOR SCHEDULE - BUILDING 4

NO.	SIZE	TYPE	MATERIAL	FINISH	FRAME	GLASS	SWITCH	OPERATION	NOTES
1	3'-0" x 7'-0"	SLIP	ALUMINUM	ANODIZED	ALUMINUM	GLASS	NO	SWING	SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
2	3'-0" x 7'-0"	SLIP	ALUMINUM	ANODIZED	ALUMINUM	GLASS	NO	SWING	SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
3	3'-0" x 7'-0"	SLIP	ALUMINUM	ANODIZED	ALUMINUM	GLASS	NO	SWING	SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.

OVERHEAD/CEILING LIGHTS - BUILDING 4

NO.	SIZE	TYPE	MATERIAL	FINISH	FRAME	GLASS	SWITCH	OPERATION	NOTES
1	4'-0" x 4'-0"	RECESSED	ALUMINUM	ANODIZED	ALUMINUM	GLASS	NO	SWING	SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
2	4'-0" x 4'-0"	RECESSED	ALUMINUM	ANODIZED	ALUMINUM	GLASS	NO	SWING	SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.
3	4'-0" x 4'-0"	RECESSED	ALUMINUM	ANODIZED	ALUMINUM	GLASS	NO	SWING	SEE SHEET 405 FOR FINISH SCHEDULE AND DETAILS. SEE THE ADD SHEETS FOR THE DIFFERENTIAL CEILING PLAN.

Sump Pump Installation



Created:
tablet1@ramaker.com
Jan 18, 2024 12:41 PM

Last Updated:
tablet1@ramaker.com
Jan 18, 2024 1:59 PM



IMG_6704
Taken on:
Jan 18, 2024 11:39 AM
Added on:
Jan 18, 2024 12:39 PM
Added by:
Tablet1 Ramaker & Associates



IMG_6710
Added on:
Jan 18, 2024 1:59 PM
Added by:
Tablet1 Ramaker & Associates



IMG_6709

Added on:
Jan 18, 2024 1:59 PM

Added by:
Tablet1 Ramaker & Associates



IMG_6705

Added on:
Jan 18, 2024 12:42 PM

Added by:
Tablet1 Ramaker & Associates



IMG_6703

Added on:
Jan 18, 2024 12:42 PM

Added by:
Tablet1 Ramaker & Associates

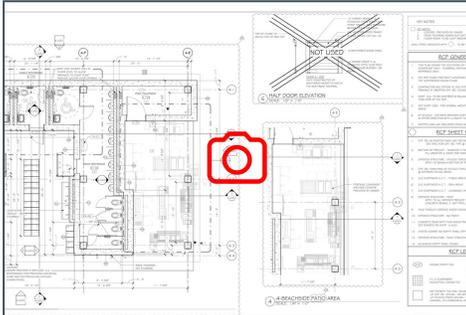


IMG_6671

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Jan 18, 2024 12:42 PM

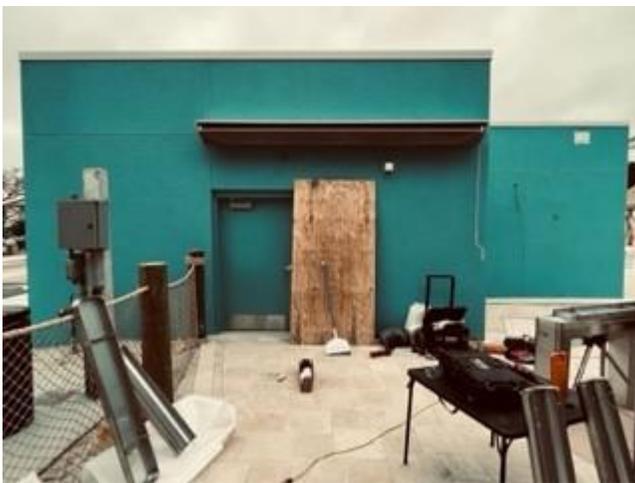
Added by:
Tablet1 Ramaker & Associates

NORTH EXTERIOR



Created:
tablet1@ramaker.com
Jan 5, 2024 3:37 PM

Last Updated:
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Jan 5, 2024 3:37 PM

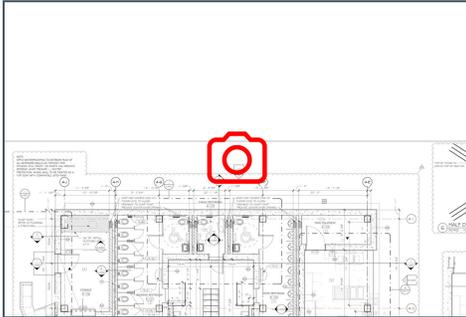


North side of Building

Added on:
Jan 5, 2024 3:37 PM

Added by:
Tablet1 Ramaker & Associates

WEST EXTERIOR



Created:
tablet1@ramaker.com
Jan 5, 2024 3:35 PM

Last Updated:
tablet1@ramaker.com
Jan 5, 2024 3:37 PM

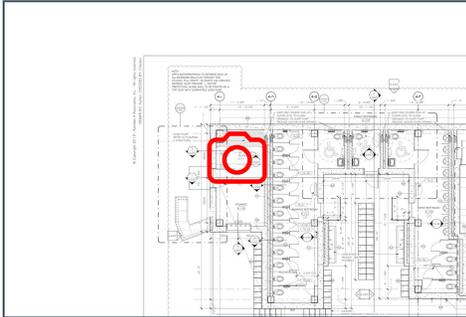


West side of Building

Added on:
Jan 5, 2024 3:37 PM

Added by:
Tablet1 Ramaker & Associates

PANEL STORAGE



Created:
tablet1@ramaker.com
Jan 5, 2024 3:35 PM

Last Updated:
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Jan 5, 2024 3:35 PM



Panel Storage 2

Added on:
Jan 5, 2024 3:35 PM

Added by:
Tablet1 Ramaker & Associates

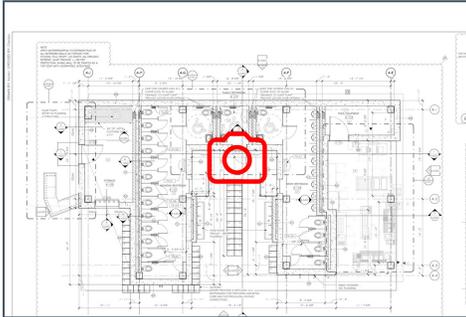


Panel Storage

Added on:
Jan 5, 2024 3:35 PM

Added by:
Tablet1 Ramaker & Associates

DOOR 4-107



Created:
tablet1@ramaker.com
Jan 5, 2024 3:34 PM

Last Updated:
tablet1@ramaker.com
Jan 5, 2024 3:34 PM



B 4-107 Installed

Added on:
Jan 5, 2024 3:34 PM

Added by:
Tablet1 Ramaker & Associates

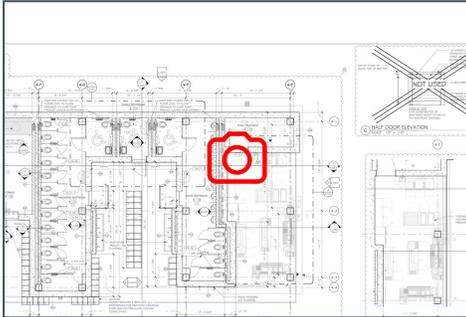


Door 4-107

Added on:
Jan 5, 2024 3:34 PM

Added by:
Tablet1 Ramaker & Associates

DOOR 4-103



Created:
tablet1@ramaker.com
Jan 5, 2024 3:33 PM

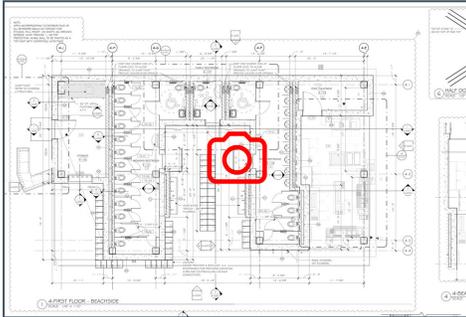
Last Updated:
tablet1@ramaker.com
Jan 5, 2024 3:34 PM



Door 4-103
Added on:
Jan 5, 2024 3:33 PM
Added by:
Tablet1 Ramaker & Associates

B 4-103 Installed
Added on:
Jan 5, 2024 3:34 PM
Added by:
Tablet1 Ramaker & Associates

OPENING 4-102



Created:
tablet1@ramaker.com
Jan 5, 2024 3:32 PM

Last Updated:
tablet1@ramaker.com
Jan 5, 2024 3:33 PM



B 4-102 Installed

Added on:
Jan 5, 2024 3:33 PM

Added by:
Tablet1 Ramaker & Associates

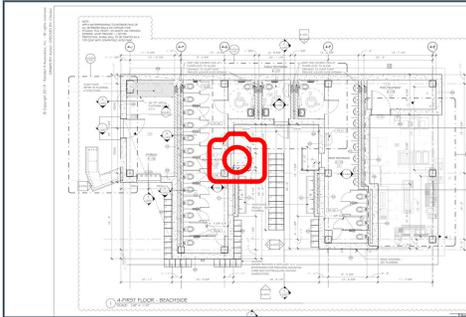


Door 4-102

Added on:
Jan 5, 2024 3:33 PM

Added by:
Tablet1 Ramaker & Associates

OPENING 4-101



Created:
tablet1@ramaker.com
Jan 5, 2024 3:32 PM

Last Updated:
tablet1@ramaker.com
Jan 5, 2024 3:32 PM



B 4-101 Installed

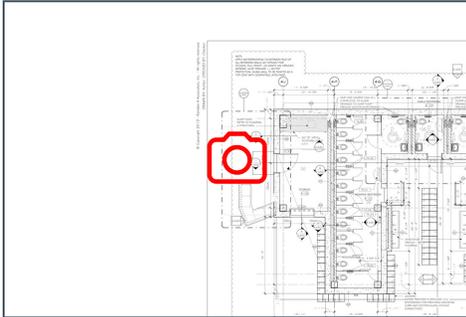
Added on:
Jan 5, 2024 3:32 PM
Added by:
Tablet1 Ramaker & Associates



Door 4-101

Added on:
Jan 5, 2024 3:32 PM
Added by:
Tablet1 Ramaker & Associates

DOOR 4-106A



Created:
tablet1@ramaker.com
Jan 5, 2024 3:31 PM

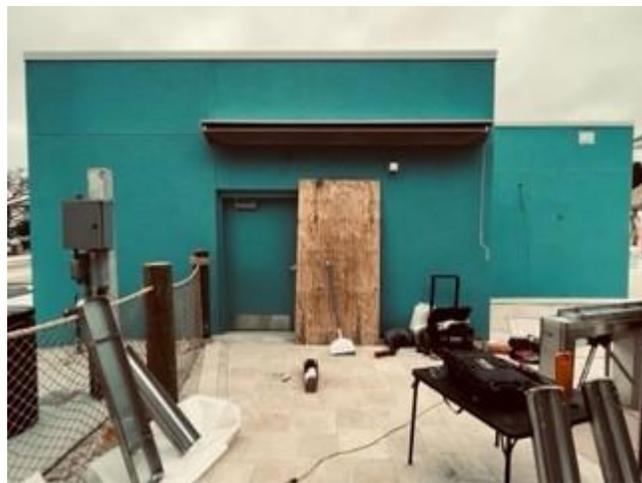
Last Updated:
tablet1@ramaker.com
Jan 5, 2024 3:31 PM



B 4-106A Installed

Added on:
Jan 5, 2024 3:31 PM

Added by:
Tablet1 Ramaker & Associates

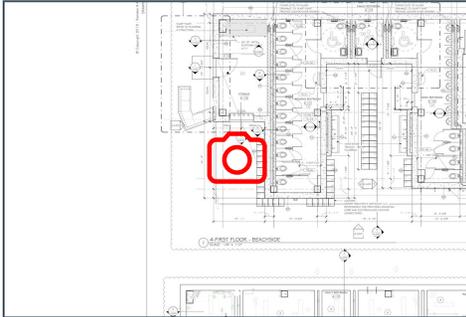


Door 4-106A

Added on:
Jan 5, 2024 3:31 PM

Added by:
Tablet1 Ramaker & Associates

FLOOD PANEL 4-106B



Created:
tablet1@ramaker.com
Jan 5, 2024 3:27 PM

Last Updated:
tablet1@ramaker.com
Jan 5, 2024 3:30 PM



B 4-106B Installed

Added on:
Jan 5, 2024 3:30 PM

Added by:
Tablet1 Ramaker & Associates

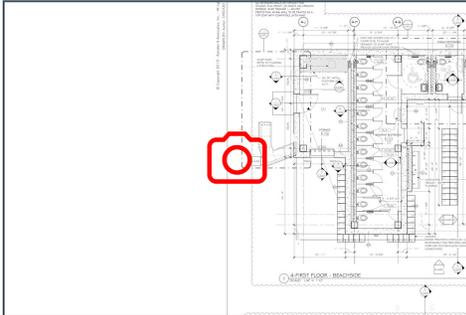


Opening 4-106B

Added on:
Jan 5, 2024 3:30 PM

Added by:
Tablet1 Ramaker & Associates

NORTH EXTERIOR



Created:
tablet1@ramaker.com
Jan 5, 2024 3:38 PM

Last Updated:
tablet1@ramaker.com
Jan 5, 2024 3:39 PM

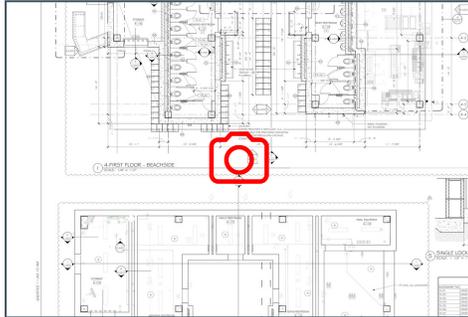


North side of Building

Added on:
Jan 5, 2024 3:39 PM

Added by:
Tablet1 Ramaker & Associates

EAST EXTERIOR



Created:
tablet1@ramaker.com
Jan 5, 2024 3:37 PM

Last Updated:
tablet1@ramaker.com
Jan 5, 2024 3:38 PM



East side (5) of Building
Added on:
Jan 5, 2024 3:38 PM
Added by:
Tablet1 Ramaker & Associates



East side (7) of Building
Added on:
Jan 5, 2024 3:38 PM
Added by:
Tablet1 Ramaker & Associates



East side (3) of Building

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Jan 5, 2024 3:38 PM

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Tablet1 Ramaker & Associates



East side (6) of Building

Added on:
Jan 5, 2024 3:38 PM

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East side (2) of Building

Added on:
Jan 5, 2024 3:38 PM

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East side (1) of Building

Added on:
Jan 5, 2024 3:38 PM

Added by:
Tablet1 Ramaker & Associates



East side (4) of Building

Added on:

Jan 5, 2024 3:38 PM

Added by:

Tablet1 Ramaker & Associates

Margaritaville Comprehensive Flood Emergency Operations Plan

Dry Floodproofing building 4 (Pool Building)

Emergency Organization Team:

- David Cesario – Resort Manager – Mobile 617-244-6165
- Ken DiLorenzo – Director of Engineering – Mobile 914-261-1157
- Frank Wood – Director of Security – Mobile 561-723-6144

Components for dry floodproofing of this building:

- Six opening (5 doorways and 1 window)
- Eleven panels - Each doorway has two panels; the window has one panel.
- One sump pump that operates on normal and battery backup power.
- No additional components

Equipment and tools needed.

- Eleven panels
- Cordless drill with a Slotted Sidewalk driver (9/16 * 3 5/8)

Installation of panels will occur:

- Within 8 hours of a tropical storm warning or hurricane watch notification.

Notification

- Notification will be given via the numbers of the Emergency Organization Team listed above.

Installation of panels; responsibility

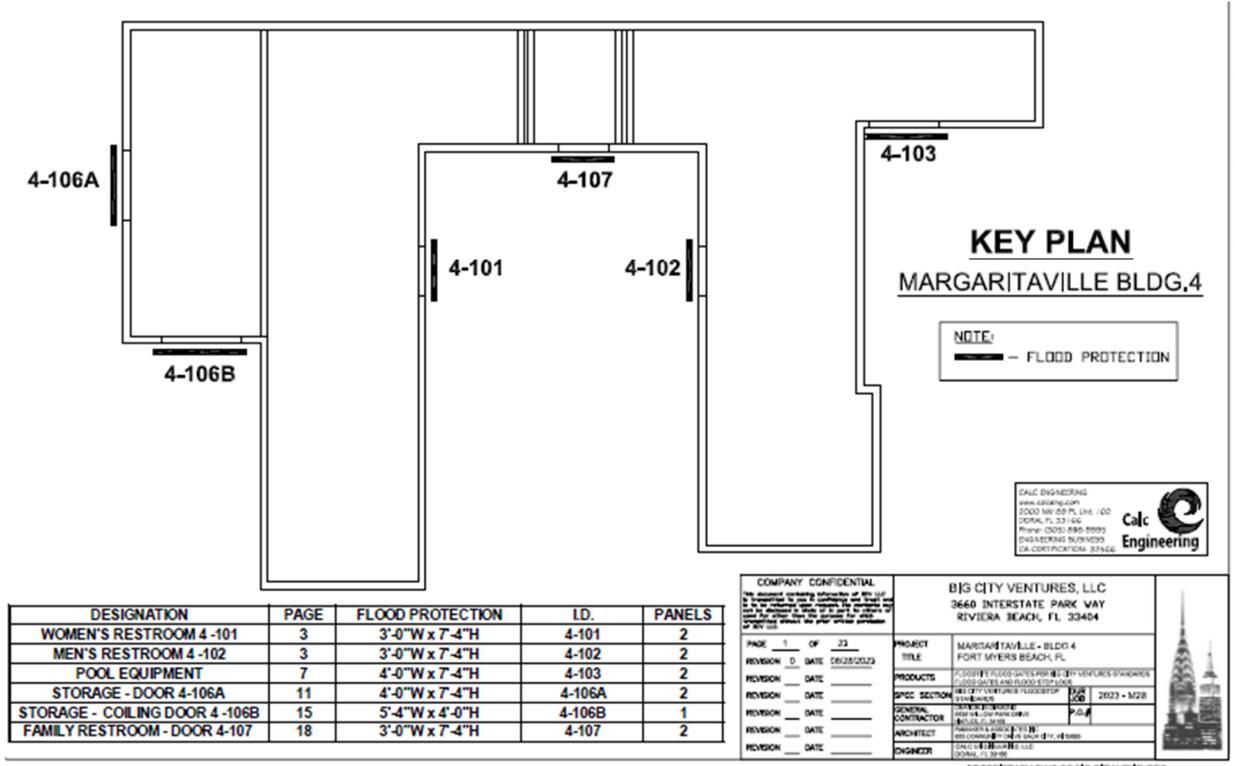
- The Director of Engineering will lead the installation.
 - Installation includes 5 doorways and 1 window panel.
 - DOE will direct personnel to install.
 - Bolts are in place and only require removal of screws, and placement of the panels.
 - Coreless drill with slotted sidewalk driver.

The decision tree is as follows; based on the timing above.

- David Cesario – Resort Manager – Mobile 617-244-6165
- Ken DiLorenzo – Director of Engineering – Mobile 914-261-1157
- Frank Wood – Director of Security – Mobile 561-723-6144

Location of the panels

- Panels will be stored in the building, the room with door labeled (4-106A)
- Coreless drill and Slotted Sidewalk bit are also stored in this room with the panels.



Power source requirements

- None needed.
- After the panels are installed, there is no internal access to the building.

Installations

- Each door requires two panels and a two-person team for installation.
- Two people will be designated for the installation as described above.

Evacuation

- Once the panels are installed the two-person crew leave the area and follow local evacuation procedures.

Training

- Training for the panel installation occurred at the initial installation on 1/2/24, and will be conducted annually.

Plan review

- This plan will be reviewed annually and adjusted as needed.

Margaritaville Comprehensive Inspection and Maintenance Plan

Dry Floodproofing building 4 (Pool Building)

Inspection and Maintenance Team:

- Ken DiLorenzo – Director of Engineering – Mobile 914-261-1157
- Frank Wood – Director of Security – Mobile 561-723-6144

Inspections

- Visual inspection of the building will occur daily by security and pool personnel.
 - Any visual deficiencies will be reported and addressed immediately.
- Monthly structural inspections will be conducted by the Team listed above. This includes structural, penetrations, foundation, walls, slabs, joints, etc.
 - Any deficiencies will be addressed as needed.
- Panel inspection will be conducted monthly and tested during training/installation of the panels.
 - This includes all seals/gaskets, fasteners, mounting hardware and tools.
- Sump pump inspection will be conducted monthly and tested.
 - This includes all testing of backup battery operation.

Sump Pumps

- There is one sump pump in this structure. It is a hybrid model that includes a battery backup to operate during permanent power loss.

Emergency Power

- There is no emergency power to this structure.

Location of panels and tools

- The location for the panels and tools is in the room labeled with door 4-106A. The panels have been evaluated and appropriately seal the openings.



TPI Hospitality | www.tpihospitality.com
103 15th Ave. NW, Suite 200 | Willmar, MN 56201

January 18, 2024

RE: TPI-FMB, LLC
1192 Estero Boulevard
Fort Myers Beach, FL 33931
Building #4
Parcel No. 19-46-24-W4-U0494.2609

To Whom It May Concern:

TPI-FMB, LLC, the building owner for the above referenced parcel, acknowledges that they are aware of the criteria for when the dry floodproofing measures must be installed and that they know how to install all the measures.

Sincerely,

A handwritten signature in black ink, appearing to read "T. Torgerson", with a long horizontal flourish extending to the right.

Thomas R. Torgerson
Manager, TPI-FMB, LLC



DEANGELIS DIAMOND

DeAngelis Diamond Construction HQ
6635 Willow Park Drive
Naples, Florida 34109
Phone: (239) 594-1994
Fax: (239) 594-1995

Submittal #10 7116-1.0 10 7116 - Storm Panels

Project: 21-037 - Margaritaville
1160 Estero Blvd
Fort Myers Beach, Florida 33931

Building 4 Storm Panels - SD

SPEC SECTION:	10 7116 - Storm Panels	SUBMITTAL MANAGER:	Drew Davis (DeAngelis Diamond Construction, LLC)
STATUS:	Open	DATE CREATED:	09/7/2023
ISSUE DATE:	09/7/2023	REVISION:	0
RESPONSIBLE CONTRACTOR:	Big City Ventures, LLC	RECEIVED FROM:	Mark Loeb
RECEIVED DATE:		SUBMIT BY:	
FINAL DUE DATE:	09/21/2023	LOCATION:	Building 4
TYPE:	Shop Drawing	COST CODE:	
APPROVERS:	Drew Davis (DeAngelis Diamond Construction, LLC), Kevin Hanson (Ramaker & Associates, Inc.), Jodi Kleist (Ramaker & Associates, Inc.)		

BALL IN COURT:
Kevin Hanson (Ramaker & Associates, Inc.), Jodi Kleist (Ramaker & Associates, Inc.)

DISTRIBUTION:
Zach Whiting (DeAngelis Diamond Construction, LLC) , Tom Torgerson (TPI-FMB, LLC) , Robert Kisabeth (TPI-FMB, LLC) , Max Tyler (DeAngelis Diamond Construction, LLC) , Kevin Hanson (Ramaker & Associates, Inc.) , Kathy Aamot (TPI-FMB, LLC) , Kameron Saffold (DeAngelis Diamond Construction, LLC) , Justin Oelke (DeAngelis Diamond Construction, LLC) , Joel Finley (TPI-FMB, LLC) , Jodi Kleist (Ramaker & Associates, Inc.) , Jeffery Miller (DeAngelis Diamond Construction, LLC) , Ingrid Arencibia (DeAngelis Diamond Construction, LLC) , Drew Davis (DeAngelis Diamond Construction, LLC) , Daniel Rohletter (DeAngelis Diamond Construction, LLC) , Chris Flagg (TPI-FMB, LLC) , Bailey Winfield (DeAngelis Diamond Construction, LLC)

DESCRIPTION:

ATTACHMENTS:

SUBMITTAL WORKFLOW

#	NAME	SUBMITTER/ APPROVER	SENT DATE	DUE DATE	RETURNED DATE	RESPONSE	ATTACHMENTS	COMMENTS
1	Mark Loeb	Submitter		9/14/2023	9/7/2023	Submitted	MARGARITAVILLE_BLDG4_REV.0.pdf	
2	Drew Davis	Approver	9/7/2023	9/12/2023	9/7/2023	Approved	MARGARITAVILLE_BLDG4_REV.0.pdf	
3	Kevin Hanson	Approver	9/7/2023	9/21/2023		Pending		
4	Jodi Kleist	Approver	9/7/2023	9/21/2023		Pending		

BY _____ DATE _____ COPIES TO _____

21-037 - Margaritaville



DEANGELIS DIAMOND

1160 Estero Blvd
Fort Myers Beach, Florida 33931
United States

DeAngelis Diamond Construction HQ
6635 Willow Park Drive
Naples, Florida 34109
United States
(239) 594-1994

Title

Building 4 Storm Panels - SD

Submittal Manager

Drew Davis

Spec Section

10 7116 - Storm Panels

Type

Shop Drawing

Number

10 7116-1

Rev

0

Description

None



Reviewed

If Reviewed or Reviewed as Noted above, fabrication may be undertaken. This DOES NOT authorize changes in Contract Sum unless stated in separate letter or Change Order. If Rejected of Revise & Resubmit above, fabrication MAY NOT be undertaken. Resubmit corrected copies for final review. Correction shall be limited to items marked.

Reviewing is only for conformance with the design concept of the project. The contractor is responsible for compliance with the information given in the Contract Documents and for dimensions to be confirmed and correlated at the site for information that pertains solely to the fabrication processes or to the means, methods, techniques, sequences, and procedures of construction, and for coordination of the Work of all trades.

BY: khanson DATE: 09/07/2023

855 Community Dr. Sauk City, WI 53583 | 1-800-332-7532

**ALL DIMENSIONS SUBJECT TO FIELD VERIFICATION.
KMH/09-07-23**



Reviewed by DeAngelis Diamond Construction, LLC. in accordance with the Contract. Review and approval of this submittal does not relieve the subcontractor from its obligation to perform all Work in accordance with the Subcontract and compliance with the requirements of the Contract Documents.

Job # 21-037 Margaritaville Fort Myers Beach

Submittal 10 7116-1.0 Building 4 Flood Panels - SD

Approved 09-07-23

DD

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PAGE <u>0</u>	OF <u>23</u>	PROJECT TITLE	MARGARITAVILLE - BLDG 4 FORT MYERS BEACH, FL	
REVISION <u>0</u>	DATE <u>08/28/2023</u>	PRODUCTS	FLOODTITE FLOOD GATES PER BIG CITY VENTURES STANDARDS FLOOD GATES AND FLOOD STOP LOGS	
REVISION _____	DATE _____	SPEC SECTION	BIG CITY VENTURES FLOODSTOP STANDARDS	
REVISION _____	DATE _____	GENERAL CONTRACTOR	DEANGELIS DIAMOND 6635 WILLOW PARK DRIVE NAPLES, FL 34109	
REVISION _____	DATE _____	ARCHITECT	RAMAKER & ASSOCIATES INC 855 COMMUNITY DRIVE SAUK CITY, WI 53583	
REVISION _____	DATE _____	ENGINEER	CALC ENGINEERING, LLC DORAL, FL 33166	
		OUR JOB	2023 - M28	
		P.O.#		

<p>CALC ENGINEERING www.calceng.com 2000 NW 89 PL Unit 102 DORAL FL 33166 Phone: (305) 898-9995 ENGINEERING BUSINESS CA CERTIFICATION: 32566</p>	 Calc Engineering
--	--

4-106A

4-106B

4-101

4-107

4-102

4-103

KEY PLAN

MARGARITAVILLE BLDG.4

NOTE:
 — FLOOD PROTECTION

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DESIGNATION	PAGE	FLOOD PROTECTION	I.D.	PANELS
WOMEN'S RESTROOM 4 -101	3	3'-0"W x 7'-4"H	4-101	2
MEN'S RESTROOM 4 -102	3	3'-0"W x 7'-4"H	4-102	2
POOL EQUIPMENT	7	4'-0"W x 7'-4"H	4-103	2
STORAGE - DOOR 4-106A	11	4'-0"W x 7'-4"H	4-106A	2
STORAGE - COILING DOOR 4 -106B	15	5'-4"W x 4'-0"H	4-106B	1
FAMILY RESTROOM - DOOR 4-107	18	3'-0"W x 7'-4"H	4-107	2

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			OUR JOB 2023 - M28 P.O.#



BILL OF MATERIALS FOR STOPLOG

PART #	QUANTITY	PART DESCRIPTION	MATERIAL	COMMENTS
GATE				
1		GATE / BARRIER PANEL		
1A	1	PANEL	5052 H32	1/4" PLATE (SEE PANEL DWGS.)
1G	AS SHOWN	VERTICAL STIFFENER	ALM 6061-T6	2"x2"x1/4" TUBE
1G-1	AS SHOWN	VERTICAL STIFFENER	ALM 6061-T6	4"x2"x1/4" TUBE
1H	AS SHOWN	HORIZONTAL STIFFENER	ALM 6061-T6	2"x2"x1/4" TUBE
FRAME & FRAME COMPONENTS				
4B	AS SHOWN	ISOLATION GASKET	RUBBER/EPDM	1/4" THK.
4C	AS SHOWN	COMPRESSION GASKET	SOFT DURO ADHESIVE	1/2" x 2"
5A	3/8" DIA.DROP-IN EXPANSION ANCHOR (SEE PAGE 23)			
5B	1/2" DIA.LDT R-59 ANCHOR (SEE PAGE 22)			
5C	3/8" DIA.DROP-IN EXPANSION ANCHOR (SEE PAGE 22)			

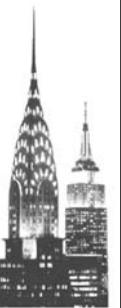
NOTES:

- 1: MATERIAL :** PER TABLE
- 2. PRESSURE:** TO FULL HEIGHT FROM ONE DIRECTION AS SHOWN ON PLAN
- 3. FINISH :** MILL FINISH
- 4: SWING:** N/A
- 5: OTHERS**
 - 1. REMOVE ALL WELD SPATTER PRIOR TO FINAL FINISH.
 - 2. CLEAN ALL EXCESS PAINT OR GALVANIZING.
- 6: SKID AND PACK IN ACCORDANCE WITH COMMERCIAL SHIPPING PRACTICES.**
- 7: APPLY APPROPRIATE PRIMER AS PER SPECS (BY INSTALLER) ON ALL METAL FRAME SURFACES IN CONTACT WITH CONCRETE**
- 8: PROVIDE 1 YEARS WARRANTY AGAINST DEFECTS IN MATERIAL & WORKMANSHIP**

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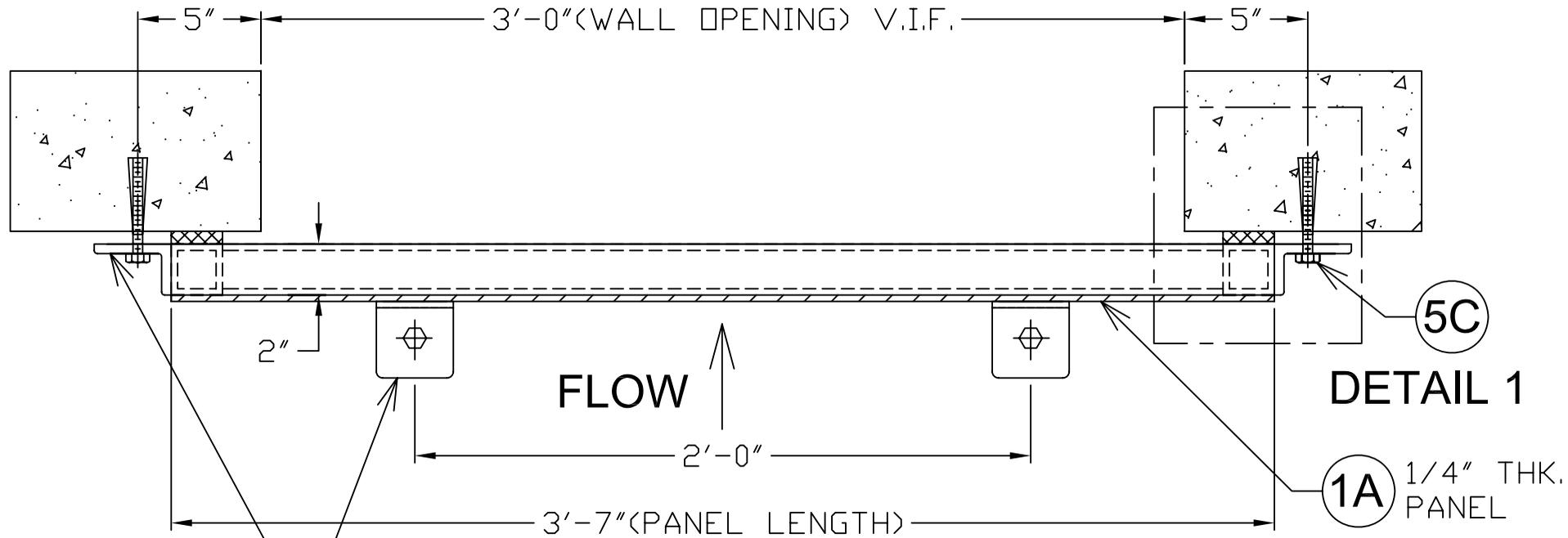


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		P.O.#	



PROPRIETARY DWG OF BIG CITY VENTURES

PROPRIETARY DWG OF BIG CITY VENTURES



TAB:
3/8" x 2" x 3" ANGLE
ALUM 6061-T6 (TYP)

**FACE MOUNTED
FLOOD PROTECTION BARRIERS ASSY**

@ WOMEN'S RESTROOM 4 -101 & MEN'S RESTROOM 4 -102

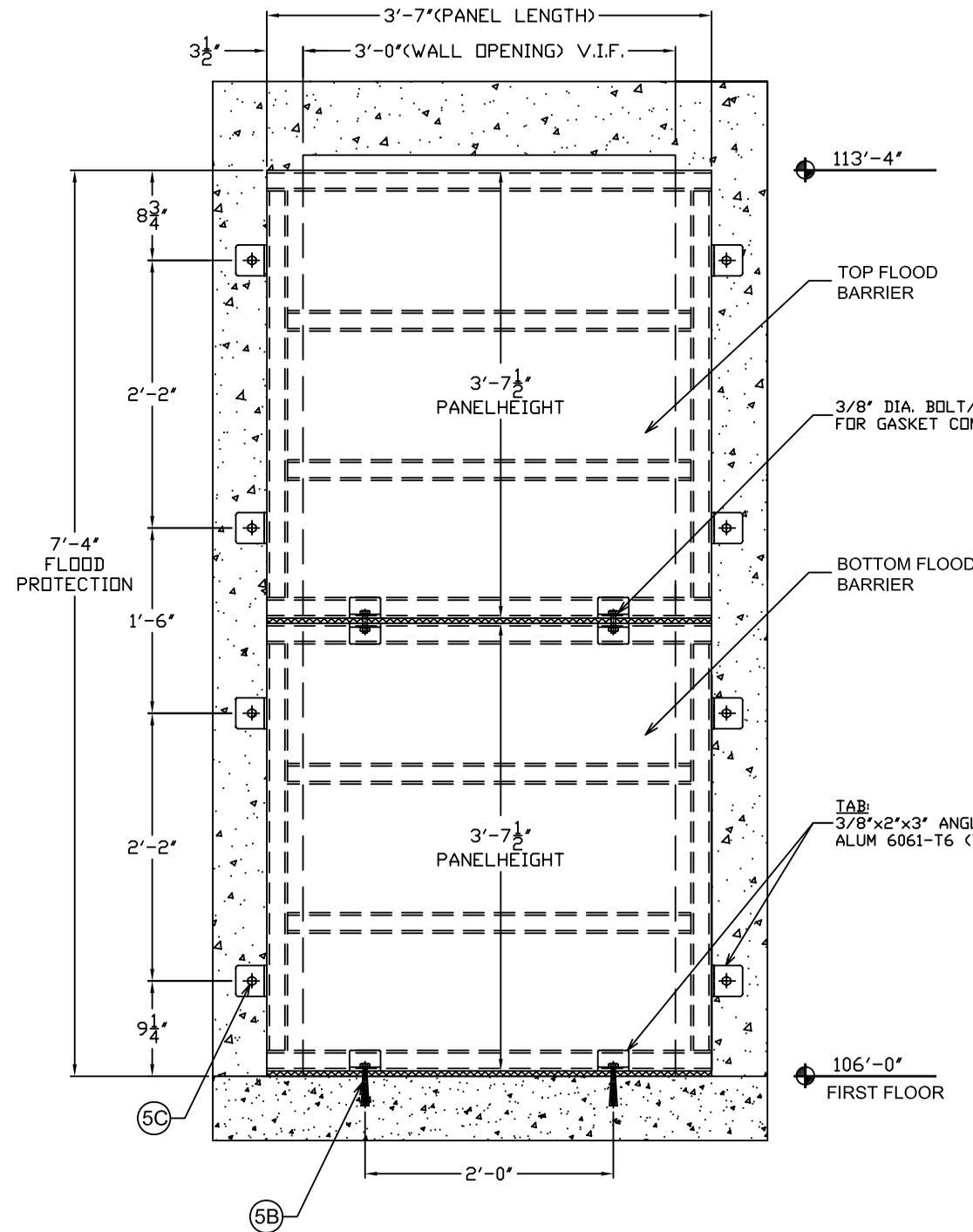
**(TYP OF 2)
(3'-0" x 7'-4")
PLAN VIEW**

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		P.O.#	





**FACE MOUNTED
FLOOD PROTECTION BARRIERS ASSY
@ 4-101 & 4-102 (TYP OF 2)
(3'-0" x 7'-4")
FRONT VIEW**

TOP FLOOD BARRIER

3/8" DIA. BOLT/NUT FOR GASKET COMPRESSION

BOTTOM FLOOD BARRIER

TAB:
3/8"x2"x3" ANGLE
ALUM 6061-T6 (TYP)

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BIG CITY VENTURES, LLC
3660 INTERSTATE PARK WAY
RIVIERA BEACH, FL 33404

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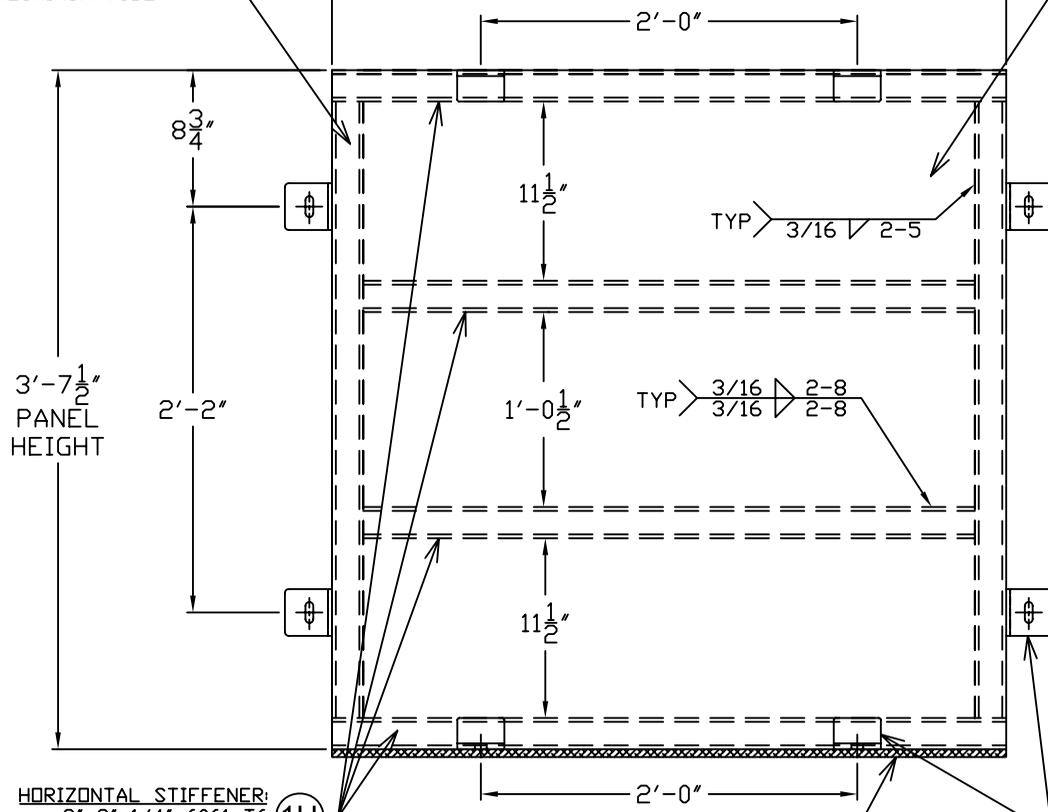


VERTICAL STIFFENER:
2"x2"x1/4" 6061-T6
ALUMINUM TUBE

1G

3'-7" (PANEL LENGTH)

1A PANEL:
1/4" BENT PLATE



HORIZONTAL STIFFENER:
2"x2"x1/4" 6061-T6
ALUMINUM TUBE

1H

2"W x 1/2" THK. SOFT DURD
ADHESIVE GASKET ATTACHED TO
SIDE TUBES AND ON BOTTOM
HORIZONTAL TUBE AS SHOWN

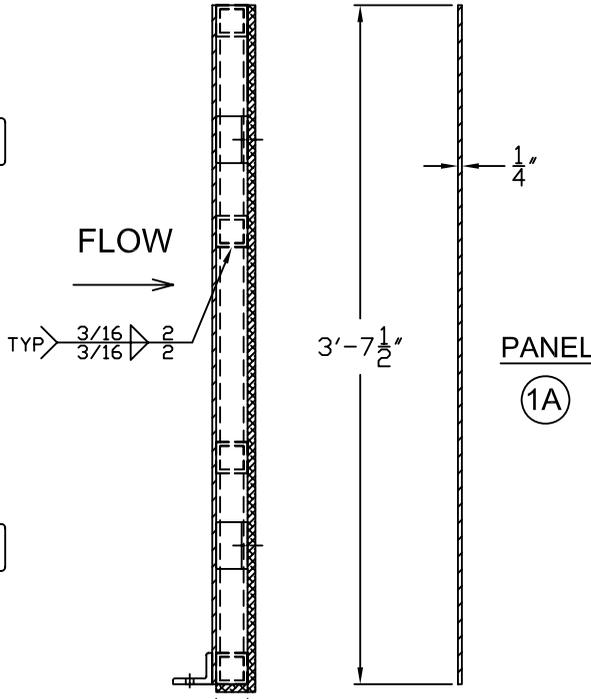
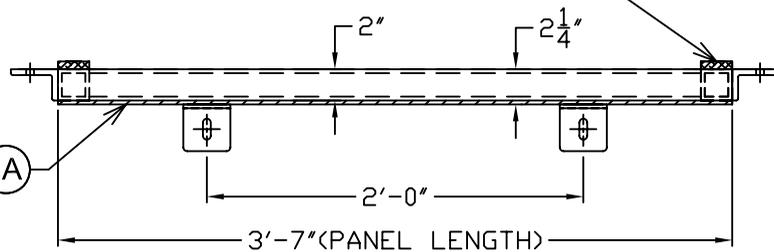
4C

TAB:
3/8"x2"x3" ANGLE
ALUM 6061-T6 (TYP)

BOTTOM FLOOD BARRIER
(TYP OF 2)

PANEL:
1/4" BENT PLATE

1A



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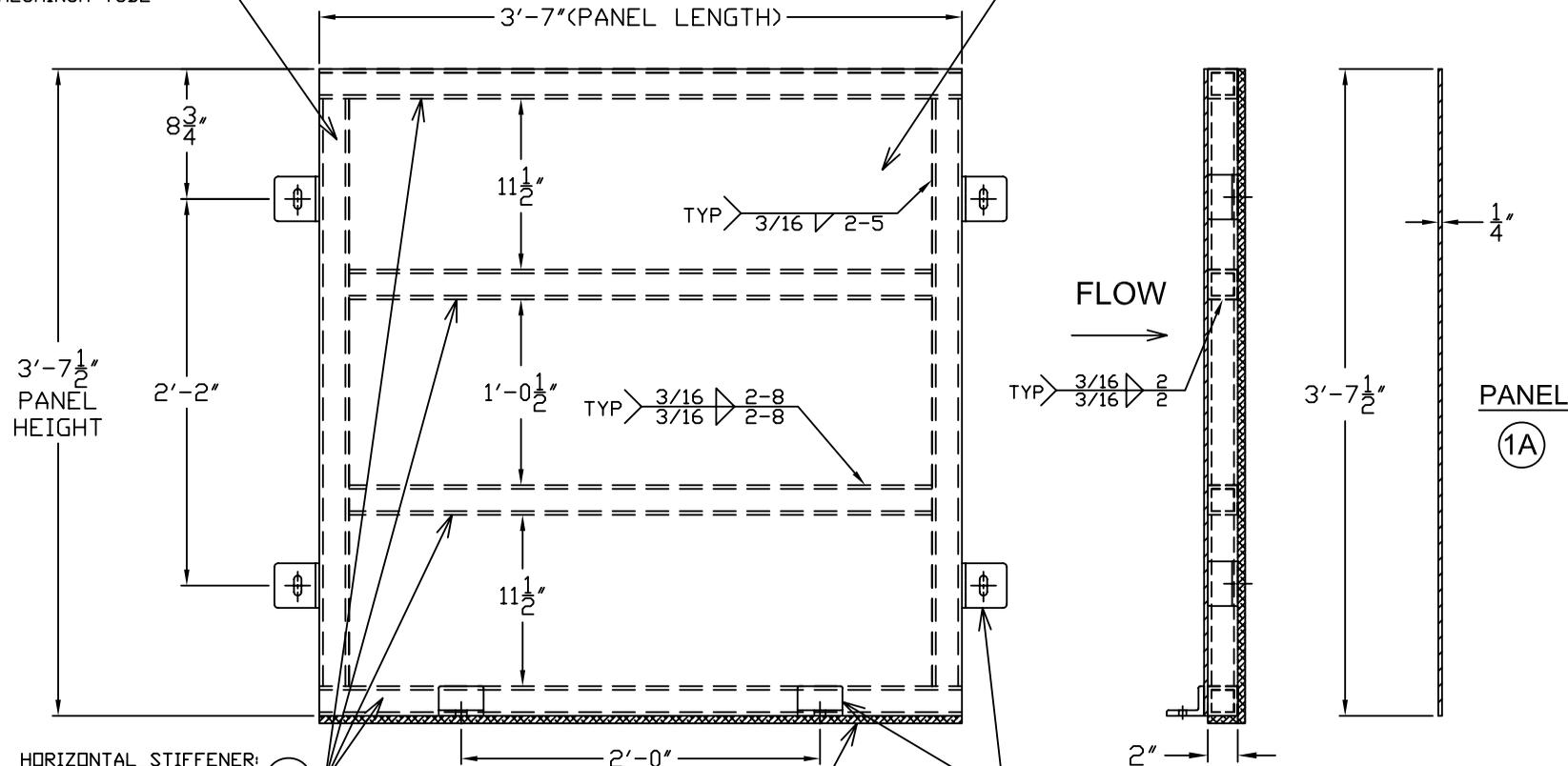


PROPRIETARY DWG OF BIG CITY VENTURES

PROPRIETARY DWG OF BIG CITY VENTURES

VERTICAL STIFFENER:
2"x2"x1/4" 6061-T6
ALUMINUM TUBE (1G)

PANEL:
1/4" BENT PLATE (1A)

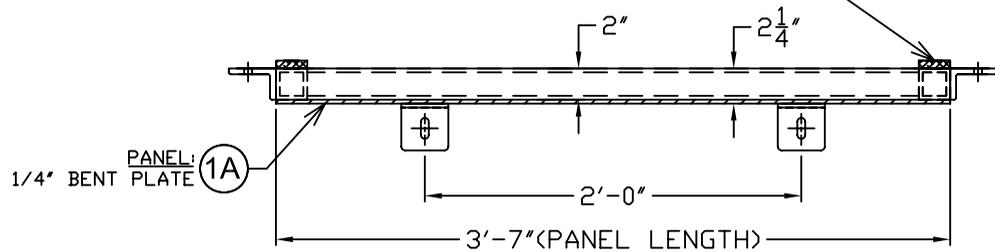


HORIZONTAL STIFFENER:
2"x2"x1/4" 6061-T6
ALUMINUM TUBE (1H)

TAB:
3/8"x2"x3" ANGLE
ALUM 6061-T6 (TYP)

2" x 1/2" THK. SOFT DURD
ADHESIVE GASKET ATTACHED TO
SIDE TUBES AND ON BOTTOM
HORIZONTAL TUBE AS SHOWN (4C)

TOP FLOOD BARRIER
(TYP OF 2)



PANEL:
1/4" BENT PLATE (1A)

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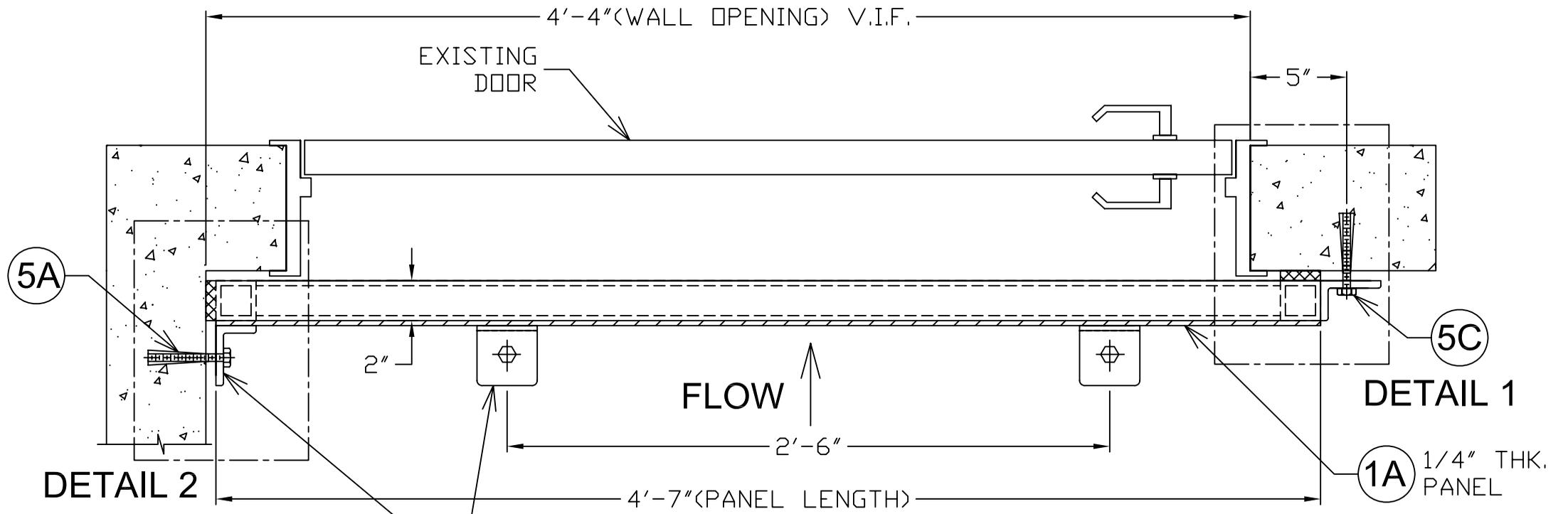
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BIG CITY VENTURES, LLC 3660 INTERSTATE PARK WAY RIVIERA BEACH, FL 33404			
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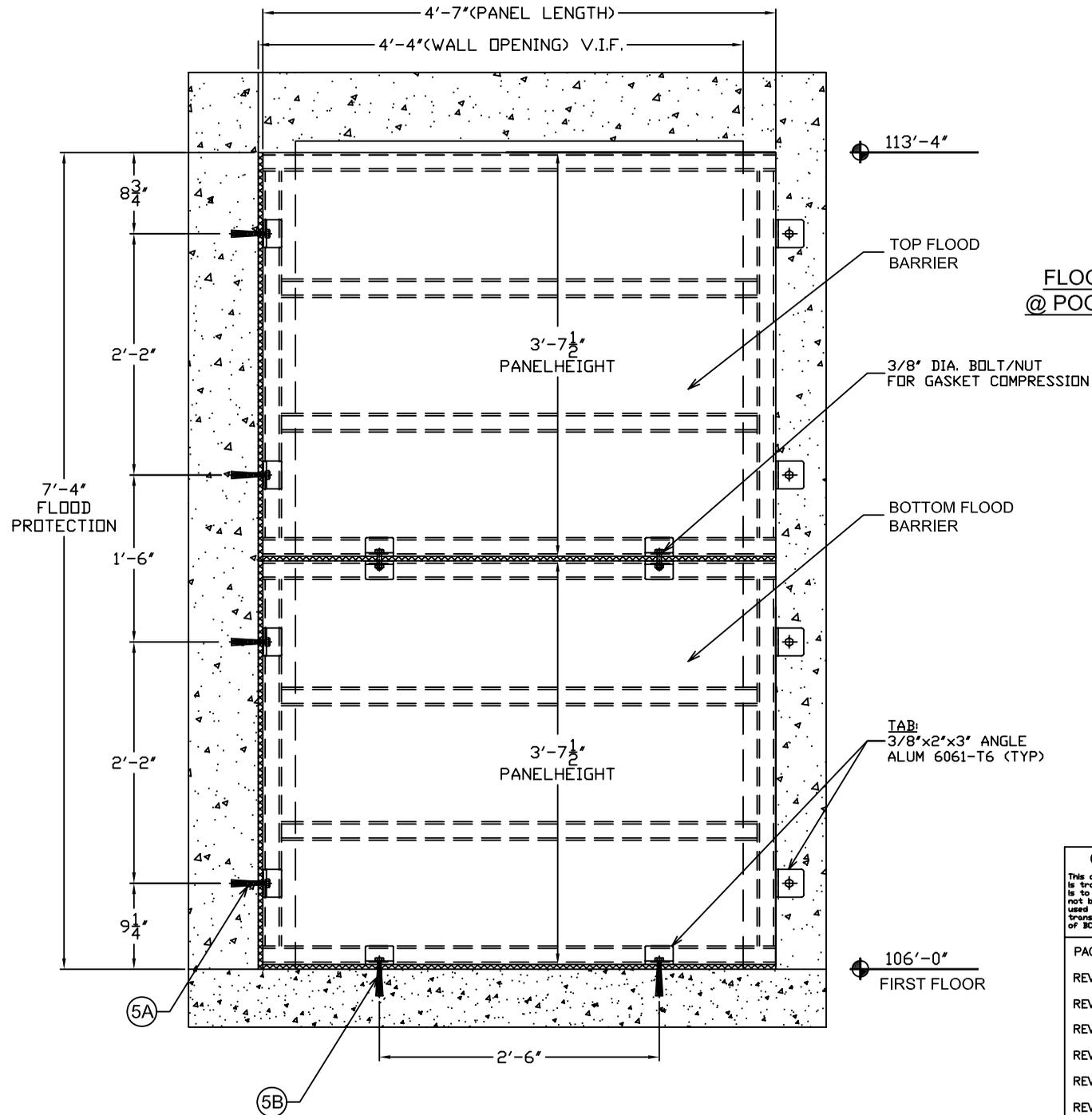
TAB:
3/8"x2"x3" ANGLE
ALUM 6061-T6 (TYP)

**FACE MOUNTED
FLOOD PROTECTION BARRIERS ASSY.
@ POOL EQUIP. DOOR 4 -103 (ONE EACH)
(4'-0" x 7'-4")
PLAN VIEW**

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REVISION DATE	ENGINEER	CALC ENGINEERING, LLC DORAL, FL 33166		



**FACE MOUNTED
FLOOD PROTECTION BARRIERS ASSY.
@ POOL EQUIP. DOOR 4 -103 (ONE EACH)
(4'-0" x 7'-4")
FRONT VIEW**

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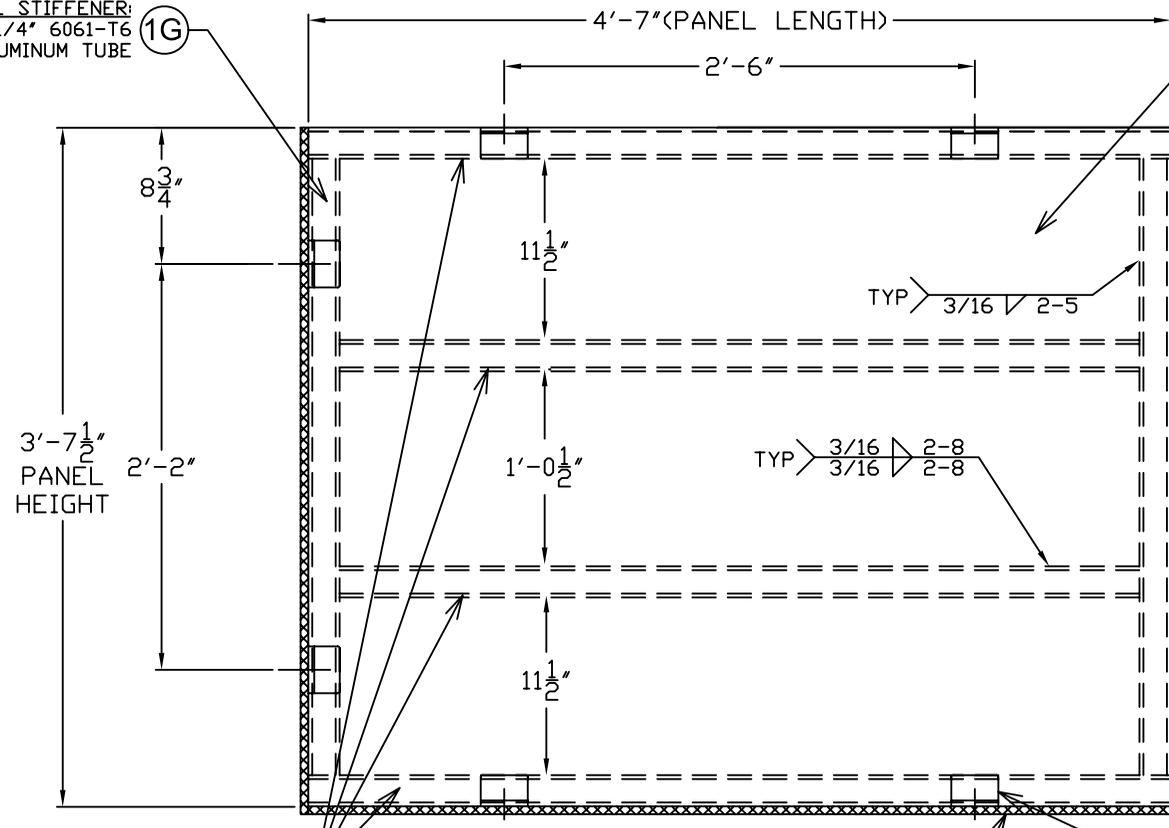


PROPRIETARY DWG OF BIG CITY VENTURES

PROPRIETARY DWG OF BIG CITY VENTURES

VERTICAL STIFFENER:
2"x2"x1/4" 6061-T6
ALUMINUM TUBE

1G



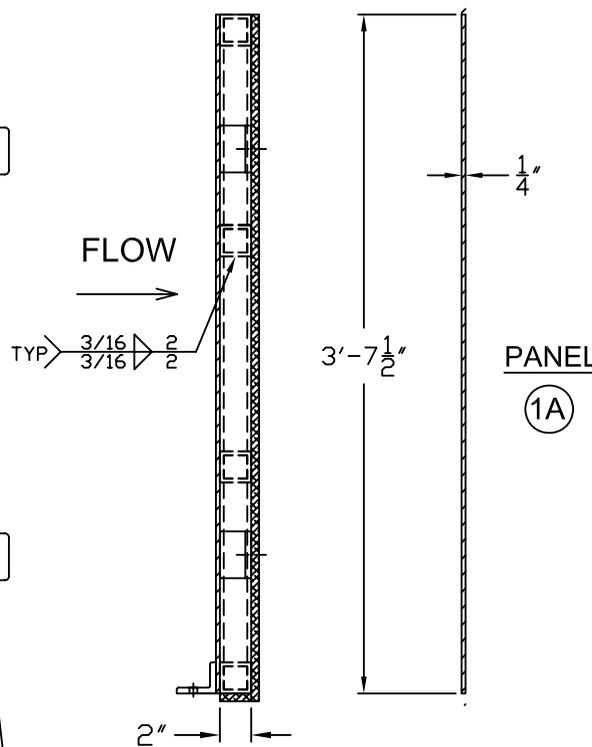
HORIZONTAL STIFFENER:
2"x2"x1/4" 6061-T6
ALUMINUM TUBE

1H

2"W x 1/2" THK, SOFT DURD
ADHESIVE GASKET ATTACHED TO
SIDE TUBES AND ON BOTTOM
HORIZONTAL TUBE AS SHOWN

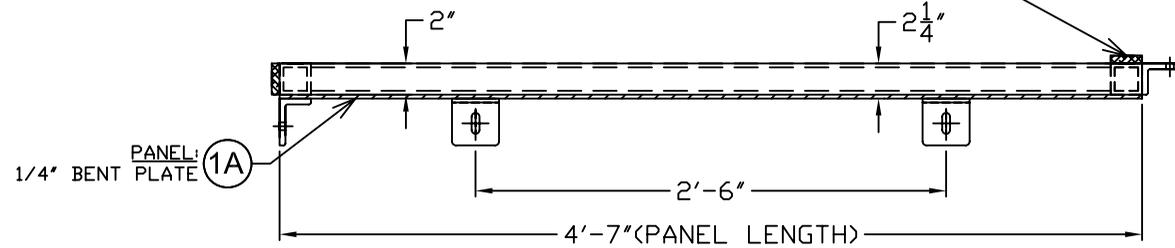
4C

1A PANEL:
1/4" BENT PLATE



TAB:
3/8"x2"x3"
ALUM 6061-T6 (TYP)

**BOTTOM FLOOD BARRIER
(ONE EACH)**



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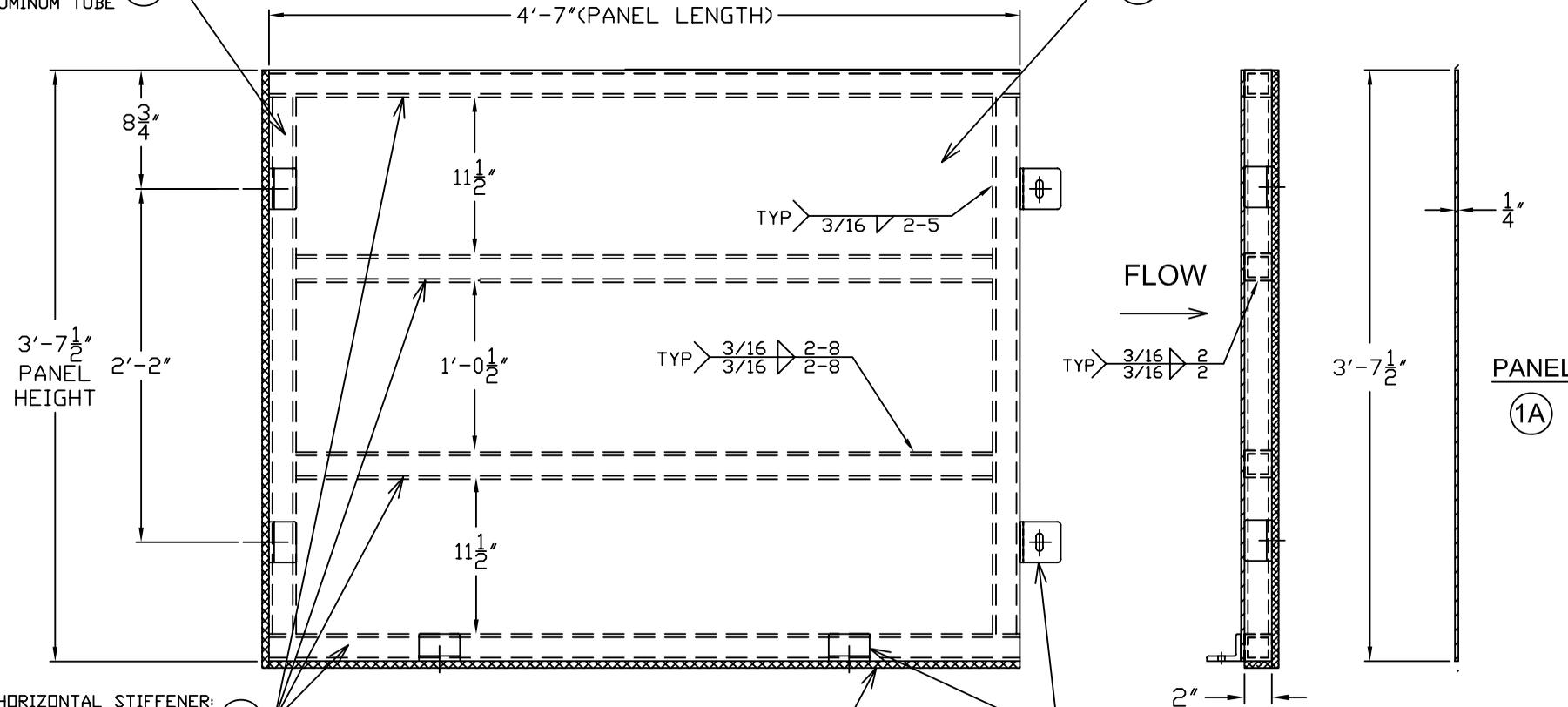


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VERTICAL STIFFENER:
2"x2"x1/4" 6061-T6
ALUMINUM TUBE (1G)

(1A) PANEL:
1/4" BENT PLATE

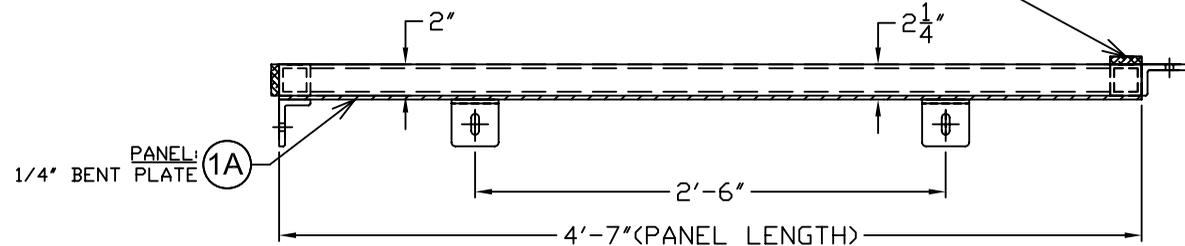


HORIZONTAL STIFFENER:
2"x2"x1/4" 6061-T6
ALUMINUM TUBE (1H)

TAB:
3/8"x2"x3" ANGLE
ALUM 6061-T6 (TYP)

2"W x 1/2" THK. SOFT DURD
ADHESIVE GASKET ATTACHED TO
SIDE TUBES AND ON BOTTOM
HORIZONTAL TUBE AS SHOWN (4C)

**TOP FLOOD BARRIER
(ONE EACH)**



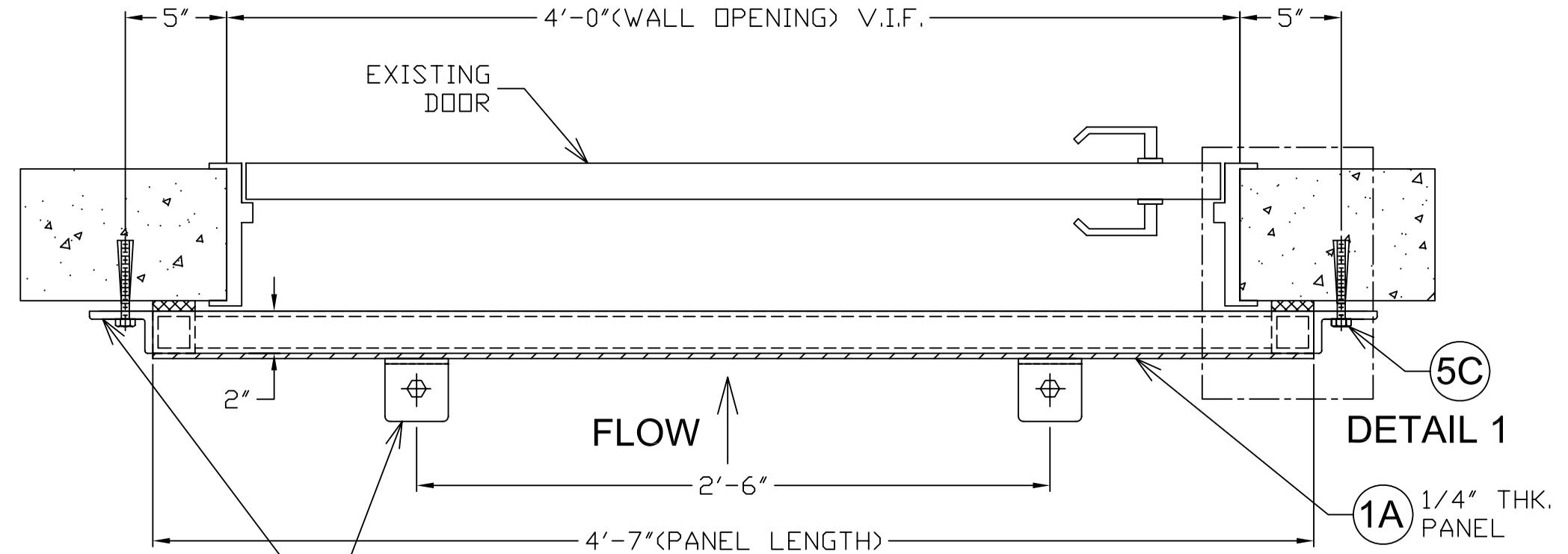
PANEL:
1/4" BENT PLATE (1A)

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REVISION 0 DATE 08/28/2023	PROJECT TITLE MARGARITAVILLE - BLDG 4 FORT MYERS BEACH, FL	PRODUCTS FLOODTITE FLOOD GATES PER BIG CITY VENTURES STANDARDS FLOOD GATES AND FLOOD STOP LOGS	
REVISION DATE	SPEC SECTION BIG CITY VENTURES FLOODSTOP STANDARDS	OUR JOB 2023 - M28	P.O.#
REVISION DATE	GENERAL CONTRACTOR DEANGELIS DIAMOND 6635 WILLOW PARK DRIVE NAPLES, FL 34109	ARCHITECT RAMAKER & ASSOCIATES INC 855 COMMUNITY DRIVE SAUK CITY, WI 53583	
REVISION DATE	ENGINEER CALC ENGINEERING, LLC DORAL, FL 33166	ENGINEER	





TAB:
3/8" x 2" x 3" ANGLE
ALUM 6061-T6 (TYP)

**FACE MOUNTED
FLOOD PROTECTION BARRIERS ASSY.
@ STORAGE DOOR 4 -106A (ONE EACH)
(4'-0" x 7'-4")
PLAN VIEW**

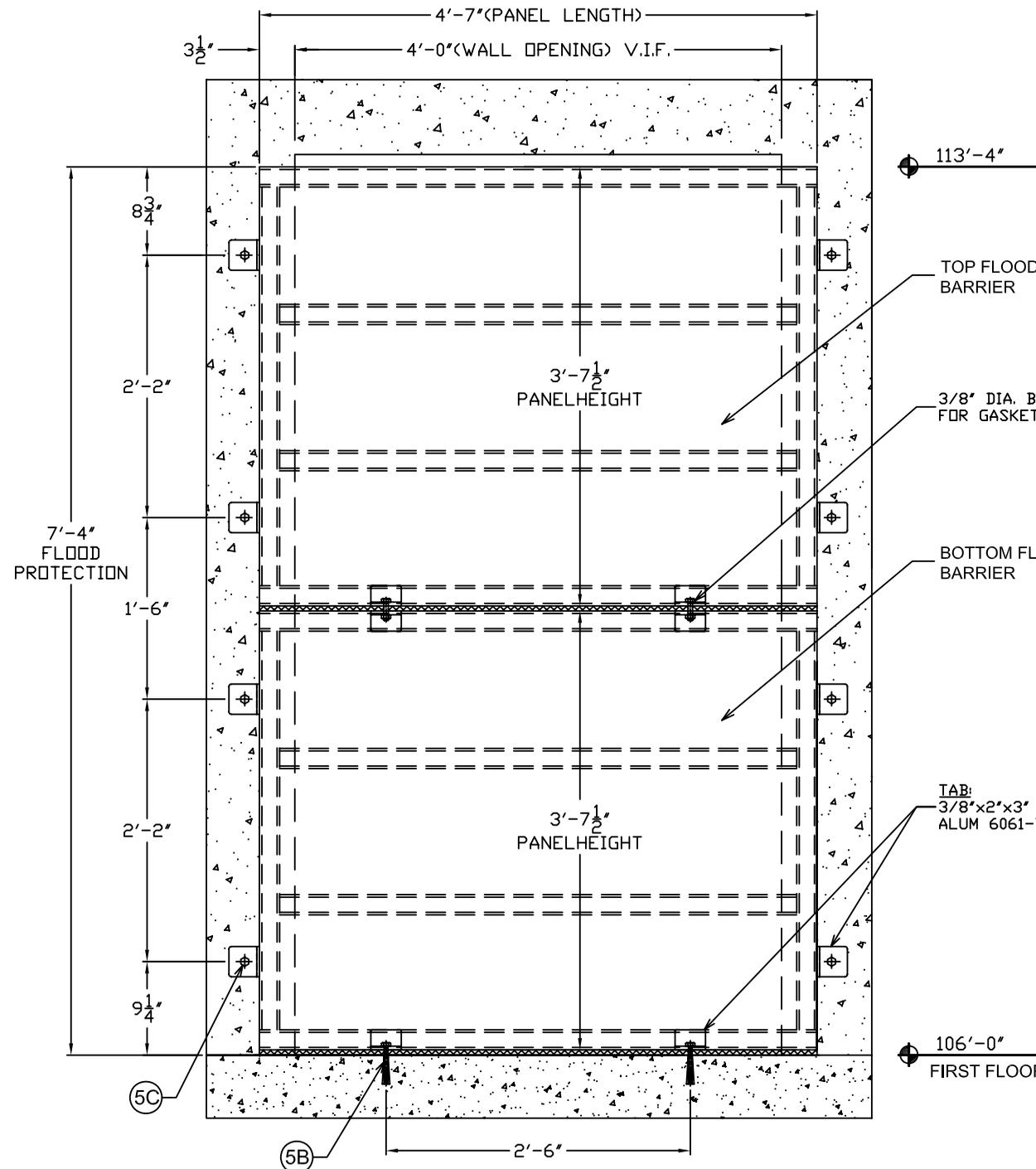
CALC ENGINEERING
 www.calceng.com
 2000 NW 89 PL Unit 102
 DORAL FL 33166
 Phone: (305) 898-9995
 ENGINEERING BUSINESS
 CA CERTIFICATION: 32566



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PAGE 11 OF 23 REVISION 0 DATE 08/28/2023 REVISION DATE REVISION DATE REVISION DATE REVISION DATE REVISION DATE	PROJECT TITLE MARGARITAVILLE - BLDG 4 FORT MYERS BEACH, FL	PRODUCTS FLOODTITE FLOOD GATES PER BIG CITY VENTURES STANDARDS FLOOD GATES AND FLOOD STOP LOGS	SPEC SECTION BIG CITY VENTURES FLOODSTOP STANDARDS
GENERAL CONTRACTOR DEANGELIS DIAMOND 6635 WILLOW PARK DRIVE NAPLES, FL 34109	OUR JOB 2023 - M28	P.O.#	ARCHITECT RAMAKER & ASSOCIATES INC 855 COMMUNITY DRIVE SAUK CITY, WI 53583
ENGINEER CALC ENGINEERING, LLC DORAL, FL 33166			

PROPRIETARY DWG OF BIG CITY VENTURES

PROPRIETARY DWG OF BIG CITY VENTURES



**FACE MOUNTED
FLOOD PROTECTION BARRIERS ASSY.
@ DOOR 4 -106A (ONE EACH)
(4'-0" x 7'-4")
FRONT VIEW**

TAB:
3/8" x 2" x 3" ANGLE
ALUM 6061-T6 (TYP)

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PAGE	12	OF	23
REVISION	0	DATE	08/28/2023
REVISION	—	DATE	—
REVISION	—	DATE	—
REVISION	—	DATE	—
REVISION	—	DATE	—
REVISION	—	DATE	—

BIG CITY VENTURES, LLC 3660 INTERSTATE PARK WAY RIVIERA BEACH, FL 33404	
PROJECT TITLE	MARGARITAVILLE - BLDG 4 FORT MYERS BEACH, FL
PRODUCTS	FLOODTITE FLOOD GATES PER BIG CITY VENTURES STANDARDS FLOOD GATES AND FLOOD STOP LOGS
SPEC SECTION	BIG CITY VENTURES FLOODSTOP STANDARDS
GENERAL CONTRACTOR	DEANGELIS DIAMOND 6635 WILLOW PARK DRIVE NAPLES, FL 34109
ARCHITECT	RAMAKER & ASSOCIATES INC 855 COMMUNITY DRIVE SAUK CITY, WI 53583
ENGINEER	CALC ENGINEERING, LLC DORAL, FL 33166



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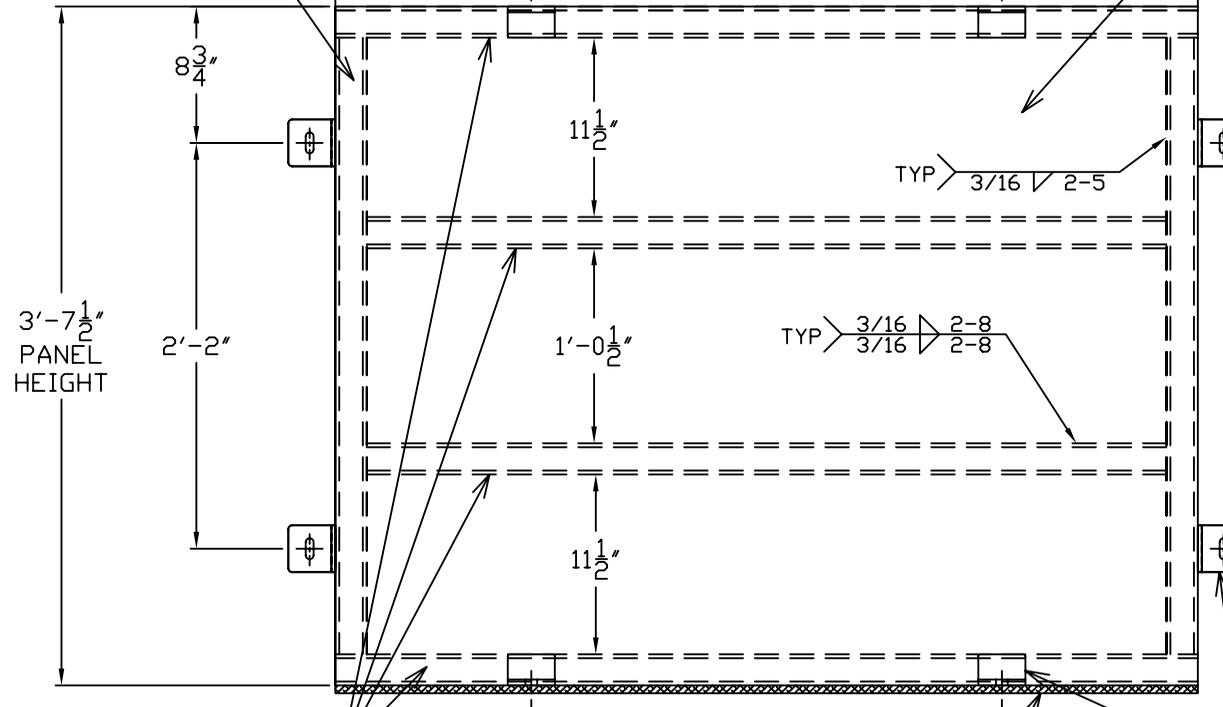
PROPRIETARY DWG OF BIG CITY VENTURES

VERTICAL STIFFENER:
2"x2"x1/4" 6061-T6
ALUMINUM TUBE

1G

4'-7" (PANEL LENGTH)

1A PANEL:
1/4" BENT PLATE



HORIZONTAL STIFFENER:
2"x2"x1/4" 6061-T6
ALUMINUM TUBE

1H

2"W x 1/2" THK. SOFT DURD
ADHESIVE GASKET ATTACHED TO
SIDE TUBES AND ON BOTTOM
HORIZONTAL TUBE AS SHOWN

4C

TAB:
3/8"x2"x3" ANGLE
ALUM 6061-T6 (TYP)

**BOTTOM FLOOD BARRIER
(ONE EACH)**

FLOW

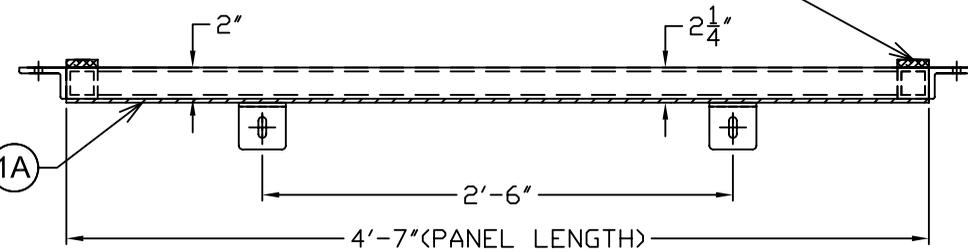


TYP > 3/16 > 2-5
TYP > 3/16 > 2-8
TYP > 3/16 > 2

3'-7 1/2"

PANEL
1A

1A



PANEL:
1/4" BENT PLATE

1A

4'-7" (PANEL LENGTH)

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BIG CITY VENTURES, LLC
3660 INTERSTATE PARK WAY
RIVIERA BEACH, FL 33404

PAGE	13	OF	23
REVISION	0	DATE	08/28/2023
REVISION		DATE	

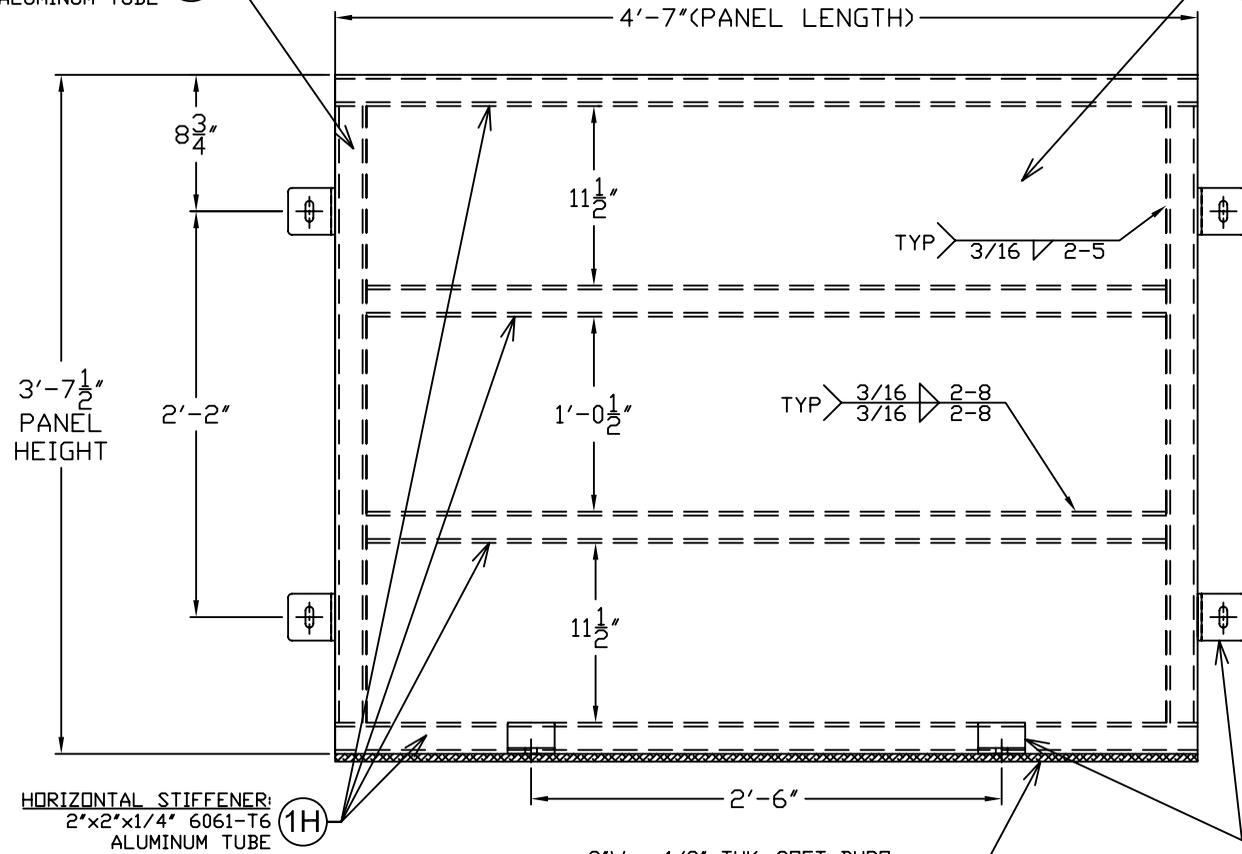
PROJECT TITLE	MARGARITAVILLE - BLDG 4 FORT MYERS BEACH, FL		
PRODUCTS	FLOODTITE FLOOD GATES PER BIG CITY VENTURES STANDARDS FLOOD GATES AND FLOOD STOP LOGS		
SPEC SECTION	BIG CITY VENTURES FLOODSTOP STANDARDS	OUR JOB	2023 - M28
GENERAL CONTRACTOR	DEANGELIS DIAMOND 6635 WILLOW PARK DRIVE NAPLES, FL 34109	P.O.#	
ARCHITECT	RAMAKER & ASSOCIATES INC 855 COMMUNITY DRIVE SAUK CITY, WI 53583		
ENGINEER	CALC ENGINEERING, LLC DORAL, FL 33166		



VERTICAL STIFFENER:
2"x2"x1/4" 6061-T6
ALUMINUM TUBE

1G

1A PANEL:
1/4" BENT PLATE



HORIZONTAL STIFFENER:
2"x2"x1/4" 6061-T6
ALUMINUM TUBE

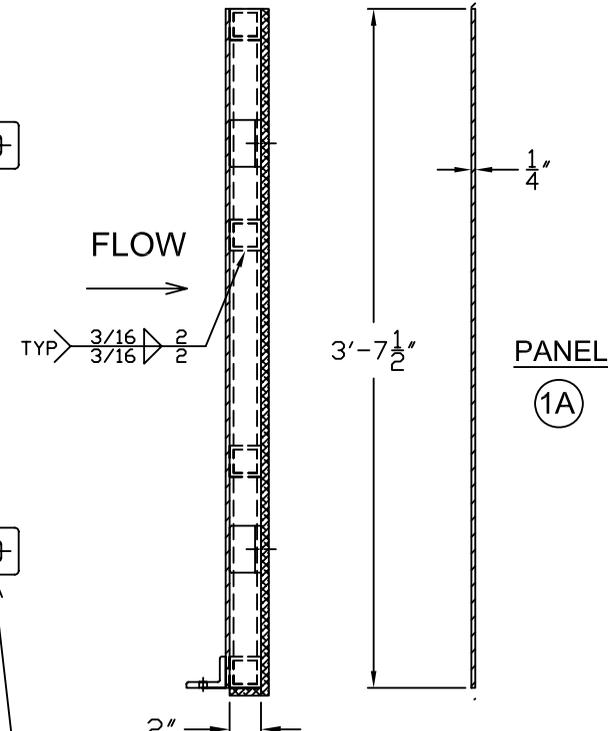
1H

2"W x 1/2" THK. SOFT DURD
ADHESIVE GASKET ATTACHED TO
SIDE TUBES AND ON BOTTOM
HORIZONTAL TUBE AS SHOWN

4C

TAB:
3/8"x2"x3" ANGLE
ALUM 6061-T6 (TYP)

TOP FLOOD BARRIER
(ONE EACH)



PANEL
1A

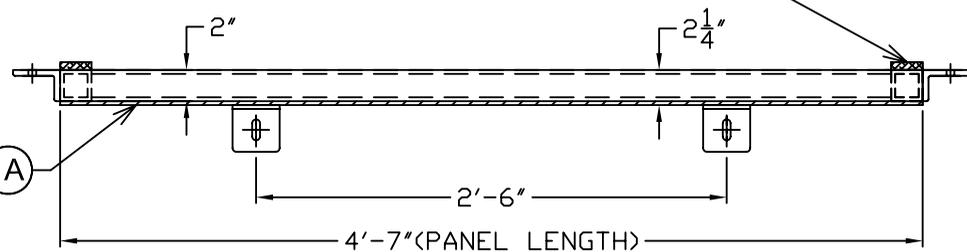
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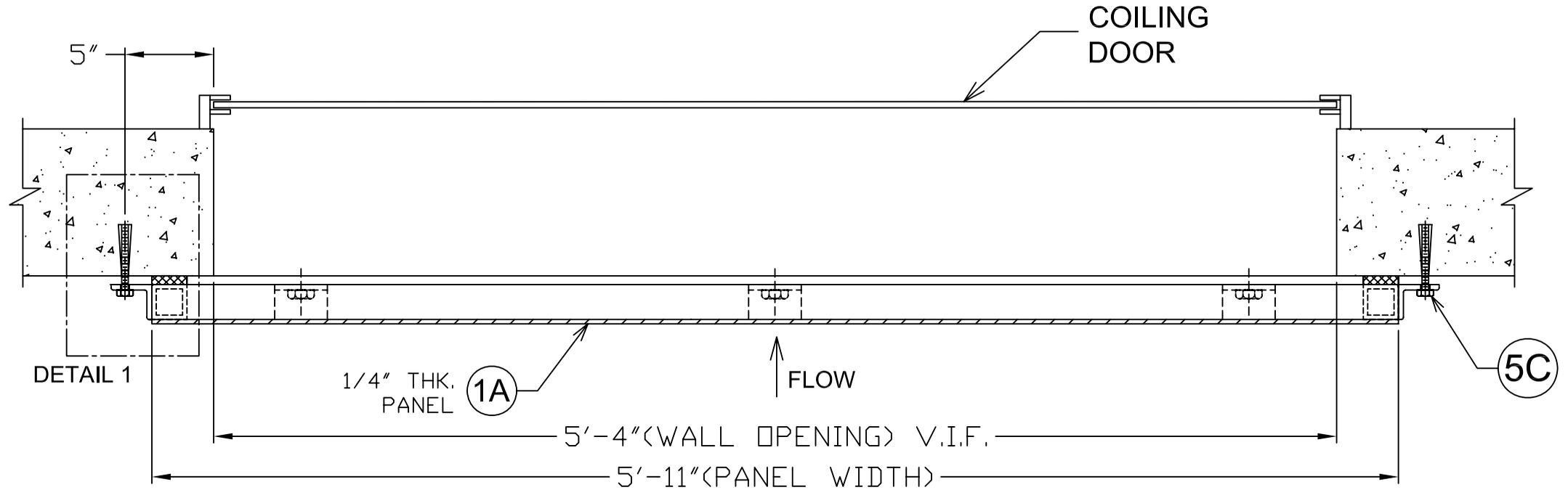
PANEL:
1/4" BENT PLATE

1A



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PAGE 14 OF 23 REVISION 0 DATE 08/28/2023 REVISION DATE REVISION DATE REVISION DATE REVISION DATE	PROJECT TITLE MARGARITAVILLE - BLDG 4 FORT MYERS BEACH, FL	PRODUCTS FLOODTITE FLOOD GATES PER BIG CITY VENTURES STANDARDS FLOOD GATES AND FLOOD STOP LOGS	SPEC SECTION BIG CITY VENTURES FLOODSTOP STANDARDS
GENERAL CONTRACTOR DEANGELIS DIAMOND 6635 WILLOW PARK DRIVE NAPLES, FL 34109	OUR JOB 2023 - M28	ARCHITECT RAMAKER & ASSOCIATES INC 855 COMMUNITY DRIVE SAUK CITY, WI 53583	P.O.#
ENGINEER CALC ENGINEERING, LLC DORAL, FL 33166			

PROPRIETARY DWG OF BIG CITY VENTURES



**FACE MOUNTED
 FLOOD PROTECTION BARRIER**
@ STORAGE ROOM COILING DOOR 4 -106B (ONE EACH)
(5'-4" x 4'-0")
FRONT VIEW

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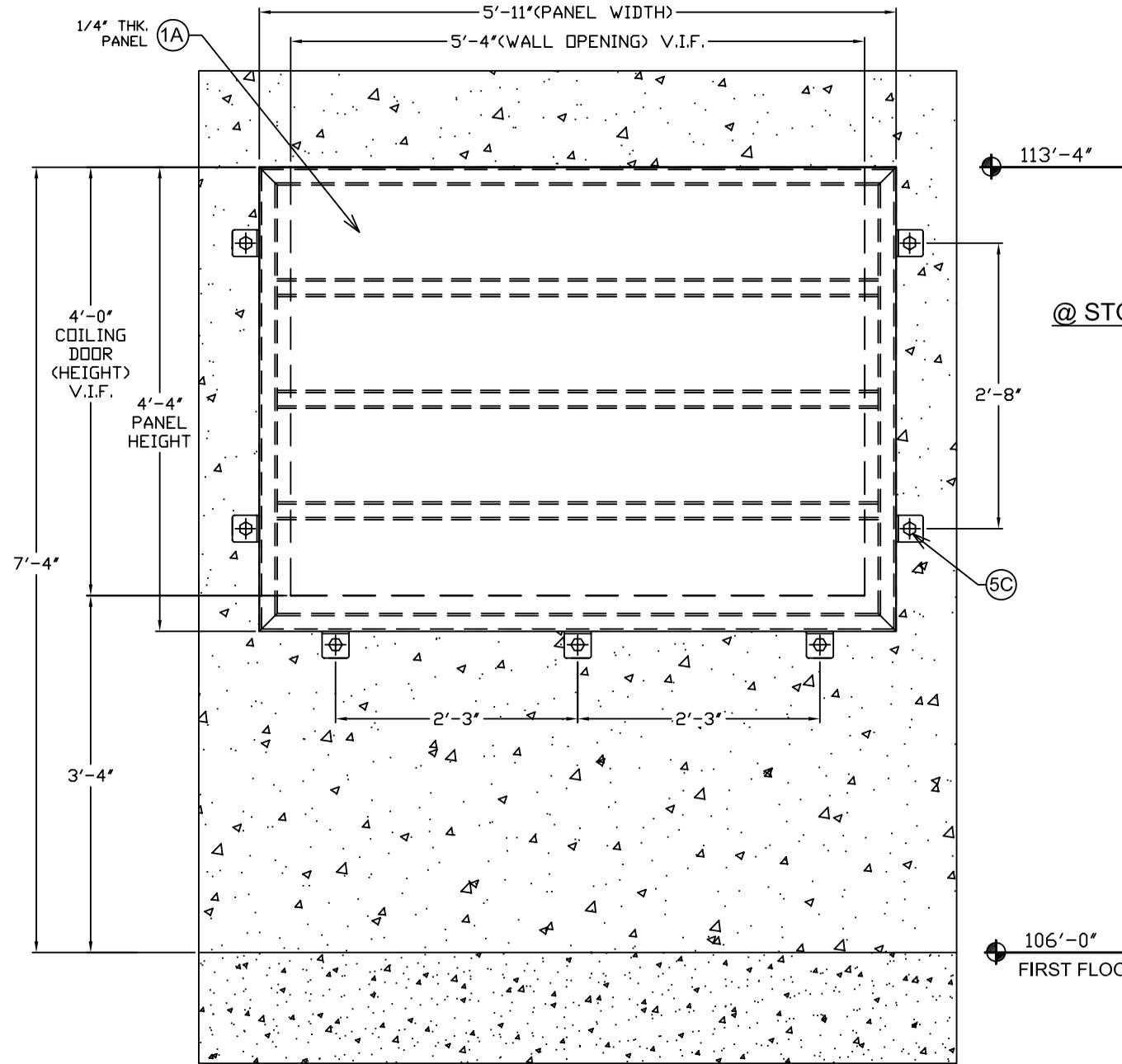


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PAGE 15 OF 23	REVISION 0 DATE 08/28/2023	PROJECT TITLE	MARGARITAVILLE - BLDG 4 FORT MYERS BEACH, FL
REVISION DATE	REVISION DATE	PRODUCTS	FLOODTITE FLOOD GATES PER BIG CITY VENTURES STANDARDS FLOOD GATES AND FLOOD STOP LOGS
REVISION DATE	REVISION DATE	SPEC SECTION	BIG CITY VENTURES FLOODSTOP STANDARDS
REVISION DATE	REVISION DATE	GENERAL CONTRACTOR	DEANGELIS DIAMOND 6635 WILLOW PARK DRIVE NAPLES, FL 34109
REVISION DATE	REVISION DATE	ARCHITECT	RAMAKER & ASSOCIATES INC 855 COMMUNITY DRIVE SAUK CITY, WI 53583
REVISION DATE	REVISION DATE	ENGINEER	CALC ENGINEERING, LLC DORAL, FL 33166
		OUR JOB	2023 - M28
		P.O.#	



PROPRIETARY DWG OF BIG CITY VENTURES

PROPRIETARY DWG OF BIG CITY VENTURES



**FACE MOUNTED
FLOOD PROTECTION BARRIER
@ STORAGE ROOM COILING DOOR 4-106B
(ONE EACH)
(5'-4" x 4'-0")
FRONT VIEW**

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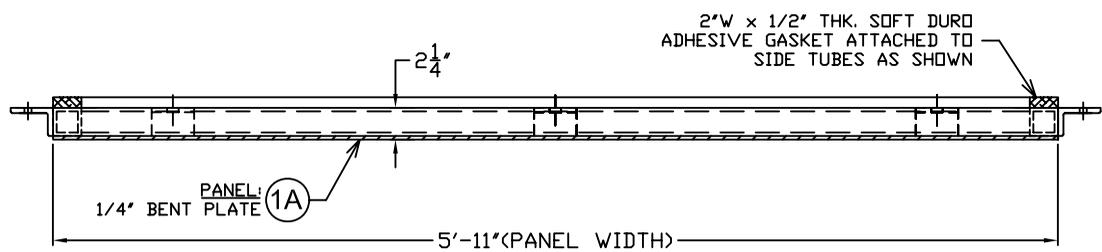
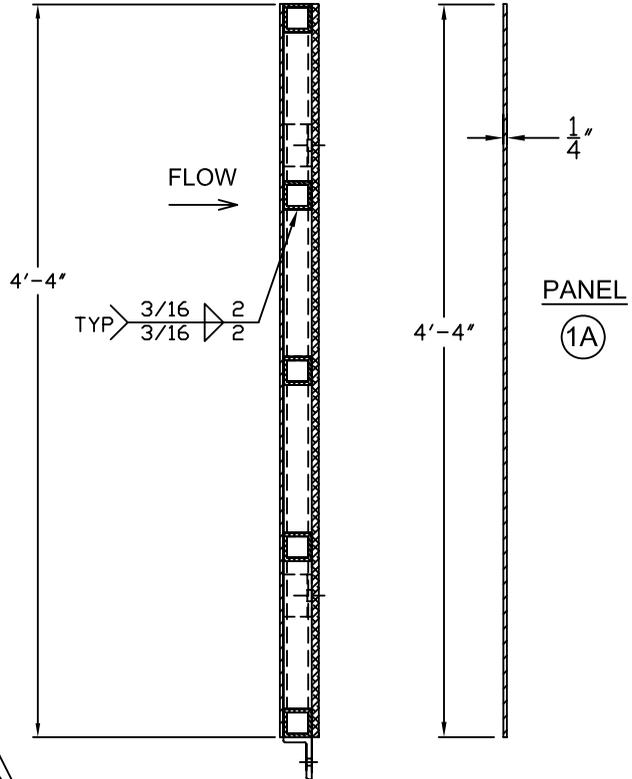
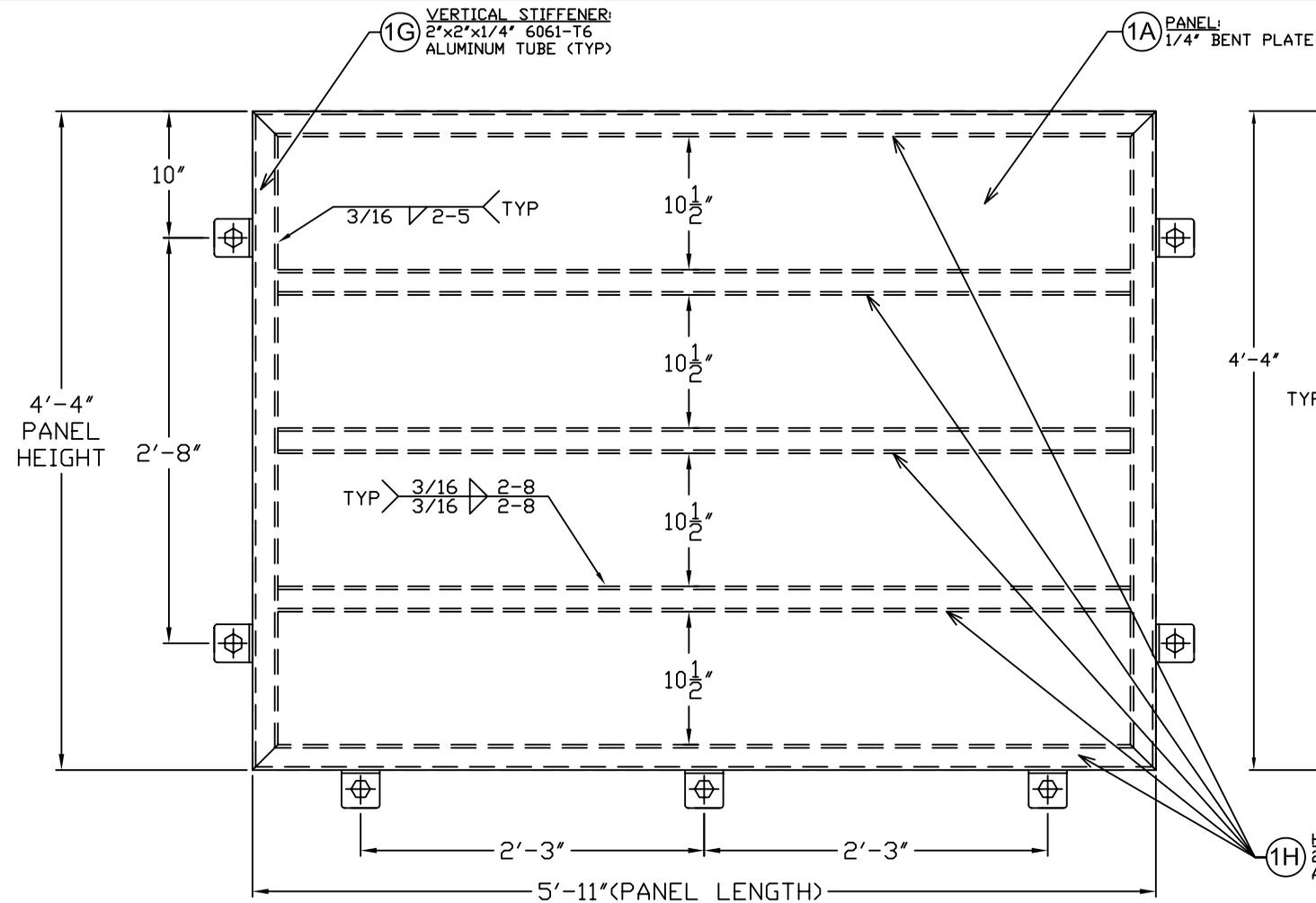


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PAGE 16 OF 23	REVISION 0 DATE 08/28/2023	PROJECT TITLE	MARGARITAVILLE - BLDG 4 FORT MYERS BEACH, FL
REVISION DATE	REVISION DATE	PRODUCTS	FLOODTITE FLOOD GATES PER BIG CITY VENTURES STANDARDS FLOOD GATES AND FLOOD STOP LOGS
REVISION DATE	REVISION DATE	SPEC SECTION	BIG CITY VENTURES FLOODSTOP STANDARDS
REVISION DATE	REVISION DATE	GENERAL CONTRACTOR	DEANGELIS DIAMOND 6635 WILLOW PARK DRIVE NAPLES, FL 34109
REVISION DATE	REVISION DATE	ARCHITECT	RAMAKER & ASSOCIATES INC 855 COMMUNITY DRIVE SAUK CITY, WI 53583
REVISION DATE	REVISION DATE	ENGINEER	CALC ENGINEERING, LLC DORAL, FL 33166
		OUR JOB	2023 - M28
		P.O.#	



PROPRIETARY DWG OF BIG CITY VENTURES

PROPRIETARY DWG OF BIG CITY VENTURES



(1H) HORIZONTAL STIFFENER:
2"x2"x1/4" 6061-T6
ALUMINUM TUBE

**FLOOD BARRIER
(ONE EACH)**

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DORAL FL 33166
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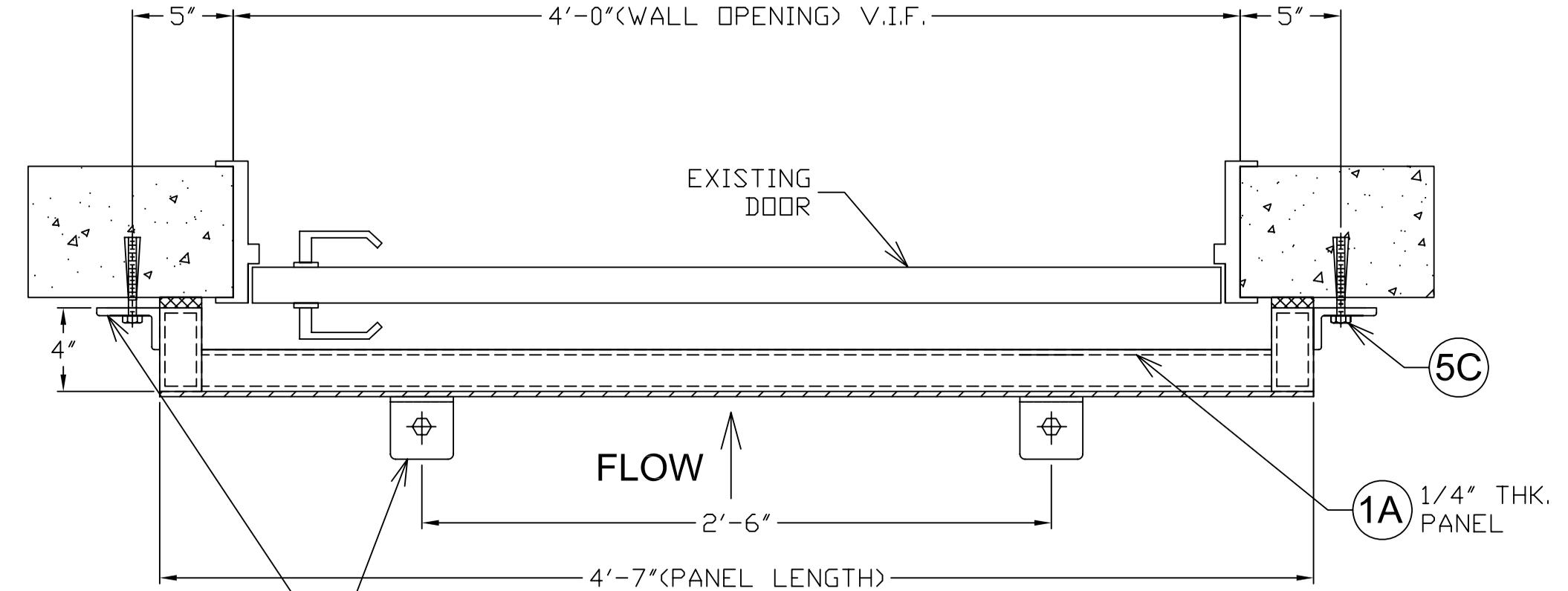
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PAGE	17	OF	23
REVISION	0	DATE	08/28/2023
REVISION	---	DATE	---
REVISION	---	DATE	---
REVISION	---	DATE	---
REVISION	---	DATE	---

BIG CITY VENTURES, LLC
3660 INTERSTATE PARK WAY
RIVIERA BEACH, FL 33404

PROJECT TITLE	MARGARITAVILLE - BLDG 4 FORT MYERS BEACH, FL		
PRODUCTS	FLOODTITE FLOOD GATES PER BIG CITY VENTURES STANDARDS FLOOD GATES AND FLOOD STOP LOGS		
SPEC SECTION	BIG CITY VENTURES FLOODSTOP STANDARDS	OUR JOB	2023 - M28
GENERAL CONTRACTOR	DEANGELIS DIAMOND 6635 WILLOW PARK DRIVE NAPLES, FL 34109	P.O.#	
ARCHITECT	RAMAKER & ASSOCIATES INC 855 COMMUNITY DRIVE SAUK CITY, WI 53583		
ENGINEER	CALC ENGINEERING, LLC DORAL, FL 33166		





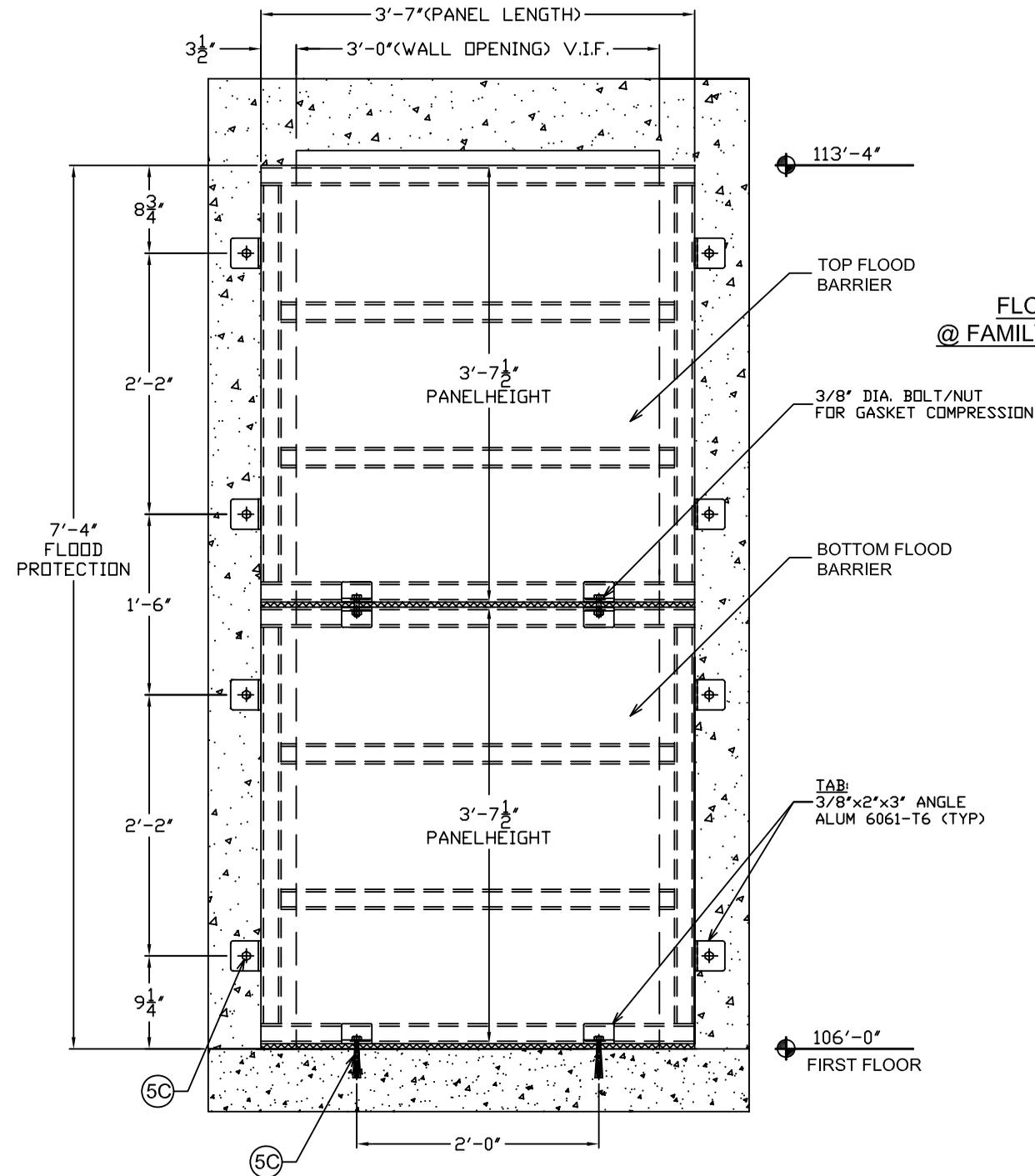
TAB:
3/8"x2"x3" ANGLE
ALUM 6061-T6 (TYP)

**FACE MOUNTED
FLOOD PROTECTION BARRIERS ASSY.
@ FAMILY RESTROOM DOOR 4 -107 (ONE EACH)
(3'-0" x 7'-4")
PLAN VIEW**

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PAGE 18 OF 23 REVISION 0 DATE 08/28/2023 REVISION DATE REVISION DATE REVISION DATE REVISION DATE REVISION DATE	PROJECT TITLE MARGARITAVILLE - BLDG 4 FORT MYERS BEACH, FL	PRODUCTS FLOODTITE FLOOD GATES PER BIG CITY VENTURES STANDARDS FLOOD GATES AND FLOOD STOP LOGS	OUR JOB 2023 - M28
SPEC SECTION BIG CITY VENTURES FLOODSTOP STANDARDS	GENERAL CONTRACTOR DEANGELIS DIAMOND 6635 WILLOW PARK DRIVE NAPLES, FL 34109	P.O.#	ARCHITECT RAMAKER & ASSOCIATES INC 855 COMMUNITY DRIVE SAUK CITY, WI 53583
REVISION DATE REVISION DATE	ENGINEER CALC ENGINEERING, LLC DORAL, FL 33166		



**FACE MOUNTED
FLOOD PROTECTION BARRIERS ASSY.
@ FAMILY RESTROOM DOOR 4 -107 (ONE EACH)
(3'-0" x 7'-4")
FRONT VIEW**

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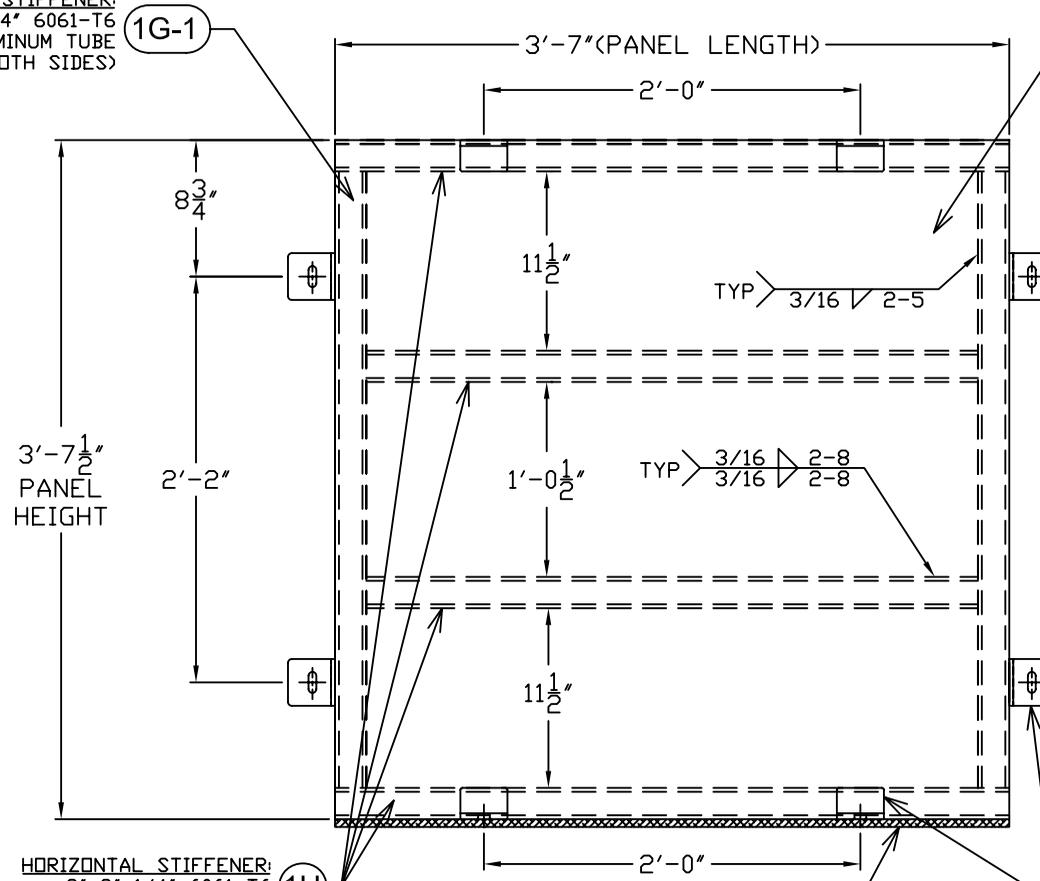
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PAGE 19 OF 23	REVISION 0 DATE 08/28/2023	PROJECT TITLE	MARGARITAVILLE - BLDG 4 FORT MYERS BEACH, FL
REVISION DATE	REVISION DATE	PRODUCTS	FLOODTITE FLOOD GATES PER BIG CITY VENTURES STANDARDS FLOOD GATES AND FLOOD STOP LOGS
REVISION DATE	REVISION DATE	SPEC SECTION	BIG CITY VENTURES FLOODSTOP STANDARDS
REVISION DATE	REVISION DATE	GENERAL CONTRACTOR	DEANGELIS DIAMOND 6635 WILLOW PARK DRIVE NAPLES, FL 34109
REVISION DATE	REVISION DATE	ARCHITECT	RAMAKER & ASSOCIATES INC 855 COMMUNITY DRIVE SAUK CITY, WI 53583
REVISION DATE	REVISION DATE	ENGINEER	CALC ENGINEERING, LLC DORAL, FL 33166
		OUR JOB	2023 - M28
		P.O.#	



PROPRIETARY DWG OF BIG CITY VENTURES

PROPRIETARY DWG OF BIG CITY VENTURES

VERTICAL STIFFENER:
4"x2"x1/4" 6061-T6
ALUMINUM TUBE
(ON BOTH SIDES)

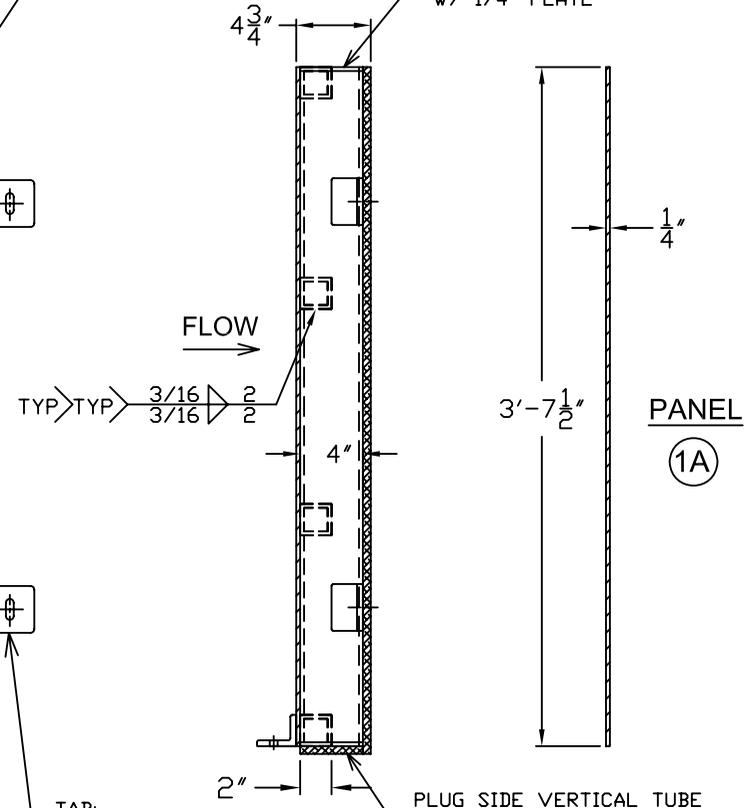


HORIZONTAL STIFFENER:
2"x2"x1/4" 6061-T6
ALUMINUM TUBE

2"W x 1/2" THK. SOFT DURD
ADHESIVE GASKET ATTACHED TO
SIDE TUBES AND ON BOTTOM
HORIZONTAL TUBE AS SHOWN

1A PANEL:
1/4" BENT PLATE

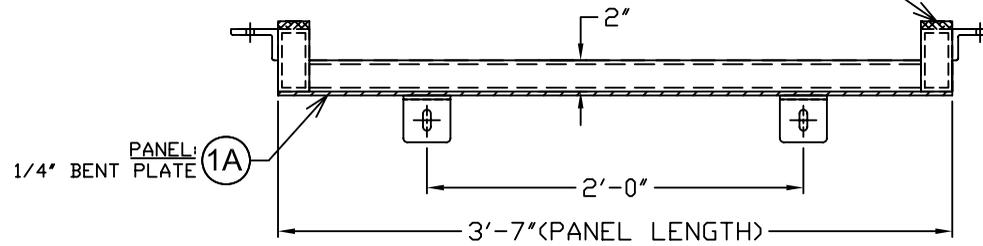
PLUG SIDE VERTICAL TUBE
4"x2"x1/4"
W/ 1/4" PLATE



TAB:
3/8"x2"x3" ANGLE
ALUM 6061-T6 (TYP)

PLUG SIDE VERTICAL TUBE
4"x2"x1/4" ON THE BOTTOM
W/ 1/4" PLATE BEFORE PUT
SELF ADHESIVE GASKET 4"x1/2"

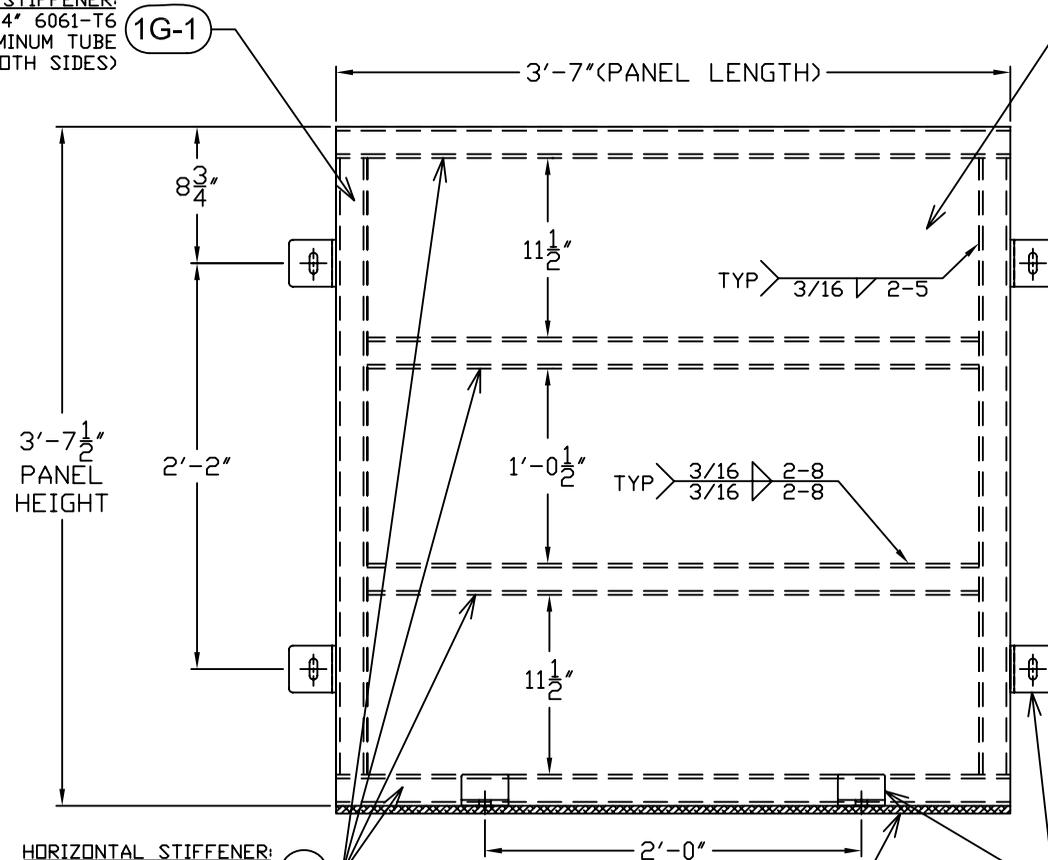
**BOTTOM FLOOD BARRIER
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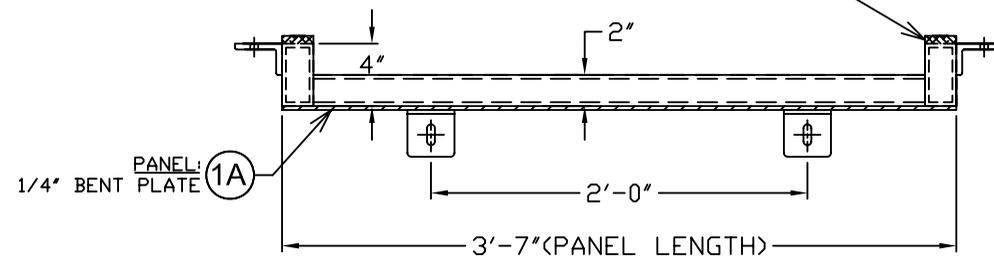
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<p>PAGE 20 OF 23</p> <p>REVISION 0 DATE 08/28/2023</p> <p>REVISION DATE</p> <p>REVISION DATE</p> <p>REVISION DATE</p> <p>REVISION DATE</p> <p>REVISION DATE</p>	<p>PROJECT TITLE</p> <p>MARGARITAVILLE - BLDG 4 FORT MYERS BEACH, FL</p>	<p>PRODUCTS</p> <p>FLOODTITE FLOOD GATES PER BIG CITY VENTURES STANDARDS FLOOD GATES AND FLOOD STOP LOGS</p>	
<p>REVISION DATE</p> <p>REVISION DATE</p> <p>REVISION DATE</p> <p>REVISION DATE</p>	<p>SPEC SECTION</p> <p>BIG CITY VENTURES FLOODSTOP STANDARDS</p>	<p>OUR JOB</p> <p>2023 - M28</p>	
<p>REVISION DATE</p> <p>REVISION DATE</p> <p>REVISION DATE</p>	<p>GENERAL CONTRACTOR</p> <p>DEANGELIS DIAMOND 6635 WILLOW PARK DRIVE NAPLES, FL 34109</p>	<p>P.O.#</p>	
<p>REVISION DATE</p> <p>REVISION DATE</p>	<p>ARCHITECT</p> <p>RAMAKER & ASSOCIATES INC 855 COMMUNITY DRIVE SAUK CITY, WI 53583</p>	<p>ENGINEER</p> <p>CALC ENGINEERING, LLC DORAL, FL 33166</p>	

VERTICAL STIFFENER:
4"x2"x1/4" 6061-T6
ALUMINUM TUBE
(ON BOTH SIDES)



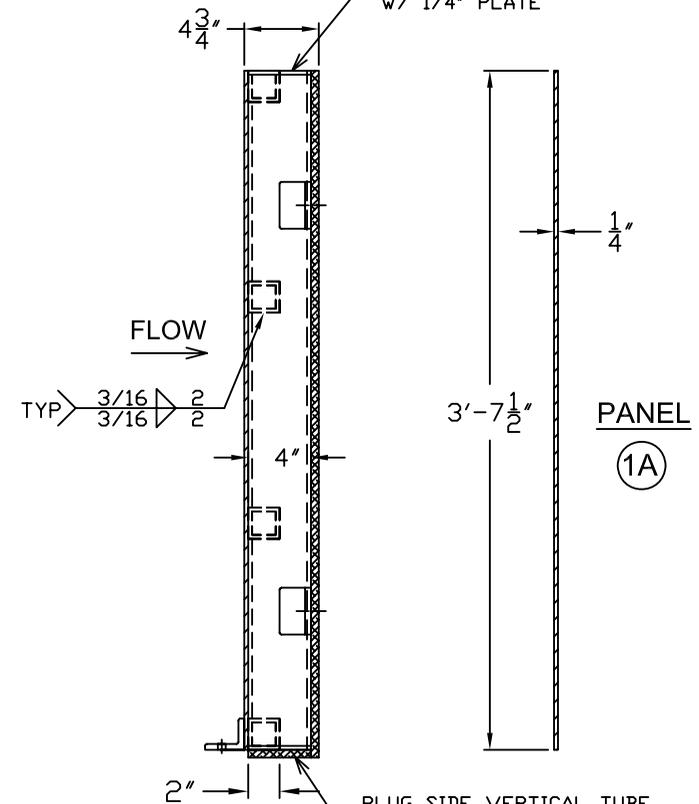
HORIZONTAL STIFFENER:
2"x2"x1/4" 6061-T6
ALUMINUM TUBE

2"W x 1/2" THK. SOFT DURD
ADHESIVE GASKET ATTACHED TO
SIDE TUBES AND ON BOTTOM
HORIZONTAL TUBE AS SHOWN



PANEL:
1/4" BENT PLATE

PLUG SIDE VERTICAL TUBE
4"x2"x1/4"
W/ 1/4" PLATE



TAB:
3/8"x2"x3" ANGLE
ALUM 6061-T6 (TYP)

**TOP FLOOD BARRIER
(ONE EACH)**

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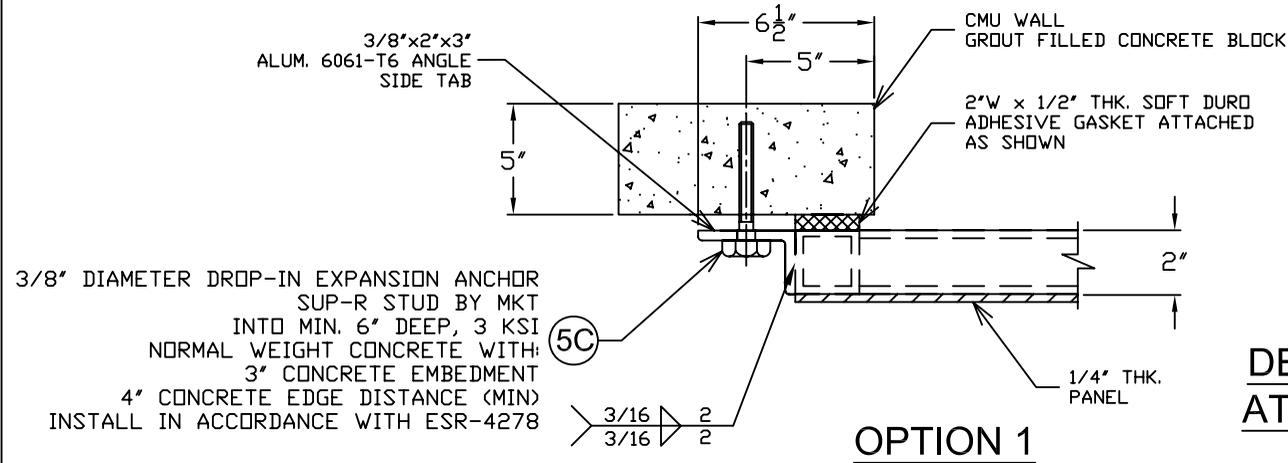
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PAGE 21 OF 23 REVISION 0 DATE 08/28/2023 REVISION DATE REVISION DATE REVISION DATE REVISION DATE	PROJECT TITLE MARGARITAVILLE - BLDG 4 FORT MYERS BEACH, FL	PRODUCTS FLOODTITE FLOOD GATES PER BIG CITY VENTURES STANDARDS FLOOD GATES AND FLOOD STOP LOGS	SPEC SECTION BIG CITY VENTURES FLOODSTOP STANDARDS
GENERAL CONTRACTOR DEANGELIS DIAMOND 6635 WILLOW PARK DRIVE NAPLES, FL 34109	OUR JOB 2023 - M28	ARCHITECT RAMAKER & ASSOCIATES INC 855 COMMUNITY DRIVE SAUK CITY, WI 53583	P.O.#
ENGINEER CALC ENGINEERING, LLC DORAL, FL 33166	ENGINEER		



PROPRIETARY DWG OF BIG CITY VENTURES

PROPRIETARY DWG OF BIG CITY VENTURES

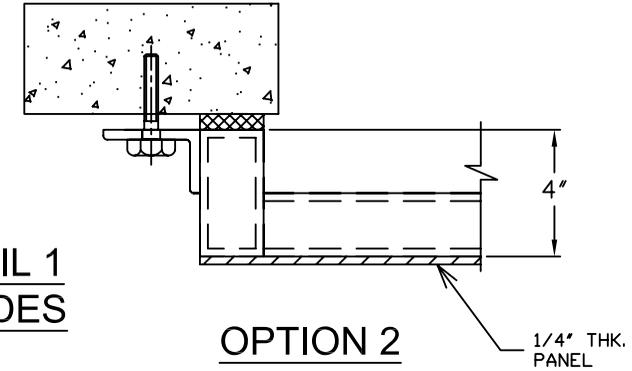
**FLOOD BARRIER
IN DEPLOYED POSITION**



3/8" DIAMETER DROP-IN EXPANSION ANCHOR SUP-R STUD BY MKT INTO MIN. 6" DEEP, 3 KSI NORMAL WEIGHT CONCRETE WITH: 3" CONCRETE EMBEDMENT 4" CONCRETE EDGE DISTANCE (MIN) INSTALL IN ACCORDANCE WITH ESR-4278

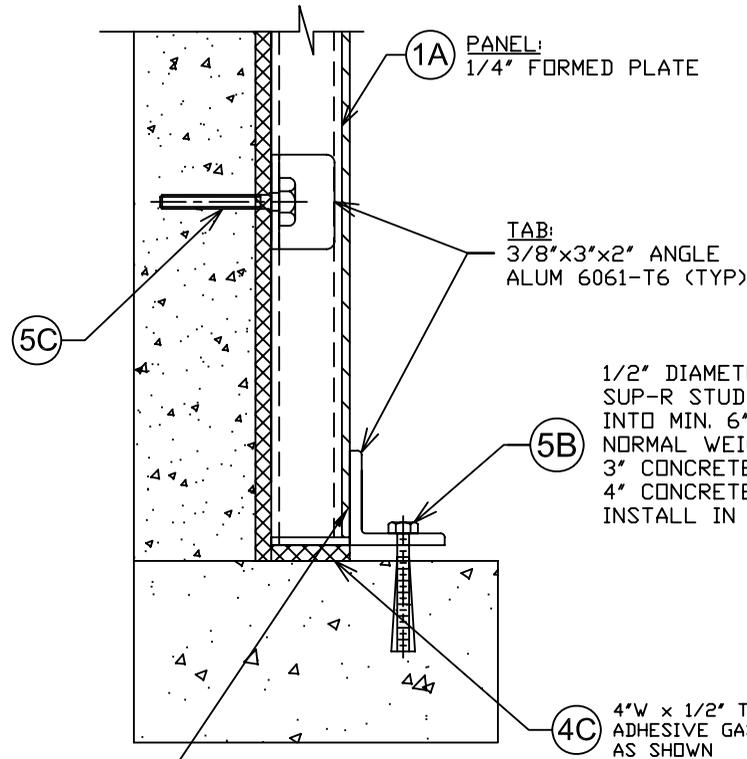
OPTION 1

**DETAIL 1
AT SIDES**



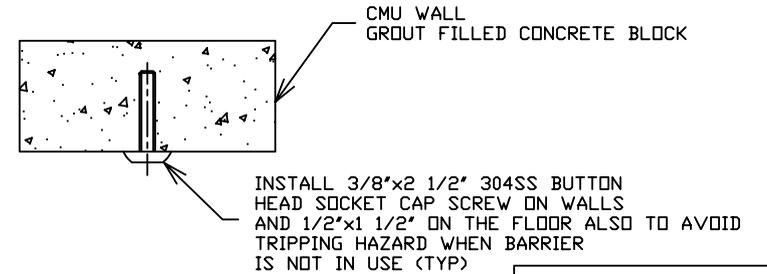
OPTION 2

**DETAIL 1
AT BOTTOM**



1/2" DIAMETER DROP-IN EXPANSION ANCHOR SUP-R STUD BY MKT INTO MIN. 6" DEEP, 3 KSI NORMAL WEIGHT CONCRETE WITH: 3" CONCRETE EMBEDMENT 4" CONCRETE EDGE DISTANCE (MIN) INSTALL IN ACCORDANCE WITH ESR-4278

**FLOOD BARRIER
IN STORED POSITION**



INSTALL 3/8"x2 1/2" 304SS BUTTON HEAD SOCKET CAP SCREW ON WALLS AND 1/2"x1 1/2" ON THE FLOOR ALSO TO AVOID TRIPPING HAZARD WHEN BARRIER IS NOT IN USE (TYP)

CALC ENGINEERING
www.calceng.com
2000 NW 89 FL Unit 102
DORAL FL 33166
Phone: (305) 898-9995
ENGINEERING BUSINESS
CA CERTIFICATION: 32566



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PAGE 22	OF 23	PROJECT TITLE	MARGARITAVILLE - BLDG 4 FORT MYERS BEACH, FL
REVISION 0	DATE 08/28/2023	PRODUCTS	FLOODTITE FLOOD GATES PER BIG CITY VENTURES STANDARDS FLOOD GATES AND FLOOD STOP LOGS
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REVISION	DATE	GENERAL CONTRACTOR	DEANGELIS DIAMOND 6635 WILLOW PARK DRIVE NAPLES, FL 34109
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REVISION	DATE	ENGINEER	CALC ENGINEERING, LLC DORAL, FL 33166
		OUR JOB	2023 - M28
		P.O.#	

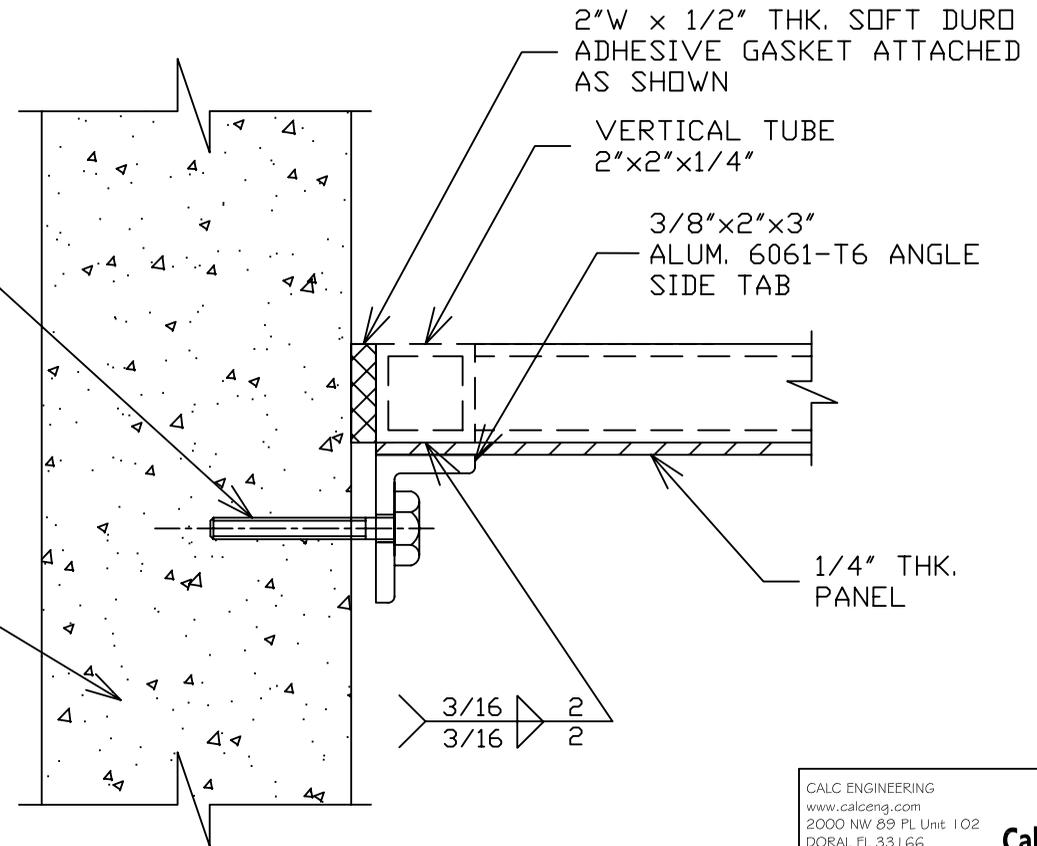


1/2" DIAMETER DROP-IN EXPANSION ANCHOR
 SUP-R STUD BY MKT
 INTO MIN. 6" DEEP, 3 KSI
 NORMAL WEIGHT CONCRETE WITH:
 4 1/2" CONCRETE EMBEDMENT
 4" CONCRETE EDGE DISTANCE (MIN)
 INSTALL IN ACCORDANCE WITH ESR-4278

DETAIL 2

CMU WALL
 GROUT FILLED CONCRETE BLOCK

5A



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 www.calceng.com
 2000 NW 89 PL Unit 102
 DORAL FL 33166
 Phone: (305) 898-9995
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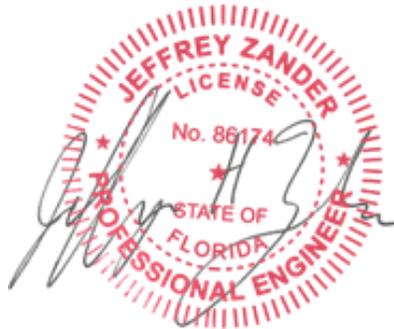
STRUCTURAL CALCULATIONS

for

Margaritaville Fort Myers Beach

Fort Myers Beach, FL
June, 2023

I hereby certify that this plan, specification, or report was prepared by me or under my direct supervision and that I am duly Licensed Professional Engineer under the laws of the State of Wisconsin



Reviewed By: Jeffrey H. Zander

Prepared By: KLM

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Building 4 Design Criteria & Loading

1.DESIGN CODE DATA

2020 FLORIDA BUILDING CODE - BUILDING

ASCE 7-16: MINIMUM DESIGN LOADS AND ASSOCIATED CRITERIA FOR BUILDINGS AND OTHER STRUCTURES.

AISC 360-16: SPECIFICATION FOR STRUCTURAL STEEL BUILDINGS

ACI 318-14: BUILDING CODE REQUIREMENTS FOR STRUCTURAL CONCRETE

TMS 402-2016: BUILDING CODE FOR MASONRY STRUCTURES

ANSI/AWC NDS-2018: NATIONAL DESIGN SPECIFICATION FOR WOOD CONSTRUCTION

AWC SDPWS-2015: SPECIAL DESIGN PROVISION FOR WIND AND SEISMIC

ASCE 24 -14: FLOOD RESISTANT DESIGN AND CONSTRUCTION

2.THIS BUILDING IS DESIGNED IN ACCORDANCE WITH ASCE 24 REQUIREMENTS FOR FLOOD RESISTANCE. IT INCLUDES ALL STRUCTURES BELOW BFE + 1 FOOT BE BREAKAWAY OR DESIGNED TO RESISTS THE FLOOD LOADING.

3.BUILDING OCCUPANCY CATEGORY= II (PER ASCE 7-16 TABLE 1.5-1)

4.DEAD LOADS:

PRECAST PLANK ROOF:35 PSF (NOT INCLUDING PLANK OR 4" TOPPING)
INCLUDING

5 PSF FUTURE SOLAR PANELS FLAT TO THE ROOF
(MUST BE ANCHORED TO THE ROOF)

15 PSF (ROOFING, CEILING, INSULATION, MEP, ETC.)

15 PSF INSULATING CONCRETE

(SEE GC FOR POSSIBLE ALTERNATE)

(INSULATING CONCRETE MAX DENSITY = 50 PCF WITH MAXIMUM THICKNESS OF 3.5".)

FLOORS:15 PSF (NOT INCLUDING PLANK OR TOPPING)

PLAZA SLABS:SEE LOADING PLAN

5.ROOF LIVE LOAD:

LESS THAN 200 SF20 PSF

200 SF TO 600 SFLINEAR INTERPOLATE

GREATER THAN 600 SF12 PSF

6.SNOW LOADS: NOT APPLICABLE

7.WIND DESIGN CRITERIA

WIND SPEED = 150 MPH

(REMOVABLE LIGHT CONSTRUCTION DESIGN WIND SPEED = 105 MPH FBC 3105.4)

EXPOSURE = D

ENCLOSURE CLASSIFICATION = ENCLOSED

Kd= 0.85

Kzt= 1.0

BASE VELOCITY PRESSURE, Qh=50.4 PSF

Ramaker & Associates, Inc.

855 Community Drive
 Sauk City, WI 53583
 608-643-4100

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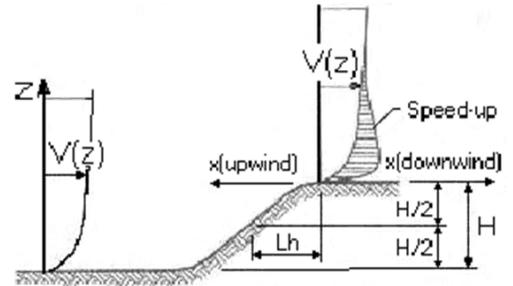
Wind Loads : ASCE 7- 16

Ultimate Wind Speed 150 mph
 Nominal Wind Speed 116.2 mph
 Risk Category I
 Exposure Category D
 Enclosure Classif. Enclosed Building
 Internal pressure +/-0.18
 Directionality (Kd) 0.85
 Kh case 1 1.030
 Kh case 2 1.030
 Type of roof Monoslope

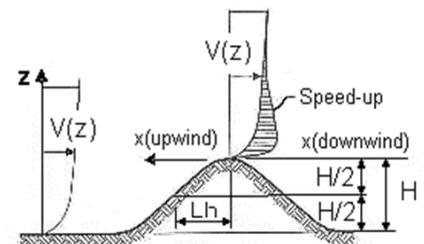
Topographic Factor (Kzt)

Topography Flat
 Hill Height (H) 80.0 ft
 Half Hill Length (Lh) 100.0 ft
 Actual H/Lh = 0.80
 Use H/Lh = 0.50
 Modified Lh = 160.0 ft
 From top of crest: x = 50.0 ft
 Bldg up/down wind? downwind

 H/Lh = 0.50 K₁ = 0.000
 x/Lh = 0.31 K₂ = 0.792
 z/Lh = 0.09 K₃ = 1.000
 At Mean Roof Ht: Kzt = (1+K₁K₂K₃)² = 1.00



ESCARPMENT



2D RIDGE or 3D AXISYMMETRICAL HILL

Gust Effect Factor

h = 11.7 ft
 B = 37.0 ft
 /z (0.6h) = 7.0 ft

Flexible structure if natural frequency < 1 Hz (T > 1 second).
 If building h/B > 4 then may be flexible and should be investigated.
 h/B = 0.32 Rigid structure (low rise bldg)

G = 0.85 Using rigid structure default

Rigid Structure
 ē = 0.13
 ℓ = 650 ft
 Z_{min} = 7 ft
 c = 0.13
 g_Q, g_v = 3.4
 L_z = 535.5 ft
 Q = 0.94
 I_z = 0.16
 G = 0.90 use G = 0.85

Flexible or Dynamically Sensitive Structure
 34 rcy (η₁) = 0.0 Hz
 Damping ratio (β) = 0
 /b = 0.80
 /α = 0.11
 Vz = 148.2
 N₁ = 0.00
 R_n = 0.000
 R_n = 28.282 η = 0.000 h = 11.7 ft
 R_B = 28.282 η = 0.000
 R_L = 28.282 η = 0.000
 g_R = 0.000
 R = 0.000
 G_f = 0.000

Enclosure Classification

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Test for Enclosed Building: $A_o < 0.01A_g$ or 4 sf, whichever is smaller

Test for Open Building: All walls are at least 80% open.
 $A_o \geq 0.8A_g$

Test for Partially Enclosed Building: Predominately open on one side only

Input			Test	
Ao	500.0 sf	$A_o \geq 1.1A_{oi}$	NO	Building is NOT Partially Enclosed
Ag	600.0 sf	$A_o > 4'$ or $0.01A_g$	YES	
Aoi	1000.0 sf	$A_{oi} / A_{gi} \leq 0.20$	YES	
Agi	10000.0 sf			

Conditions to qualify as Partially Enclosed Building. Must satisfy all of the following:

- $A_o \geq 1.1A_{oi}$
- $A_o >$ smaller of 4' or $0.01 A_g$
- $A_{oi} / A_{gi} \leq 0.20$

Where:

- Ao = the total area of openings in a wall that receives positive external pressure.
- Ag = the gross area of that wall in which Ao is identified.
- Aoi = the sum of the areas of openings in the building envelope (walls and roof) not including Ao.
- Agi = the sum of the gross surface areas of the building envelope (walls and roof) not including Ag.

Test for Partially Open Building: A building that does not qualify as open, enclosed or partially enclosed.
(This type building will have same wind pressures as an enclosed building.)

Reduction Factor for large volume partially enclosed buildings (Ri) :

If the partially enclosed building contains a single room that is unpartitioned , the internal pressure coefficient may be multiplied by the reduction factor Ri.

Total area of all wall & roof openings (Aog):	0 sf
Unpartitioned internal volume (Vi) :	0 cf
Ri =	1.00

Ground Elevation Factor (Ke)

Grd level above sea level =	0.0 ft	Ke =	1.0000
Constant =	0.00256	Adj Constant =	0.00256

Wind Loads - MWFRS all h (Except for Open Buildings)

Kh (case 2) = 1.03 h = 11.7 ft GCpi = +/-0.18
 Base pressure (q_n) = **50.4 psf** ridge ht = 12.1 ft G = 0.85
 Roof Angle (θ) = 1.2 deg L = 68.0 ft qi = qh
 Roof tributary area - (h/2)*L: 397 sf B = 37.0 ft
 (h/2)*B: 216 sf

Ultimate Wind Surface Pressures (psf)

Surface	Wind Normal to Ridge				Wind Parallel to Ridge				
	B/L = 0.54	h/L = 0.32			L/B = 1.84	h/L = 0.17			
	Cp	q _n GC _p	w/+q _i GC _{pi}	w/-q _i GC _{pi}	Dist.*	Cp	q _n GC _p	w/+q _i GC _{pi}	w/-q _i GC _{pi}
Windward Wall (WW)	0.80	34.3	see table below			0.80	34.3	see table below	
Leeward Wall (LW)	-0.50	-21.4	-30.5	-12.4		-0.33	-14.3	-23.3	-5.2
Side Wall (SW)	-0.70	-30.0	-39.1	-20.9		-0.70	-30.0	-39.1	-20.9
Leeward Roof (LR)	**				Included in windward roof				
Neg Windward Roof: 0 to h/2*	-0.90	-38.6	-47.7	-29.5	0 to h/2*	-0.90	-38.6	-47.7	-29.5
h/2 to h*	-0.90	-38.6	-47.7	-29.5	h/2 to h*	-0.90	-38.6	-47.7	-29.5
h to 2h*	-0.50	-21.44	-30.52	-12.36	h to 2h*	-0.50	-21.4	-30.5	-12.4
> 2h*	-0.30	-12.86	-21.94	-3.78	> 2h*	-0.30	-12.9	-21.9	-3.8
Pos/min windward roof press.	-0.18	-7.7	-16.8	1.4	Min press.	-0.18	-7.7	-16.8	1.4

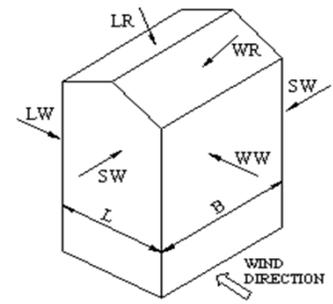
**Roof angle < 10 degrees. Therefore, leeward roof is included in windward roof pressure zones.

*Horizontal distance from windward edge

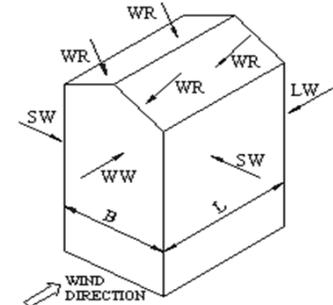
For monoslope roofs, entire roof surface is either windward or leeward surface.

Windward Wall Pressures at "z" (psf)

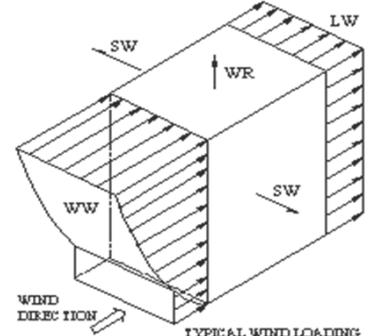
z	Kz	Kzt	Windward Wall			Combined WW + LW	
			q _z GC _p	w/+q _i GC _{pi}	w/-q _i GC _{pi}	Normal to Ridge	Parallel to Ridge
h= 0 to 15'	1.03	1.00	34.3	25.2	43.4	55.7	48.6



WIND NORMAL TO RIDGE



WIND PARALLEL TO RIDGE



TYPICAL WIND LOADING

NOTE:
 See figure in ASCE7 for the application of full and partial loading of the above wind pressures. There are 4 different loading cases.

Parapet

z	Kz	Kzt	qp (psf)
13.5 ft	1.03	1.00	50.4

Windward parapet: 75.7 psf (GCpn = +1.5)
 Leeward parapet: -50.4 psf (GCpn = -1.0)

Windward roof overhangs (add to windward roof pressure) : 34.3 psf (upward)

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Ultimate Wind Pressures

Wind Loads - Components & Cladding : h ≤ 60'

Kh (case 1) = 1.03 h = 11.7 ft 0.2h = 2.3 ft
 Base pressure (qh) = **50.4 psf** 0.6h = 7.0 ft
 Minimum parapet ht = 1.7 ft GCpi = +/-0.18
 Roof Angle (θ) = 1.2 deg qi = qh = 50.4 psf
 Type of roof = Monoslope

Roof

Area	Surface Pressure (psf)							
	10 sf	20 sf	50 sf	100 sf	200 sf	350 sf	500 sf	1000 sf
Negative Zone 1	-94.8	-88.6	-80.3	-74	-67.8	-62.7	-59.5	-59.5
Negative Zone 1'	-54.5	-54.5	-54.5	-54.5	-46.9	-40.8	-36.8	-29.3
Negative Zone 2	-125.1	-117	-106.4	-98.4	-90.3	-83.8	-79.7	-79.7
Negative Zone 3	-170.5	-154.4	-133.1	-117	-101.0	-88.0	-79.7	-79.7
Positive All Zones	24.2	22.7	20.7	19.2	19.2	19.2	19.2	19.2
Overhang Zone 1&1'	-85.7	-84.2	-82.2	-80.7	-67.7	-57.1	-50.4	-50.4
Overhang Zone 2	-116	-105.3	-91.1	-80.4	-69.7	-61.0	-55.5	-55.5
Overhang Zone 3	-161.4	-142.6	-117.8	-99.1	-80.3	-65.1	-55.5	-55.5

User input	
40 sf	300 sf
-82.3	-64.1
-54.5	-42.4
-109.0	-85.6
-138.3	-91.5
21.2	19.2
-82.7	-60.0
-94.6	-63.4
-123.9	-69.3

Overhang pressures in the table above assume an internal pressure coefficient (Gcpi) of 0.0
 Overhang soffit pressure equals adj wall pressure (which includes internal pressure of 9.1 psf)

Parapet

qp = 50.4 psf

Solid Parapet Pressure	Surface Pressure (psf)					
	10 sf	20 sf	50 sf	100 sf	200 sf	500 sf
CASE A: Zone 2:	161.4	151.0	137.1	126.7	116.2	102.4
Zone 3:	206.8	188.3	163.8	145.3	126.8	102.4
CASE B: Interior zone:	-95.3	-90.5	-84.1	-79.3	-74.5	-68.1
Corner zone:	-109.0	-101.7	-92.1	-84.9	-77.7	-68.1

User input
40 sf
140.5
169.8
-85.7
-94.5

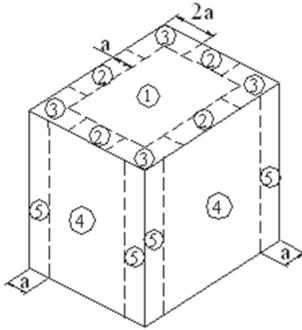
Walls

Area	GCp +/- GCpi				Surface Pressure at h			
	10 sf	100 sf	200 sf	500 sf	10 sf	100 sf	200 sf	500 sf
Negative Zone 4	-1.17	-1.01	-0.96	-0.90	-59.0	-51.0	-48.6	-45.4
Negative Zone 5	-1.44	-1.12	-1.03	-0.90	-72.6	-56.6	-51.8	-45.4
Positive Zone 4 & 5	1.08	0.92	0.87	0.81	54.5	46.5	44.0	40.9

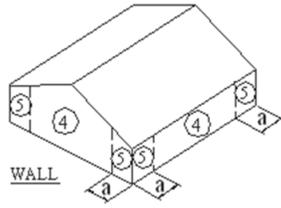
User input	
66 sf	200 sf
-52.4	-48.6
-59.5	-51.8
47.9	44.0

Note: GCp reduced by 10% due to roof angle ≤ 10 deg.

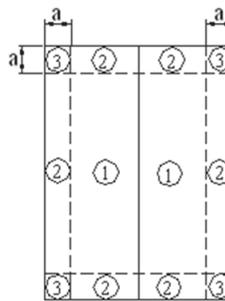
Location of C&C Wind Pressure Zones - ASCE 7-10 & earlier



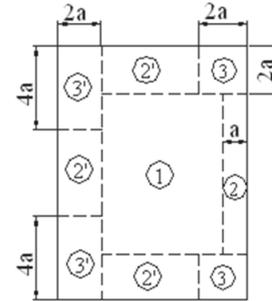
Roofs w/ $\theta \leq 10^\circ$
 and all walls
 $h > 60'$



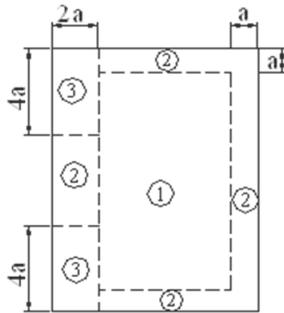
Walls $h \leq 60'$
 & alt design $h < 90'$



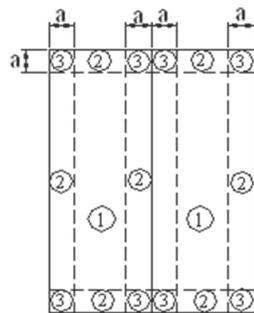
Gable, Sawtooth and
 Multispan Gable $\theta \leq 7$ degrees &
 Monoslope ≤ 3 degrees
 $h \leq 60'$ & alt design $h < 90'$



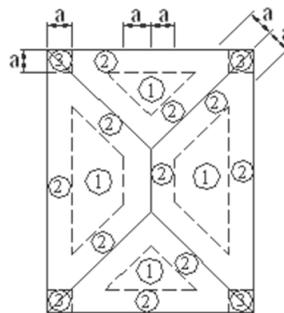
Monoslope roofs
 $3^\circ < \theta \leq 10^\circ$
 $h \leq 60'$ & alt design $h < 90'$



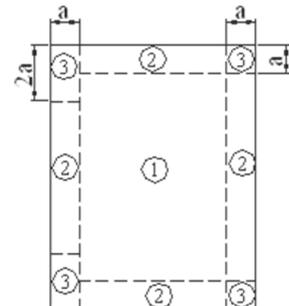
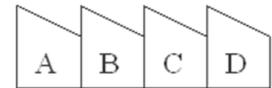
Monoslope roofs
 $10^\circ < \theta \leq 30^\circ$
 $h \leq 60'$ & alt design $h < 90'$



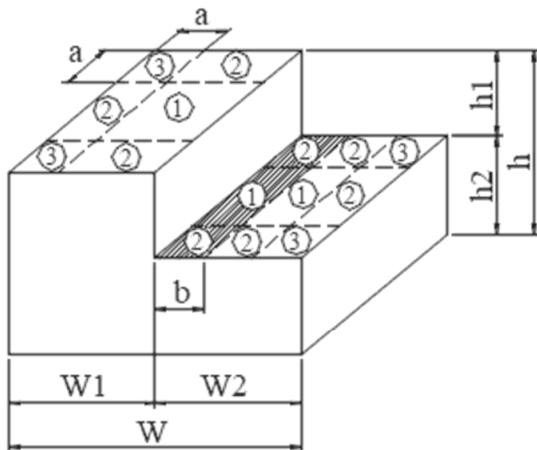
Multispan Gable &
 Gable $7^\circ < \theta \leq 45^\circ$



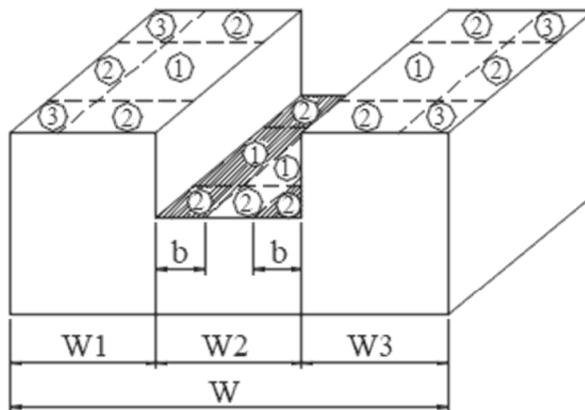
Hip $7^\circ < \theta \leq 27^\circ$



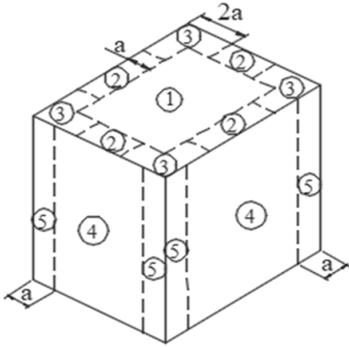
Sawtooth $10^\circ < \theta \leq 45^\circ$
 $h \leq 60'$ & alt design $h < 90'$



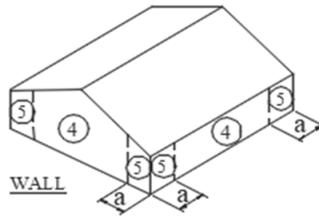
Stepped roofs $\theta \leq 3^\circ$
 $h \leq 60'$ & alt design $h < 90'$



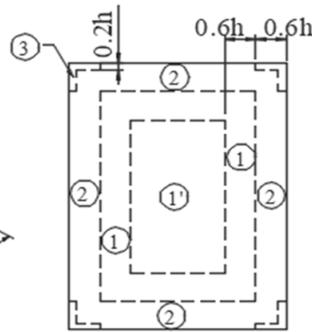
Location of C&C Wind Pressure Zones - ASCE 7-16



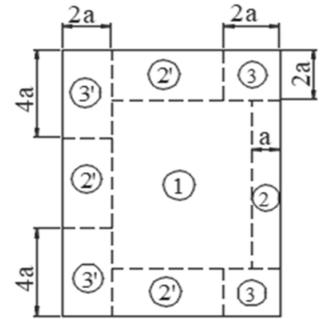
Roofs w/ $\theta \leq 10^\circ$
 and all walls
 $h > 60'$



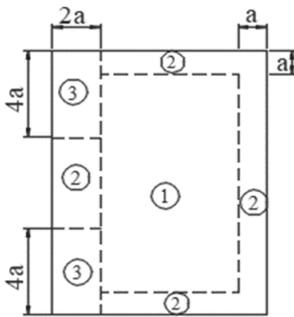
Walls $h \leq 60'$
 & alt design $h < 90'$



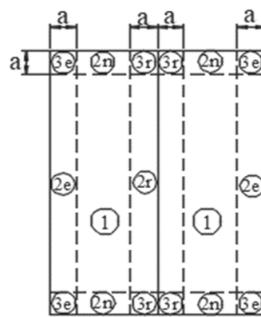
Gable, Sawtooth and
 Multispan Gable $\theta \leq 7$ degrees &
 Monoslope ≤ 3 degrees
 $h \leq 60'$ & alt design $h < 90'$



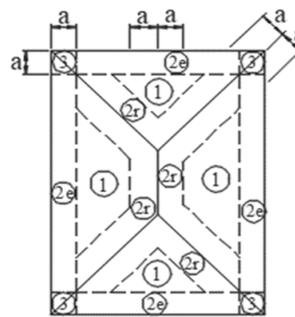
Monoslope roofs
 $3^\circ < \theta \leq 10^\circ$
 $h \leq 60'$ & alt design $h < 90'$



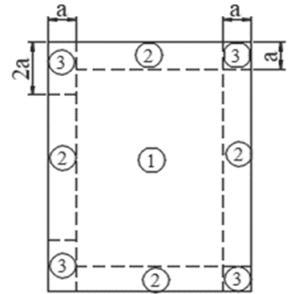
Monoslope roofs
 $10^\circ < \theta \leq 30^\circ$
 $h \leq 60'$ & alt design $h < 90'$



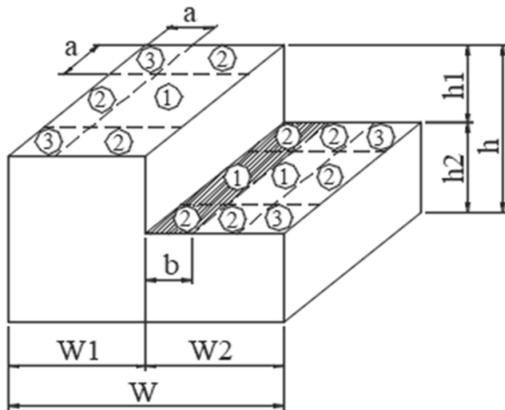
Multispan Gable &
 Gable $7^\circ < \theta \leq 45^\circ$



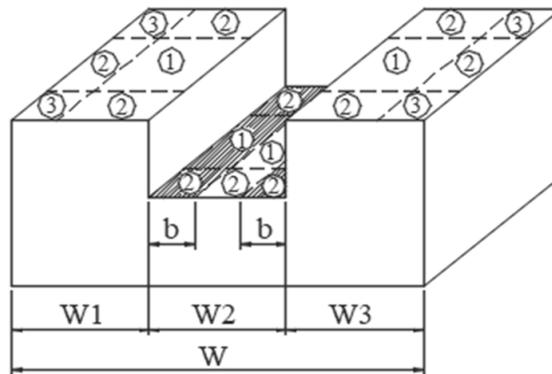
Hip $7^\circ < \theta \leq 27^\circ$



Sawtooth $10^\circ < \theta \leq 45^\circ$
 $h \leq 60'$ & alt design $h < 90'$



Stepped roofs $\theta \leq 3^\circ$
 $h \leq 60'$ & alt design $h < 90'$



Roof Height	11.7 ft
BFE	12.0 ft
G	6.0 ft
Cp	2.8
γ_w	64.0 pcf
W	2000.0 lbs
Cd	1.00
Cb	1.00
CSTR	0.80
α	45 °

Table 5.4-1 Value of Dynamic Pressure Coefficient, C_p

Risk Category ^a	C_p
I	1.6
II	2.8
III	3.2
IV	3.5

^aFor Risk Category, see Table 1.5-1.

$$d_s = 3.90 \text{ ft} \qquad d_s = 0.65(\text{BFE} - G) \qquad (5.4-3)$$

$$P_{\max} = 998.4 \text{ psf} \qquad P_{\max} = C_p \gamma_w d_s + 1.2 \gamma_w d_s \qquad (5.4-5)$$

Ft = 4848 plf applied near still water

$$V = 5.6 \text{ ft/sec} \qquad V = \text{velocity of water (ft/sec), approximated by } 1/2(gd_s)^{1/2}$$

Fi = 8.96 kips at ds

COASTAL 24-14 BASIC VALUES

BFE = 12'

ASCE 24

EQN 5.4-3

$$d_s = .65(BFE - G) \quad d_s = .65(12 - 6)$$

$$= 3.9'$$

EQN 5.4-2

BREAKING WAVE
 HEIGHT

$$H_b = .78 d_s \quad H_b = (.78) 3.9'$$

$$= 3.04'$$

CREST OF WAVE ELEVATION

$$G + (1.55 d_s)$$

$$6 + 1.55(3.9')$$

$$= 12.045'$$

$$DFE = BFE + 1' = 13'$$

WAVE ON COLUMN

EQN 5.4-4 = $.5(W)(C_D)(D)H_b^2$

$F_D \Rightarrow$

$$F_D = (.5)(64)(2.25)(1.4)(1.33)(3.04)^2$$

$$F_D = 1.24 \text{ kips}$$

DEBRIS IMPACT

$$F_i = WVC_D C_B C_{str}$$

$$V = \frac{1}{2}(32.2 \times 3.9)^{1/2} = 5.6 \text{ ft/sec}$$

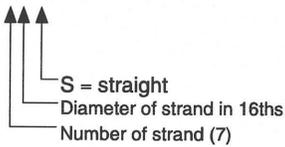
$$F_i = (4,000)(5.6)(1)(1)(.4)$$

$$= 8.9 \text{ kips}$$

3.6 Hollow-Core Load Tables (cont.)

Strand Pattern Designation

76-S



Safe loads shown include dead load of 10 lb/ft² for untopped members and 15 lb/ft² for topped members. Remainder is live load. Long-time cambers include superimposed dead load but do not include live load.

Capacity of sections of other configurations are similar. For precise values, see local hollow-core manufacturer.

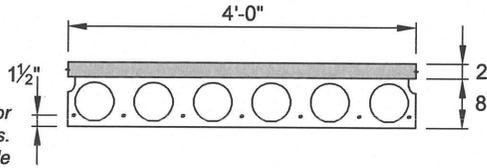
Key

385- Safe superimposed service load, lb/ft²

0.1 - Estimated camber at erection, in.

0.2 - Estimated long-time camber, in.

4'-0" x 8"
Normalweight Concrete



Section Properties

	No Topping	2 in. topping
A	215 in. ²	-
I	1666 in. ⁴	3071 in. ⁴
y _b	4.00 in.	5.29 in.
y _t	4.00 in.	4.71 in.
S _b	417 in. ³	581 in. ³
S _t	417 in. ³	652 in. ³
wt	224 lb/ft	324 lb/ft
DL	56 lb/ft²	81 lb/ft²
V/S	1.92 in.	

f'_c = 5000 psi

f_{pu} = 270,000 psi

4HC8

Table of safe superimposed service load, lb/ft², and cambers, in.

No Topping

Strand designation code	Span, ft																																																																
	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40																																			
66-S	ROOF:																				124	110	98	87	77	69	61	54	48	43	38	33	29																																
	50 PSF TOPPING																				0.3	0.2	0.2	0.2	0.2	0.1	0.0	0.0	-0.1	-0.2	-0.3	-0.5	-0.7	-0.9																															
	15 PSF SUPER DL																				0.3	0.2	0.2	0.1	0.0	-0.1	-0.2	-0.3	-0.5	-0.7	-0.9																																		
76-S	15 PSF INSULATING CONC.																				149	133	119	106	95	86	77	69	62	55	50	44	39	35	31	26																													
	5 PSF FUTURE SOLAR																				0.4	0.4	0.3	0.3	0.3	0.3	0.2	0.2	0.1	0.0	-0.1	-0.2	-0.4	-0.6	-0.8																														
	20 PSF LL																				0.4	0.4	0.3	0.3	0.2	0.1	0.0	-0.1	-0.2	-0.4	-0.6	-0.8																																	
58-S	105 PSF TOTAL																				179	169	160	144	138	118	107	97	88	80	72	66	60	54	48	42	37	32	28																										
																					0.6	0.6	0.6	0.6	0.6	0.6	0.5	0.5	0.5	0.4	0.3	0.2	0.1	0.0	-0.4	-0.3	-0.5	-0.7	-0.9																										
																					0.7	0.7	0.7	0.7	0.6	0.6	0.6	0.5	0.4	0.3	0.2	0.0	-0.2	-0.4	-0.6	-0.9	-1.2	-1.6	-2.0	-2.4																									
68-S																					209	200	180	165	153	142	132	121	110	101	92	84	77	70	63	56	51	45	40																										
																					0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.7	0.7	0.6	0.5	0.4	0.2	0.1	-0.1	-0.3																									
																					0.9	1.0	1.0	1.0	1.0	0.9	0.9	0.9	0.8	0.7	0.6	0.4	0.2	0.0	-0.2	-0.5	-0.8	-1.1	-1.5																										
78-S																					488	442	402	370	341	318	295	275	259	241	229	215	203	195	180	168	157	144	135	126	118	110	101	92	84	77	70	63	56	51	45	40													
																					0.3	0.3	0.4	0.5	0.5	0.6	0.6	0.7	0.7	0.8	0.9	1.0	1.0	1.0	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.0	0.9	0.8	0.7	0.6	0.5	0.3												
																					0.4	0.5	0.5	0.6	0.7	0.8	0.8	0.9	1.0	1.0	1.1	1.2	1.2	1.2	1.3	1.3	1.3	1.3	1.3	1.2	1.2	1.1	1.0	0.8	0.7	0.5	0.3	0.0	-0.3	-0.7															

4HC8 + 2

Table of safe superimposed service load, lb/ft², and cambers, in.

2 in. Normalweight Topping

Strand designation code	Span, ft																																												
	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40																	
66-S	400	365	333	308	282	256	224	197	173	153	135	119	105	93	82	68	56	45	36	26																									
	0.2	0.2	0.2	0.2	0.2	0.2	0.3	0.3	0.3	0.3	0.2	0.2	0.2	0.2	0.1	0.0	-0.0	-0.1	-0.2	-0.3																									
	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.1	0.1	0.0	-0.1	-0.2	-0.3	-0.4	-0.6	-0.7	-0.9	-1.2	-1.4																									
76-S	474	435	396	366	340	304	267	235	208	184	164	146	130	116	103	88	74	62	51	41	31																								
	0.2	0.2	0.3	0.3	0.3	0.3	0.3	0.4	0.4	0.4	0.3	0.3	0.3	0.2	0.2	0.1	0.0	-0.1	-0.2	-0.4	-0.5	-0.7	-0.9	-1.2	-1.4																				
	0.2	0.2	0.3	0.3	0.3	0.3	0.3	0.3	0.2	0.2	0.2	0.1	0.0	-0.1	-0.2	-0.4	-0.5	-0.7	-0.9	-1.2	-1.4																								
58-S	445	405	374	342	318	298	275	260	243	228	217	196	177	159	143	126	110	95	82	70	59																								
	0.3	0.3	0.3	0.4	0.4	0.5	0.5	0.5	0.5	0.6	0.6	0.6	0.6	0.6	0.5	0.5	0.5	0.1	0.3	0.2																									
	0.3	0.3	0.4	0.4	0.4	0.4	0.5	0.5	0.5	0.5	0.4	0.3	0.3	0.2	0.1	-0.1	-0.2	-0.4	-0.6	-0.9	-1.2	-1.5	-1.8																						
68-S	463	426	393	366	342	319	299	282	267	251	239	216	195	177	158	140	124	110	97	84																									
	0.4	0.4	0.5	0.5	0.6	0.6	0.7	0.7	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.7	0.7																									
	0.4	0.5	0.5	0.6	0.6	0.6	0.6	0.7	0.7	0.7	0.6	0.6	0.6	0.5	0.4	0.3	0.2	0.0	-0.2	-0.4	-0.6	-0.9	-1.2	-1.6	-2.0	-2.4																			
78-S	472	435	402	375	348	325	305	288	273	257	245	232	220	207	186	167	149	133	119	106																									
	0.5	0.5	0.6	0.6	0.7	0.7	0.8	0.9	0.9	1.0	1.0	1.0	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1																									
	0.5	0.6	0.6	0.7	0.7	0.8	0.8	0.8	0.9	0.9	0.9	0.9	0.9	0.8	0.8	0.7	0.7	0.6	0.4	0.3	0.1	-0.1	-0.3	-0.6	-0.9	-1.3	-1.7	-2.2																	

Strength is based on strain compatibility; bottom tension is limited to 7.5√f'_c; see pages 3-8 through 3-11 for explanation. See item 3, note 4, Section 3.3.2 for explanation of vertical line.

Building 4 Gravity Design



Bentley

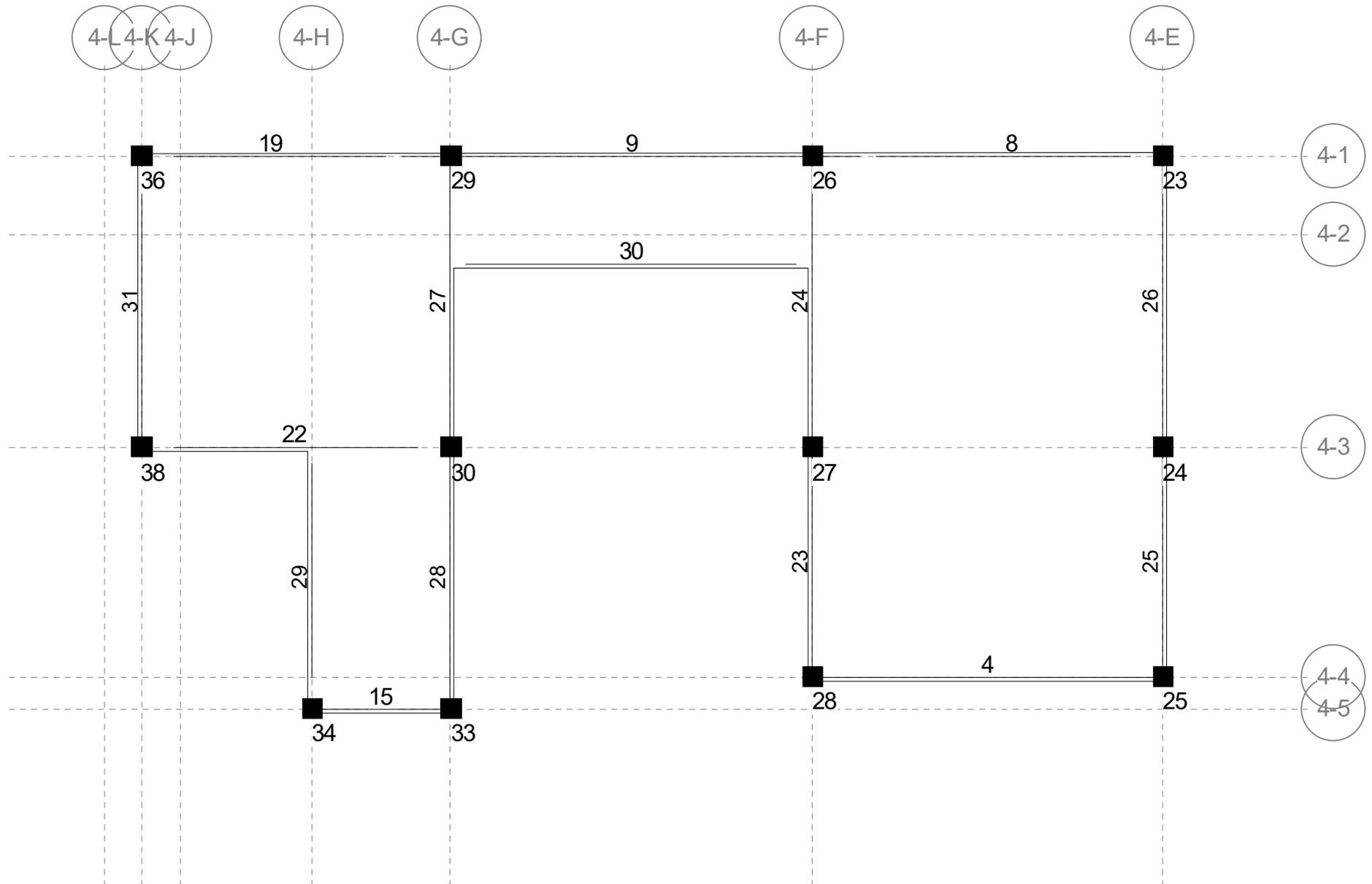
RAM Steel 17.04.02.12
DataBase: 30479 Building 4
Building Code: IBC

Floor Map

01/23/23 13:59:36
Steel Code: AISC 360-16 LRFD

Floor Type: ROOF

Beam Numbers





Gravity Beam Design

RAM Steel 17.04.02.12
DataBase: 30479 Building 4
Building Code: IBC

01/23/23 13:59:36
Steel Code: AISC 360-16 LRFD

Floor Type: ROOF

Beam Number = 8

SPAN INFORMATION (ft): I-End (42.67,0.00) J-End (61.67,0.00)

Beam Size (User Selected) = W10X33 Fy = 50.0 ksi
Total Beam Length (ft) = 19.00
Mp (kip-ft) = 161.67

LINE LOADS (k/ft):

Load	Dist	DL	LL	Red%	Type	PartL
1	11.670	0.080	0.000	0.0%	Red	0.000
	19.000	0.080	0.000			0.000
2	0.000	0.016	0.000	---	NonR	0.000
	19.000	0.016	0.000			0.000
3	0.000	0.015	0.005	0.0%	Roof	0.000
	19.000	0.015	0.005			0.000
4	0.000	0.033	0.000	---	NonR	0.000
	19.000	0.033	0.000			0.000

SHEAR (Ultimate): Max Vu (1.4DL) = 1.53 kips 1.00Vn = 84.65 kips

MOMENTS (Ultimate):

Span	Cond	LoadCombo	Mu kip-ft	@ ft	Lb ft	Cb	Phi	Phi*Mn kip-ft
Center	Max +	1.4DL	5.7	11.2	19.0	1.14	0.90	115.97
Controlling		1.4DL	5.7	11.2	19.0	1.14	0.90	115.97

REACTIONS (kips):

	Left	Right
DL reaction	0.73	1.09
Max +LL reaction	0.05	0.05
Max +total reaction (factored)	1.02	1.53

DEFLECTIONS:

				Ratio
Dead load (in)	at 9.78 ft =	-0.054	L/D = 4249	
Live load (in)	at 9.78 ft =	-0.003	L/D = 7471 > 360	0.00
			2	
Net Total load (in)	at 9.78 ft =	-0.057	L/D = 4021 > 240	0.06



Gravity Beam Design

RAM Steel 17.04.02.12
DataBase: 30479 Building 4
Building Code: IBC

Page 2/4
01/23/23 13:59:36
Steel Code: AISC 360-16 LRFD

Floor Type: ROOF

Beam Number = 19

SPAN INFORMATION (ft): I-End (-2.50,-0.00) J-End (14.00,0.00)

Beam Size (User Selected) = W10X33 Fy = 50.0 ksi
Total Beam Length (ft) = 16.50
Mp (kip-ft) = 161.67

LINE LOADS (k/ft):

Load	Dist	DL	LL	Red%	Type	PartL
1	0.000	0.016	0.000	---	NonR	0.000
	16.500	0.016	0.000			0.000
2	0.000	0.015	0.005	0.0%	Roof	0.000
	16.500	0.015	0.005			0.000
3	0.000	0.033	0.000	---	NonR	0.000
	16.500	0.033	0.000			0.000

SHEAR (Ultimate): Max Vu (1.4DL) = 0.75 kips 1.00Vn = 84.65 kips

MOMENTS (Ultimate):

Span	Cond	LoadCombo	Mu kip-ft	@ ft	Lb ft	Cb	Phi	Phi*Mn kip-ft
Center	Max +	1.4DL	3.1	8.3	16.5	1.14	0.90	126.09
Controlling		1.4DL	3.1	8.3	16.5	1.14	0.90	126.09

REACTIONS (kips):

	Left	Right
DL reaction	0.54	0.54
Max +LL reaction	0.04	0.04
Max +total reaction (factored)	0.75	0.75

DEFLECTIONS:

				Ratio
Dead load (in)	at 8.25 ft =	-0.022	L/D = 9072	
Live load (in)	at 8.25 ft =	-0.002	L/D = 1139 > 360	0.00
			54	
Net Total load (in)	at 8.25 ft =	-0.024	L/D = 8403 > 240	0.03



Gravity Beam Design

RAM Steel 17.04.02.12
DataBase: 30479 Building 4
Building Code: IBC

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01/23/23 13:59:36
Steel Code: AISC 360-16 LRFD

Floor Type: ROOF

Beam Number = 22

SPAN INFORMATION (ft): I-End (-2.50,-18.33) J-End (17.00,-18.33)

Beam Size (User Selected) = W10X33 Fy = 50.0 ksi
Total Beam Length (ft) = 19.50
Mp (kip-ft) = 161.67

POINT LOADS (kips):

Dist	DL	RedLL	Red%	NonRLL	StorLL	Red%	RoofLL	Red%	PartL
10.830	4.89	0.00	0.0	0.00	0.00	0.0	0.75	0.0	0.00

LINE LOADS (k/ft):

Load	Dist	DL	LL	Red%	Type	PartL
1	0.000	0.016	0.000	---	NonR	0.000
	10.571	0.016	0.000			0.000
2	0.000	0.015	0.005	0.0%	Roof	0.000
	10.571	0.015	0.005			0.000
3	10.572	0.016	0.000	---	NonR	0.000
	10.830	0.000	0.000			0.000
4	10.572	0.015	0.005	0.0%	Roof	0.000
	10.830	0.000	0.000			0.000
5	0.000	0.033	0.000	---	NonR	0.000
	19.500	0.033	0.000			0.000

SHEAR (Ultimate): Max Vu (1.2DL+1.6LL) = 4.45 kips 1.00Vn = 84.65 kips

MOMENTS (Ultimate):

Span	Cond	LoadCombo	Mu kip-ft	@ ft	Lb ft	Cb	Phi	Phi*Mn kip-ft
Center	Max +	1.2DL+1.6LL	37.1	10.8	10.8	1.60	0.90	145.50
Controlling		1.2DL+1.6LL	37.1	10.8	10.8	1.60	0.90	145.50

REACTIONS (kips):

	Left	Right
DL reaction	2.75	3.13
Max +LL reaction	0.37	0.43
Max +total reaction (factored)	3.89	4.45

DEFLECTIONS:

			Ratio
Dead load (in)	at 10.04 ft =	-0.293	L/D = 799
Live load (in)	at 10.04 ft =	-0.042	L/D = 5622 > 360 0.06
Net Total load (in)	at 10.04 ft =	-0.334	L/D = 700 > 240 0.34



Gravity Beam Design

RAM Steel 17.04.02.12
 DataBase: 30479 Building 4
 Building Code: IBC

Page 4/4
 01/23/23 13:59:36
 Steel Code: AISC 360-16 LRFD

Floor Type: ROOF

Beam Number = 29

SPAN INFORMATION (ft): I-End (8.33,-34.67) J-End (8.33,-18.33)

Beam Size (User Selected) = W10X33 Fy = 50.0 ksi
 Total Beam Length (ft) = 16.34
 Mp (kip-ft) = 161.67

LINE LOADS (k/ft):

Load	Dist	DL	LL	Red%	Type	PartL
1	0.000	0.016	0.000	---	NonR	0.000
	16.081	0.016	0.000			0.000
2	0.000	0.015	0.005	0.0%	Roof	0.000
	16.081	0.015	0.005			0.000
3	16.082	0.016	0.000	---	NonR	0.000
	16.340	0.000	0.000			0.000
4	16.082	0.015	0.005	0.0%	Roof	0.000
	16.340	0.000	0.000			0.000
5	0.000	0.275	0.000	---	NonR	0.000
	16.340	0.275	0.000			0.000
6	0.000	0.260	0.087	0.0%	Roof	0.000
	16.340	0.260	0.087			0.000
7	0.000	0.033	0.000	---	NonR	0.000
	16.340	0.033	0.000			0.000

SHEAR (Ultimate): Max Vu (1.2DL+1.6LL) = 7.08 kips 1.00Vn = 84.65 kips

MOMENTS (Ultimate):

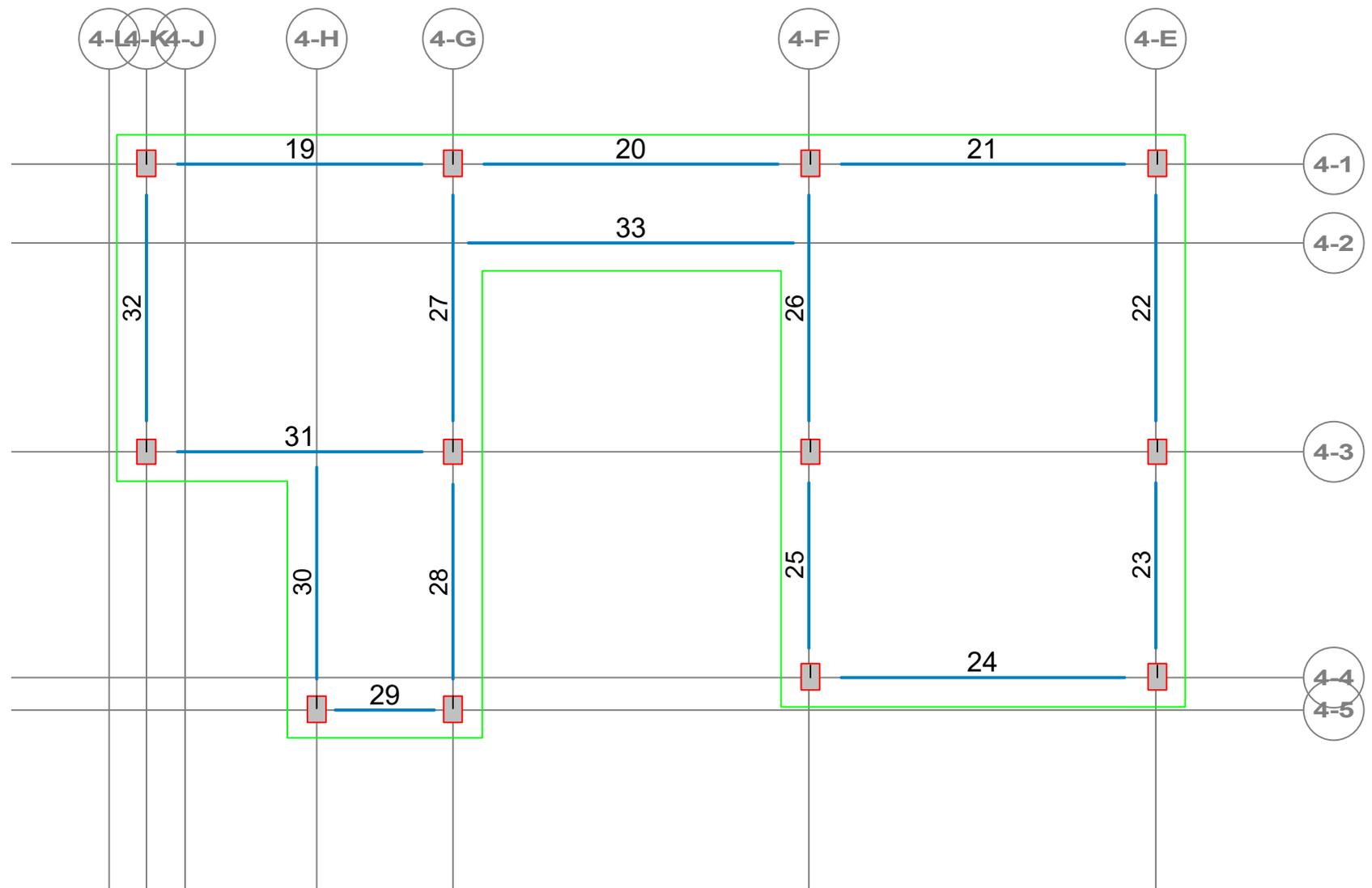
Span	Cond	LoadCombo	Mu kip-ft	@ ft	Lb ft	Cb	Phi	Phi*Mn kip-ft
Center	Max +	1.2DL+1.6LL	28.9	8.2	0.0	1.00	0.90	145.50
Controlling		1.2DL+1.6LL	28.9	8.2	0.0	1.00	0.90	145.50

REACTIONS (kips):

	Left	Right
DL reaction	4.90	4.89
Max +LL reaction	0.75	0.75
Max +total reaction (factored)	7.08	7.07

DEFLECTIONS:

				Ratio
Dead load (in)	at 8.17 ft =	-0.194	L/D = 1011	
Live load (in)	at 8.17 ft =	-0.030	L/D = 6599 > 360	0.05
Net Total load (in)	at 8.17 ft =	-0.224	L/D = 877 > 240	0.27





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BEAM INFORMATION:

Story Level _____ FIRST FLOOR
 Beam Number _____ 19 Grid Location _ (-2.50ft--0.00ft)-(-17.00ft-0.00ft)
 Beam Line Number _ 2 Span Number _ 1

Geometry

Size: _____ **42Hx22B**
 Depth (in) _____ 42.00 Web Width (in) _____ 22.00
 Flange Width (in) _____ NA Flange Thickness (in) _____ NA
 Length c-c (ft) _____ 19.50 Clear Length (ft) _____ 18.17
 Left Support Length (in) _____ 16.00 Right Support Length (in) _____ 16.00
 Left Support Width (in) _____ 32.00 Right Support Width (in) _____ 16.00

MATERIAL PROPERTIES:

f_c (ksi) _____ 5.00 f_y Longitudinal (ksi) _____ 60.00
 f_{ct} (ksi) _____ 0.00 f_{yt} Transverse (ksi) _____ 60.00
 Conc. Weight (pcf) _____ 145.00 Conc. Type _____ NWC
 Conc. Modulus (ksi) _____ 4074.28 Reinf. Modulus (ksi) _____ 29000.00

TOP LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
1	#6	3	39.500	Upper	1	0.000	1	10.000	Hooked	Splice
2	#6	3	39.500	Upper	2	-9.500	2	0.000	Splice	Hooked

Max. Bar Depth Limit (in): ___ 39.625 Clear Bar Cover (in): _____ Top: 1.500 Side: 1.500

BOTTOM LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
1	#6	3	39.500	Lower	1	0.000	1	19.500	Hooked	Hooked

Max. Bar Depth Limit (in): ___ 39.625 Clear Bar Cover (in): _____ Bot.: 1.500 Side: 1.500

LONGITUDINAL BAR DESIGN DETAILS:

Loc. (ft)	Positive Moment				Negative Moment			
	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)
0.000	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
0.667	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
1.623	11.99	232.11	0.09	1.32	0.00	-232.11	0.00	1.32
2.579	22.27	232.11	0.17	1.32	0.00	-232.11	0.00	1.32
3.535	30.85	232.11	0.23	1.32	0.00	-232.11	0.00	1.32



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Loc.	Mu	øMn	As req.	As	Mu	øMn	As req.	As
4.491	37.73	232.11	0.28	1.32	0.00	-232.11	0.00	1.32
4.873	40.00	232.11	0.30	1.32	0.00	-232.11	0.00	1.32
4.877	40.02	232.11	0.30	1.32	0.00	-232.11	0.00	1.32
5.447	42.91	232.11	0.32	1.32	0.00	-232.11	0.00	1.32
6.404	46.38	232.11	0.35	1.32	0.00	-232.11	0.00	1.32
7.360	48.15	232.11	0.36	1.32	0.00	-232.11	0.00	1.32
8.316	48.22	232.11	0.36	1.32	0.00	-232.11	0.00	1.32
9.272	46.59	232.11	0.35	1.32	0.00	-232.11	0.00	1.13
9.748	45.14	232.11	0.34	1.32	0.00	-232.11	0.00	1.35
9.752	45.13	232.11	0.34	1.32	0.00	-232.11	0.00	1.35
10.228	43.25	232.11	0.32	1.32	0.00	-232.11	0.00	1.35
11.184	38.22	232.11	0.29	1.32	0.00	-232.11	0.00	1.32
12.140	31.48	232.11	0.24	1.32	0.00	-232.11	0.00	1.32
13.096	23.03	232.11	0.17	1.32	0.00	-232.11	0.00	1.32
14.053	12.89	232.11	0.10	1.32	0.00	-232.11	0.00	1.32
14.623	6.03	232.11	0.05	1.32	0.00	-232.11	0.00	1.32
14.627	5.97	232.11	0.04	1.32	0.00	-232.11	0.00	1.32
15.009	1.04	232.11	0.01	1.32	0.00	-232.11	0.00	1.32
15.965	0.00	232.11	0.00	1.32	-12.51	-232.11	0.09	1.32
16.921	0.00	232.11	0.00	1.32	-27.76	-232.11	0.21	1.32
17.877	0.00	232.11	0.00	1.32	-44.72	-232.11	0.34	1.32
18.833	0.00	232.11	0.00	1.32	-63.37	-232.11	0.48	1.32
19.500	0.00	232.11	0.00	1.32	-63.37	-232.11	0.48	1.32

TRANSVERSE REINFORCEMENT:

Set	Size	Spacing	Num	Start		End		Stirrup	
				Supp.	Loc. (ft)	Supp.	Loc. (ft)	Legs	Type
1	#4	18.00	13	1	0.833	1	18.667	2	Closed

TRANSVERSE BAR DESIGN DETAILS AND TORSION FORCE:

Loc. (ft)	Vu (kip)	øVn (kip)	Tu (kip-ft)	Av req. (in ²)	Av prv. (in ²)
0.000	13.43	92.17	1.21	0.00	0.00
0.667	13.43	92.17	1.21	0.00	0.00
1.623	11.65	131.67	1.21	0.23	0.27
2.579	9.87	131.67	1.21	0.23	0.27
3.535	8.08	131.67	1.21	0.23	0.27
3.958	7.30	131.67	1.21	0.23	0.27
4.491	6.30	131.67	1.21	0.23	0.27
4.873	5.59	131.67	1.21	0.23	0.27
4.877	5.59	131.67	1.21	0.23	0.27
5.447	4.52	131.67	1.21	0.23	0.27
6.404	2.74	131.67	1.21	0.23	0.27



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Loc.	Vu	øVn	Tu	Av req.	Av prv.
7.360	0.96	131.67	1.21	0.23	0.27
8.316	0.82	131.67	1.21	0.23	0.27
9.272	2.60	131.67	1.21	0.23	0.27
9.748	3.48	131.67	1.21	0.23	0.27
9.752	3.49	131.67	1.21	0.23	0.27
10.228	4.38	131.67	1.21	0.23	0.27
11.184	6.16	131.67	1.21	0.23	0.27
12.140	7.94	131.67	1.21	0.23	0.27
13.096	9.72	131.67	1.21	0.23	0.27
14.053	11.50	131.67	1.21	0.23	0.27
14.623	12.56	131.67	1.21	0.23	0.27
14.627	12.57	131.67	1.21	0.23	0.27
15.009	13.28	131.67	1.21	0.23	0.27
15.542	14.27	131.67	1.21	0.23	0.27
15.965	15.06	131.67	1.21	0.23	0.27
16.921	16.84	131.67	1.21	0.23	0.27
17.877	18.62	131.67	1.21	0.23	0.27
18.833	20.40	92.17	1.21	0.00	0.00
19.500	20.40	92.17	1.21	0.00	0.00

TORSION CAPACITY:

0.75 Tn (kip-ft) _____ 29.48

Tu (kip-ft) _____ 1.21

DEFLECTIONS: (Camber = 0.000 in)

Type	Distance (ft)	Delta (in)	Ieff (in4)	Ieff/Ig	Ln/d	Status
Dead Load	8.98	0.003	135828.0	1.00	66673.0	
Live Load	12.06	0.000	135828.0	1.00	119086048.0	OK
Long Term + LL	8.98	0.006	135828.0	1.00	35903.6	OK
Net Total Load	8.98	0.009	135828.0	1.00	23336.7	

Mcr Tension Bot (kip-ft) = 285.85

Mcr Tension Top (kip-ft) = 285.85

Ig (in4) = 135828.00

λ = 1.86

Controlling Deflection Ratio (Long Term + LL) = 0.007 **OK**

Span Moments For Ieff

	Mlt (kip-ft)	Mmid (kip-ft)	Mrt(kip-ft)
Dead Load	0.01	32.24	-45.25
LL down defl	0.00	0.01	0.03
LL up defl	0.00	0.00	0.00



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BEAM INFORMATION:

Story Level _____ FIRST FLOOR
 Beam Number _____ 21 Grid Location _ (39.67ft-0.00ft)-(61.67ft-0.00ft)
 Beam Line Number _ 4 Span Number _ 1

Geometry

Size: _____ **42Hx22B**
 Depth (in) _____ 42.00 Web Width (in) _____ 22.00
 Flange Width (in) _____ NA Flange Thickness (in) _____ NA
 Length c-c (ft) _____ 22.00 Clear Length (ft) _____ 20.67
 Left Support Length (in) _____ 16.00 Right Support Length (in) _____ 16.00
 Left Support Width (in) _____ 16.00 Right Support Width (in) _____ 16.00

MATERIAL PROPERTIES:

f_c (ksi) _____ 5.00 f_y Longitudinal (ksi) _____ 60.00
 f_{ct} (ksi) _____ 0.00 f_{yt} Transverse (ksi) _____ 60.00
 Conc. Weight (pcf) _____ 145.00 Conc. Type _____ NWC
 Conc. Modulus (ksi) _____ 4074.28 Reinf. Modulus (ksi) _____ 29000.00

TOP LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
1	#6	3	39.500	Upper	1	0.000	1	11.000	Hooked	Splice
2	#6	3	39.500	Upper	2	-11.000	2	0.000	Splice	Hooked

Max. Bar Depth Limit (in): ___ 39.625 Clear Bar Cover (in): _____ Top: 1.500 Side: 1.500

BOTTOM LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
1	#6	3	39.500	Lower	1	0.000	1	22.000	Hooked	Hooked

Max. Bar Depth Limit (in): ___ 39.625 Clear Bar Cover (in): _____ Bot.: 1.500 Side: 1.500

LONGITUDINAL BAR DESIGN DETAILS:

Loc. (ft)	Positive Moment				Negative Moment			
	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)
0.000	0.00	232.11	0.00	1.32	-79.87	-232.11	0.60	1.32
0.667	0.00	232.11	0.00	1.32	-79.87	-232.11	0.60	1.32
1.651	0.00	232.11	0.00	1.32	-58.04	-232.11	0.44	1.32
2.635	0.00	232.11	0.00	1.32	-38.00	-232.11	0.28	1.32
3.619	0.00	232.11	0.00	1.32	-19.77	-232.11	0.15	1.32



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Loc.	Mu	øMn	As req.	As	Mu	øMn	As req.	As
4.603	0.00	232.11	0.00	1.32	-3.34	-232.11	0.03	1.32
5.498	10.03	232.11	0.08	1.32	0.00	-232.11	0.00	1.32
5.502	10.09	232.11	0.08	1.32	0.00	-232.11	0.00	1.32
5.587	11.28	232.11	0.08	1.32	0.00	-232.11	0.00	1.32
6.571	24.11	232.11	0.18	1.32	0.00	-232.11	0.00	1.32
7.556	35.12	232.11	0.26	1.32	0.00	-232.11	0.00	1.32
8.540	44.34	232.11	0.33	1.32	0.00	-232.11	0.00	1.32
9.524	51.75	232.11	0.39	1.32	0.00	-232.11	0.00	1.32
10.508	57.36	232.11	0.43	1.32	0.00	-232.11	0.00	0.98
10.998	59.47	232.11	0.45	1.32	0.00	-232.11	0.00	1.35
11.002	59.49	232.11	0.45	1.32	0.00	-232.11	0.00	1.35
11.492	61.16	232.11	0.46	1.32	0.00	-232.11	0.00	0.98
12.476	63.16	232.11	0.47	1.32	0.00	-232.11	0.00	1.32
13.460	63.36	232.11	0.48	1.32	0.00	-232.11	0.00	1.32
14.444	61.75	232.11	0.46	1.32	0.00	-232.11	0.00	1.32
15.429	58.34	232.11	0.44	1.32	0.00	-232.11	0.00	1.32
16.413	53.12	232.11	0.40	1.32	0.00	-232.11	0.00	1.32
16.498	52.59	232.11	0.39	1.32	0.00	-232.11	0.00	1.32
16.502	52.56	232.11	0.39	1.32	0.00	-232.11	0.00	1.32
17.397	46.11	232.11	0.35	1.32	0.00	-232.11	0.00	1.32
18.381	37.29	232.11	0.28	1.32	0.00	-232.11	0.00	1.32
19.365	26.66	232.11	0.20	1.32	0.00	-232.11	0.00	1.32
20.349	14.23	232.11	0.11	1.32	0.00	-232.11	0.00	1.32
21.333	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
22.000	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32

TRANSVERSE REINFORCEMENT:

Set	Size	Spacing	Num	Start		End		Stirrup	
				Supp.	Loc. (ft)	Supp.	Loc. (ft)	Legs	Type
1	#4	18.00	15	1	0.833	1	21.167	2	Closed

TRANSVERSE BAR DESIGN DETAILS AND TORSION FORCE:

Loc. (ft)	Vu (kip)	øVn (kip)	Tu (kip-ft)	Av req. (in ²)	Av prv. (in ²)
0.000	23.11	92.17	0.59	0.00	0.00
0.667	23.11	92.17	0.59	0.00	0.00
1.651	21.27	131.67	0.59	0.23	0.27
2.635	19.44	131.67	0.59	0.23	0.27
3.619	17.61	131.67	0.59	0.23	0.27
3.958	16.98	131.67	0.59	0.23	0.27
4.603	15.78	131.67	0.59	0.23	0.27
5.498	14.11	131.67	0.59	0.23	0.27
5.502	14.10	131.67	0.59	0.23	0.27



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Loc.	Vu	øVn	Tu	Av req.	Av prv.
5.587	13.94	131.67	0.59	0.23	0.27
6.571	12.11	131.67	0.59	0.23	0.27
7.556	10.28	131.67	0.59	0.23	0.27
8.540	8.45	131.67	0.59	0.23	0.27
9.524	6.61	131.67	0.59	0.23	0.27
10.508	4.78	131.67	0.59	0.23	0.27
10.998	3.87	131.67	0.59	0.23	0.27
11.002	3.86	131.67	0.59	0.23	0.27
11.492	2.95	131.67	0.59	0.23	0.27
12.476	1.12	131.67	0.59	0.23	0.27
13.460	0.72	131.67	0.59	0.23	0.27
14.444	2.55	131.67	0.59	0.23	0.27
15.429	4.38	131.67	0.59	0.23	0.27
16.413	6.21	131.67	0.59	0.23	0.27
16.498	6.37	131.67	0.59	0.23	0.27
16.502	6.38	131.67	0.59	0.23	0.27
17.397	8.05	131.67	0.59	0.23	0.27
18.042	9.25	131.67	0.59	0.23	0.27
18.381	9.88	131.67	0.59	0.23	0.27
19.365	11.71	131.67	0.59	0.23	0.27
20.349	13.54	131.67	0.59	0.23	0.27
21.333	15.38	92.17	0.59	0.00	0.00
22.000	15.38	92.17	0.59	0.00	0.00

TORSION CAPACITY:

0.75 Tn (kip-ft) _____ 29.48

Tu (kip-ft) _____ 0.59

DEFLECTIONS: (Camber = 0.000 in)

Type	Distance (ft)	Delta (in)	Ieff (in4)	Ieff/Ig	Ln/d	Status
Dead Load	11.87	0.006	135828.0	1.00	44555.0	
Live Load	8.39	0.000	135828.0	1.00	174588752.0	OK
Long Term + LL	11.87	0.010	135828.0	1.00	23998.1	OK
Net Total Load	11.87	0.016	135828.0	1.00	15597.2	

Mcr Tension Bot (kip-ft) = 285.85

Mcr Tension Top (kip-ft) = 285.85

Ig (in4) = 135828.00

λ = 1.86

Controlling Deflection Ratio (Long Term + LL) = 0.010 **OK**

Span Moments For Ieff

	Mlt (kip-ft)	Mmid (kip-ft)	Mrt(kip-ft)
Dead Load	-57.04	42.49	0.01
LL down defl	0.02	0.01	0.00
LL up defl	0.00	0.00	0.00



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BEAM INFORMATION: (Check Design Warnings)

Story Level _____ FIRST FLOOR

Beam Number _____ 23

Beam Line Number ___ 5

Grid Location _ (61.67ft--32.67ft)-(61.67ft--18.33ft)

Span Number _ 1

GRADE BEAM LENGTH CLASSIFIES IT AS A DEEP BEAM

Geometry

Size: _____ **42Hx22B**

Depth (in) _____ 42.00

Flange Width (in) _____ NA

Length c-c (ft) _____ 14.34

Left Support Length (in) ___ 16.00

Left Support Width (in) ___ 16.00

Web Width (in) _____ 22.00

Flange Thickness (in) _____ NA

Clear Length (ft) _____ 13.01

Right Support Length (in) ___ 16.00

Right Support Width (in) ___ 16.00

MATERIAL PROPERTIES:

f_c (ksi) _____ 5.00

f_{ct} (ksi) _____ 0.00

Conc. Weight (pcf) _____ 145.00

Conc. Modulus (ksi) _____ 4074.28

f_y Longitudinal (ksi) _____ 60.00

f_{yt} Transverse (ksi) _____ 60.00

Conc. Type _____ NWC

Reinf. Modulus (ksi) _____ 29000.00

General Warning(s):

Section must be designed as a Deep Beam per ACI 318-11 for shear. Section must be designed as a Deep Beam per ACI 318-11 for flexural design.

TOP LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Supp.	Start	End	End-Condition		
						Loc. (ft)	Supp. Loc. (ft)	Start	End	
1	#6	3	39.500	Upper	1	0.000	1	7.000	Hooked	Splice
2	#6	3	39.500	Upper	2	-7.340	2	9.660	Splice	Splice

Max. Bar Depth Limit (in): ___ 39.625 Clear Bar Cover (in): _____ Top: 1.500 Side: 1.500

BOTTOM LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Supp.	Start	End	End-Condition		
						Loc. (ft)	Supp. Loc. (ft)	Start	End	
1	#6	3	39.500	Lower	1	0.000	1	14.000	Hooked	Splice

Max. Bar Depth Limit (in): ___ 39.625 Clear Bar Cover (in): _____ Bot.: 1.500 Side: 1.500

LONGITUDINAL BAR DESIGN DETAILS:

Positive Moment					Negative Moment				
Loc. (ft)	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)	
0.000	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32	



Beam Design

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Loc.	Mu	øMn	As req.	As	Mu	øMn	As req.	As
0.667	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
1.596	19.35	232.11	0.14	1.32	0.00	-232.11	0.00	1.32
2.525	34.44	232.11	0.26	1.32	0.00	-232.11	0.00	1.32
3.454	45.26	232.11	0.34	1.32	0.00	-232.11	0.00	1.32
3.583	46.43	232.11	0.35	1.32	0.00	-232.11	0.00	1.32
3.587	46.46	232.11	0.35	1.32	0.00	-232.11	0.00	1.32
4.383	51.82	232.11	0.39	1.32	0.00	-232.11	0.00	1.32
5.312	54.11	232.11	0.41	1.32	0.00	-232.11	0.00	1.32
6.241	52.13	232.11	0.39	1.32	0.00	-232.11	0.00	1.14
7.168	45.91	232.11	0.34	1.32	0.00	-232.11	0.00	1.35
7.170	45.89	232.11	0.34	1.32	0.00	-232.11	0.00	1.35
7.172	45.87	232.11	0.34	1.32	0.00	-232.11	0.00	1.35
8.099	35.38	232.11	0.27	1.32	0.00	-232.11	0.00	1.32
9.028	20.61	232.11	0.15	1.32	0.00	-232.11	0.00	1.32
9.957	1.57	232.11	0.01	1.32	0.00	-232.11	0.00	1.32
10.753	0.00	232.11	0.00	1.32	-18.13	-232.11	0.14	1.32
10.757	0.00	232.11	0.00	1.32	-18.24	-232.11	0.14	1.32
10.886	0.00	232.11	0.00	1.32	-21.73	-232.11	0.16	1.32
11.815	0.00	232.11	0.00	1.32	-49.30	-232.11	0.37	1.32
12.744	0.00	232.11	0.00	1.32	-81.13	-232.11	0.61	1.32
13.673	0.00	232.11	0.00	1.35	-117.23	-232.11	0.88	1.32
14.340	0.00	232.11	0.00	1.35	-117.23	-232.11	0.88	1.32

TRANSVERSE REINFORCEMENT:

Set	Size	Spacing	Num	Start		End		Stirrup	
				Supp.	Loc. (ft)	Supp.	Loc. (ft)	Legs	Type
1	#4	18.00	10	1	0.833	1	13.500	2	Closed

TRANSVERSE BAR DESIGN DETAILS AND TORSION FORCE:

Loc. (ft)	Vu (kip)	øVn (kip)	Tu (kip-ft)	Av req. (in ²)	Av prv. (in ²)
0.000	23.13	92.17	0.67	0.00	0.00
0.667	23.13	92.17	0.67	0.00	0.00
1.596	18.53	131.67	0.67	0.23	0.27
2.525	13.94	131.67	0.67	0.23	0.27
3.454	9.35	131.67	0.67	0.23	0.27
3.583	8.71	131.67	0.67	0.23	0.27
3.587	8.69	131.67	0.67	0.23	0.27
3.958	6.86	131.67	0.67	0.23	0.27
4.383	4.76	131.67	0.67	0.23	0.27
5.312	0.17	131.67	0.67	0.23	0.27
6.241	4.42	131.67	0.67	0.23	0.27
7.168	9.00	131.67	0.67	0.23	0.27



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Loc.	Vu	øVn	Tu	Av req.	Av prv.
7.170	9.01	131.67	0.67	0.23	0.27
7.172	9.02	131.67	0.67	0.23	0.27
8.099	13.60	131.67	0.67	0.23	0.27
9.028	18.20	131.67	0.67	0.23	0.27
9.957	22.79	131.67	0.67	0.23	0.27
10.382	24.89	131.67	0.67	0.23	0.27
10.753	26.72	131.67	0.67	0.23	0.27
10.757	26.74	131.67	0.67	0.23	0.27
10.886	27.38	131.67	0.67	0.23	0.27
11.815	31.97	131.67	0.67	0.23	0.27
12.744	36.56	131.67	0.67	0.23	0.27
13.673	41.15	92.17	0.67	0.00	0.00
14.340	41.15	92.17	0.67	0.00	0.00

TORSION CAPACITY:

0.75 Tn (kip-ft) _____ 29.48

Tu (kip-ft) _____ 0.67

DEFLECTIONS: (Camber = 0.000 in)

Type	Distance (ft)	Delta (in)	Ieff (in4)	Ieff/Ig	Ln/d	Status
Dead Load	5.85	0.002	135828.0	1.00	89008.8	
Live Load	8.87	0.000	135828.0	1.00	29619938.0	OK
Long Term + LL	5.85	0.003	135828.0	1.00	47859.0	OK
Net Total Load	5.85	0.005	135828.0	1.00	31124.0	

Mcr Tension Bot (kip-ft) = 285.85

Mcr Tension Top (kip-ft) = 285.85

Ig (in4) = 135828.00

λ = 1.86

Controlling Deflection Ratio (Long Term + LL) = 0.005 **OK**

Span Moments For Ieff

	Mlt (kip-ft)	Mmid (kip-ft)	Mrt(kip-ft)
Dead Load	0.01	32.78	-83.71
LL down defl	0.00	0.08	0.15
LL up defl	0.00	0.00	0.00



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BEAM INFORMATION:

Story Level _____ FIRST FLOOR
 Beam Number _____ 22 Grid Location _ (61.67ft--18.33ft)-(61.67ft-0.00ft)
 Beam Line Number _ 5 Span Number _ 2

Geometry

Size: _____ **42Hx22B**
 Depth (in) _____ 42.00 Web Width (in) _____ 22.00
 Flange Width (in) _____ NA Flange Thickness (in) _____ NA
 Length c-c (ft) _____ 18.33 Clear Length (ft) _____ 17.00
 Left Support Length (in) _____ 16.00 Right Support Length (in) _____ 16.00
 Left Support Width (in) _____ 16.00 Right Support Width (in) _____ 16.00

MATERIAL PROPERTIES:

f_c (ksi) _____ 5.00 f_y Longitudinal (ksi) _____ 60.00
 f_{ct} (ksi) _____ 0.00 f_{yt} Transverse (ksi) _____ 60.00
 Conc. Weight (pcf) _____ 145.00 Conc. Type _____ NWC
 Conc. Modulus (ksi) _____ 4074.28 Reinf. Modulus (ksi) _____ 29000.00

TOP LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Supp.	Start	End	End-Condition		
						Loc. (ft)	Supp. (ft)	Loc. (ft)	Start	End
2	#6	3	39.500	Upper	2	-7.340	2	9.660	Splice	Splice
3	#6	3	39.500	Upper	3	-8.670	3	-0.003	Splice	Hooked

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Top: 1.500 Side: 1.500

BOTTOM LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Supp.	Start	End	End-Condition		
						Loc. (ft)	Supp. (ft)	Loc. (ft)	Start	End
2	#6	3	39.500	Lower	2	-0.340	2	18.327	Splice	Hooked

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Bot.: 1.500 Side: 1.500

LONGITUDINAL BAR DESIGN DETAILS:

Loc. (ft)	Positive Moment			Negative Moment				
	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)
14.340	0.00	232.11	0.00	1.35	-127.91	-232.11	0.96	1.32
15.007	0.00	232.11	0.00	1.30	-127.91	-232.11	0.96	1.32
16.006	0.00	232.11	0.00	1.32	-80.87	-232.11	0.61	1.32
17.006	0.00	232.11	0.00	1.32	-38.76	-232.11	0.29	1.32
18.006	0.00	232.11	0.00	1.32	-1.60	-232.11	0.01	1.32



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Loc.	Mu	øMn	As req.	As	Mu	øMn	As req.	As
18.920	28.07	232.11	0.21	1.32	0.00	-232.11	0.00	1.32
18.925	28.19	232.11	0.21	1.32	0.00	-232.11	0.00	1.32
19.006	30.63	232.11	0.23	1.32	0.00	-232.11	0.00	1.32
20.006	57.91	232.11	0.43	1.32	0.00	-232.11	0.00	1.32
21.005	80.26	232.11	0.60	1.32	0.00	-232.11	0.00	1.32
22.005	97.66	232.11	0.73	1.32	0.00	-232.11	0.00	1.32
23.005	110.13	232.11	0.83	1.32	0.00	-232.11	0.00	1.29
23.503	114.49	232.11	0.86	1.32	0.00	-232.11	0.00	0.98
23.507	114.52	232.11	0.86	1.32	0.00	-232.11	0.00	0.98
24.005	117.65	232.11	0.89	1.32	0.00	-232.11	0.00	1.35
25.005	120.24	232.11	0.90	1.32	0.00	-232.11	0.00	1.30
26.005	117.88	232.11	0.89	1.32	0.00	-232.11	0.00	1.32
27.004	110.58	232.11	0.83	1.32	0.00	-232.11	0.00	1.32
28.004	98.35	232.11	0.74	1.32	0.00	-232.11	0.00	1.32
28.085	97.14	232.11	0.73	1.32	0.00	-232.11	0.00	1.32
28.090	97.07	232.11	0.73	1.32	0.00	-232.11	0.00	1.32
29.004	81.17	232.11	0.61	1.32	0.00	-232.11	0.00	1.32
30.004	59.06	232.11	0.44	1.32	0.00	-232.11	0.00	1.32
31.004	32.00	232.11	0.24	1.32	0.00	-232.11	0.00	1.32
32.003	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
32.670	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

TRANSVERSE REINFORCEMENT:

Set	Size	Spacing	Num	Start		End		Stirrup	
				Supp.	Loc. (ft)	Supp.	Loc. (ft)	Legs	Type
2	#4	18.00	13	2	0.827	2	17.493	2	Closed

TRANSVERSE BAR DESIGN DETAILS AND TORSION FORCE:

Loc. (ft)	Vu (kip)	øVn (kip)	Tu (kip-ft)	Av req. (in ²)	Av prv. (in ²)
14.340	49.53	92.17	0.44	0.00	0.00
15.007	49.53	92.17	0.44	0.00	0.00
16.006	44.58	131.67	0.44	0.23	0.27
17.006	39.64	131.67	0.44	0.23	0.27
18.006	34.70	131.67	0.44	0.23	0.27
18.298	33.26	131.67	0.44	0.23	0.27
18.920	30.18	131.67	0.44	0.23	0.27
18.925	30.16	131.67	0.44	0.23	0.27
19.006	29.76	131.67	0.44	0.23	0.27
20.006	24.82	131.67	0.44	0.23	0.27
21.005	19.88	131.67	0.44	0.23	0.27
22.005	14.94	131.67	0.44	0.23	0.27
23.005	10.00	131.67	0.44	0.23	0.27



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Loc.	Vu	øVn	Tu	Av req.	Av prv.
23.503	7.54	131.67	0.44	0.23	0.27
23.507	7.52	131.67	0.44	0.23	0.27
24.005	5.06	131.67	0.44	0.23	0.27
25.005	0.11	131.67	0.44	0.23	0.27
26.005	4.83	131.67	0.44	0.23	0.27
27.004	9.77	131.67	0.44	0.23	0.27
28.004	14.71	131.67	0.44	0.23	0.27
28.085	15.11	131.67	0.44	0.23	0.27
28.090	15.13	131.67	0.44	0.23	0.27
28.712	18.21	131.67	0.44	0.23	0.27
29.004	19.65	131.67	0.44	0.23	0.27
30.004	24.59	131.67	0.44	0.23	0.27
31.004	29.53	131.67	0.44	0.23	0.27
32.003	34.47	92.17	0.44	0.00	0.00
32.670	34.47	92.17	0.44	0.00	0.00

TORSION CAPACITY:

0.75 Tn (kip-ft) _____ 29.48

Tu (kip-ft) _____ 0.44

DEFLECTIONS: (Camber = 0.000 in)

Type	Distance (ft)	Delta (in)	Ieff (in4)	Ieff/Ig	Ln/d	Status
Dead Load	9.89	0.008	135828.0	1.00	26649.6	
Live Load	6.99	0.000	135828.0	1.00	24491038.0	OK
Long Term + LL	9.89	0.015	135828.0	1.00	14065.1	OK
Net Total Load	9.89	0.022	135828.0	1.00	9206.2	

Mcr Tension Bot (kip-ft) = 285.85

Mcr Tension Top (kip-ft) = 285.85

Ig (in4) = 135828.00

λ = 1.89

Controlling Deflection Ratio (Long Term + LL) = 0.017 **OK**

Span Moments For Ieff

	Mlt (kip-ft)	Mmid (kip-ft)	Mrt(kip-ft)
Dead Load	-91.34	81.79	0.02
LL down defl	0.14	0.07	0.00
LL up defl	0.00	0.00	0.00



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BEAM INFORMATION:

Story Level _____ FIRST FLOOR

Beam Number _____ 24

Grid Location _ (39.67ft--32.67ft)-(61.67ft--32.67ft)

Beam Line Number _ 6

Span Number _ 1

Geometry

Size: _____ 42Hx22B

Depth (in) _____ 42.00

Web Width (in) _____ 22.00

Flange Width (in) _____ NA

Flange Thickness (in) _____ NA

Length c-c (ft) _____ 22.00

Clear Length (ft) _____ 20.67

Left Support Length (in) _____ 16.00

Right Support Length (in) _____ 16.00

Left Support Width (in) _____ 16.00

Right Support Width (in) _____ 16.00

MATERIAL PROPERTIES:

f_c (ksi) _____ 5.00

f_y Longitudinal (ksi) _____ 60.00

f_{ct} (ksi) _____ 0.00

f_{yt} Transverse (ksi) _____ 60.00

Conc. Weight (pcf) _____ 145.00

Conc. Type _____ NWC

Conc. Modulus (ksi) _____ 4074.28

Reinf. Modulus (ksi) _____ 29000.00

TOP LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
1	#6	3	39.500	Upper	1	0.000	1	11.000	Hooked	Splice
2	#6	3	39.500	Upper	2	-11.000	2	0.000	Splice	Hooked

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Top: 1.500 Side: 1.500

BOTTOM LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
1	#6	3	39.500	Lower	1	0.000	1	22.000	Hooked	Hooked

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Bot.: 1.500 Side: 1.500

LONGITUDINAL BAR DESIGN DETAILS:

Loc. (ft)	Positive Moment				Negative Moment			
	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)
0.000	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
0.667	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
1.651	18.03	232.11	0.14	1.32	0.00	-232.11	0.00	1.32
2.635	34.27	232.11	0.26	1.32	0.00	-232.11	0.00	1.32
3.619	48.69	232.11	0.37	1.32	0.00	-232.11	0.00	1.32



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Loc.	Mu	øMn	As req.	As	Mu	øMn	As req.	As
4.603	61.32	232.11	0.46	1.32	0.00	-232.11	0.00	1.32
5.498	71.23	232.11	0.53	1.32	0.00	-232.11	0.00	1.32
5.502	71.27	232.11	0.54	1.32	0.00	-232.11	0.00	1.32
5.587	72.14	232.11	0.54	1.32	0.00	-232.11	0.00	1.32
6.571	81.16	232.11	0.61	1.32	0.00	-232.11	0.00	1.32
7.556	88.37	232.11	0.66	1.32	0.00	-232.11	0.00	1.32
8.540	93.78	232.11	0.70	1.32	0.00	-232.11	0.00	1.32
9.524	97.39	232.11	0.73	1.32	0.00	-232.11	0.00	1.32
10.508	99.19	232.11	0.75	1.32	0.00	-232.11	0.00	0.98
10.998	99.42	232.11	0.75	1.32	0.00	-232.11	0.00	1.35
11.002	99.42	232.11	0.75	1.32	0.00	-232.11	0.00	1.35
11.492	99.19	232.11	0.75	1.32	0.00	-232.11	0.00	0.98
12.476	97.39	232.11	0.73	1.32	0.00	-232.11	0.00	1.32
13.460	93.78	232.11	0.70	1.32	0.00	-232.11	0.00	1.32
14.444	88.37	232.11	0.66	1.32	0.00	-232.11	0.00	1.32
15.429	81.16	232.11	0.61	1.32	0.00	-232.11	0.00	1.32
16.413	72.14	232.11	0.54	1.32	0.00	-232.11	0.00	1.32
16.498	71.28	232.11	0.54	1.32	0.00	-232.11	0.00	1.32
16.502	71.23	232.11	0.53	1.32	0.00	-232.11	0.00	1.32
17.397	61.32	232.11	0.46	1.32	0.00	-232.11	0.00	1.32
18.381	48.70	232.11	0.37	1.32	0.00	-232.11	0.00	1.32
19.365	34.27	232.11	0.26	1.32	0.00	-232.11	0.00	1.32
20.349	18.04	232.11	0.14	1.32	0.00	-232.11	0.00	1.32
21.333	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
22.000	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32

TRANSVERSE REINFORCEMENT:

Set	Size	Spacing	Num	Start		End		Stirrup	
				Supp.	Loc. (ft)	Supp.	Loc. (ft)	Legs	Type
1	#4	18.00	15	1	0.833	1	21.167	2	Closed

TRANSVERSE BAR DESIGN DETAILS AND TORSION FORCE:

Loc. (ft)	Vu (kip)	øVn (kip)	Tu (kip-ft)	Av req. (in ²)	Av prv. (in ²)
0.000	19.24	92.17	0.06	0.00	0.00
0.667	19.24	92.17	0.06	0.00	0.00
1.651	17.41	131.67	0.06	0.23	0.27
2.635	15.58	131.67	0.06	0.23	0.27
3.619	13.74	131.67	0.06	0.23	0.27
3.958	13.11	131.67	0.06	0.23	0.27
4.603	11.91	131.67	0.06	0.23	0.27
5.498	10.25	131.67	0.06	0.23	0.27
5.502	10.24	131.67	0.06	0.23	0.27



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Loc.	Vu	øVn	Tu	Av req.	Av prv.
5.587	10.08	131.67	0.06	0.23	0.27
6.571	8.25	131.67	0.06	0.23	0.27
7.556	6.41	131.67	0.06	0.23	0.27
8.540	4.58	131.67	0.06	0.23	0.27
9.524	2.75	131.67	0.06	0.23	0.27
10.508	0.92	131.67	0.06	0.23	0.27
10.998	0.00	131.67	0.06	0.23	0.27
11.002	0.00	131.67	0.06	0.23	0.27
11.492	0.92	131.67	0.06	0.23	0.27
12.476	2.75	131.67	0.06	0.23	0.27
13.460	4.58	131.67	0.06	0.23	0.27
14.444	6.41	131.67	0.06	0.23	0.27
15.429	8.25	131.67	0.06	0.23	0.27
16.413	10.08	131.67	0.06	0.23	0.27
16.498	10.24	131.67	0.06	0.23	0.27
16.502	10.25	131.67	0.06	0.23	0.27
17.397	11.91	131.67	0.06	0.23	0.27
18.042	13.11	131.67	0.06	0.23	0.27
18.381	13.74	131.67	0.06	0.23	0.27
19.365	15.58	131.67	0.06	0.23	0.27
20.349	17.41	131.67	0.06	0.23	0.27
21.333	19.24	92.17	0.06	0.00	0.00
22.000	19.24	92.17	0.06	0.00	0.00

TORSION CAPACITY:

0.75 Tn (kip-ft) _____ 29.48

Tu (kip-ft) _____ 0.06

DEFLECTIONS: (Camber = 0.000 in)

Type	Distance (ft)	Delta (in)	Ieff (in4)	Ieff/Ig	Ln/d	Status
Dead Load	10.71	0.010	135828.0	1.00	24175.6	
Live Load	22.00	-0.000	135828.0	1.00	2589049241	OK
					6.0	
Long Term + LL	10.71	0.019	135828.0	1.00	13023.9	OK
Net Total Load	10.71	0.029	135828.0	1.00	8464.1	

Mcr Tension Bot (kip-ft) = 285.85

Mcr Tension Top (kip-ft) = 285.85

Ig (in4) = 135828.00

λ = 1.86

Controlling Deflection Ratio (Long Term + LL) = 0.018 **OK**

Span Moments For Ieff

	Mlt (kip-ft)	Mmid (kip-ft)	Mrt(kip-ft)
Dead Load	0.01	71.01	0.01
LL down defl	-0.00	0.00	0.00
LL up defl	0.00	0.00	0.00



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BEAM INFORMATION: (Check Design Warnings)

GRADE BEAM LENGTH CLASSIFIES IT AS A DEEP BEAM

Story Level _____ FIRST FLOOR

Beam Number _____ 25

Grid Location _ (39.67ft--32.67ft)-(39.67ft--18.33ft)

Beam Line Number _ 7

Span Number _ 1

Geometry

Size: _____ 42Hx22B

Depth (in) _____ 42.00

Web Width (in) _____ 22.00

Flange Width (in) _____ NA

Flange Thickness (in) _____ NA

Length c-c (ft) _____ 14.34

Clear Length (ft) _____ 13.01

Left Support Length (in) _____ 16.00

Right Support Length (in) _____ 16.00

Left Support Width (in) _____ 16.00

Right Support Width (in) _____ 16.00

MATERIAL PROPERTIES:

f_c (ksi) _____ 5.00

f_y Longitudinal (ksi) _____ 60.00

f_{ct} (ksi) _____ 0.00

f_{yt} Transverse (ksi) _____ 60.00

Conc. Weight (pcf) _____ 145.00

Conc. Type _____ NWC

Conc. Modulus (ksi) _____ 4074.28

Reinf. Modulus (ksi) _____ 29000.00

General Warning(s):

Section must be designed as a Deep Beam per ACI 318-11 for shear. Section must be designed as a Deep Beam per ACI 318-11 for flexural design.

TOP LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Supp.	Start	End	End-Condition		
						Loc. (ft)	Supp. Loc. (ft)	Start	End	
1	#6	3	39.500	Upper	1	0.000	1	7.000	Hooked	Splice
2	#6	3	39.500	Upper	2	-7.340	2	9.660	Splice	Splice

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Top: 1.500 Side: 1.500

BOTTOM LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Supp.	Start	End	End-Condition		
						Loc. (ft)	Supp. Loc. (ft)	Start	End	
1	#6	3	39.500	Lower	1	0.000	1	14.000	Hooked	Splice

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Bot.: 1.500 Side: 1.500

LONGITUDINAL BAR DESIGN DETAILS:

Positive Moment					Negative Moment				
Loc. (ft)	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)	
0.000	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32	



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Loc.	Mu	øMn	As req.	As	Mu	øMn	As req.	As
0.667	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
1.596	17.77	232.11	0.13	1.32	0.00	-232.11	0.00	1.32
2.525	31.27	232.11	0.23	1.32	0.00	-232.11	0.00	1.32
3.454	40.50	232.11	0.30	1.32	0.00	-232.11	0.00	1.32
3.583	41.45	232.11	0.31	1.32	0.00	-232.11	0.00	1.32
3.587	41.48	232.11	0.31	1.32	0.00	-232.11	0.00	1.32
4.383	45.48	232.11	0.34	1.32	0.00	-232.11	0.00	1.32
5.312	46.18	232.11	0.35	1.32	0.00	-232.11	0.00	1.32
6.241	42.62	232.11	0.32	1.32	0.00	-232.11	0.00	1.14
7.168	34.82	232.11	0.26	1.32	0.00	-232.11	0.00	1.35
7.170	34.79	232.11	0.26	1.32	0.00	-232.11	0.00	1.35
7.172	34.77	232.11	0.26	1.32	0.00	-232.11	0.00	1.35
8.099	22.70	232.11	0.17	1.32	0.00	-232.11	0.00	1.32
9.028	6.35	232.11	0.05	1.32	0.00	-232.11	0.00	1.32
9.957	0.00	232.11	0.00	1.32	-14.28	-232.11	0.11	1.32
10.753	0.00	232.11	0.00	1.32	-35.33	-232.11	0.26	1.32
10.757	0.00	232.11	0.00	1.32	-35.45	-232.11	0.27	1.32
10.886	0.00	232.11	0.00	1.32	-39.16	-232.11	0.29	1.32
11.815	0.00	232.11	0.00	1.32	-68.32	-232.11	0.51	1.32
12.744	0.00	232.11	0.00	1.32	-101.74	-232.11	0.76	1.32
13.673	0.00	258.74	0.00	1.50	-139.42	-232.11	1.05	1.32
14.340	0.00	282.20	0.00	1.64	-139.42	-232.11	1.05	1.32

TRANSVERSE REINFORCEMENT:

Set	Size	Spacing	Num	Start		End		Stirrup	
				Supp.	Loc. (ft)	Supp.	Loc. (ft)	Legs	Type
1	#4	18.00	10	1	0.833	1	13.500	2	Closed

TRANSVERSE BAR DESIGN DETAILS AND TORSION FORCE:

Loc. (ft)	Vu (kip)	øVn (kip)	Tu (kip-ft)	Av req. (in ²)	Av prv. (in ²)
0.000	21.42	92.17	0.71	0.00	0.00
0.667	21.42	92.17	0.71	0.00	0.00
1.596	16.83	131.67	0.71	0.23	0.27
2.525	12.24	131.67	0.71	0.23	0.27
3.454	7.65	131.67	0.71	0.23	0.27
3.583	7.01	131.67	0.71	0.23	0.27
3.587	6.99	131.67	0.71	0.23	0.27
3.958	5.15	131.67	0.71	0.23	0.27
4.383	3.06	131.67	0.71	0.23	0.27
5.312	1.54	131.67	0.71	0.23	0.27
6.241	6.13	131.67	0.71	0.23	0.27
7.168	10.71	131.67	0.71	0.23	0.27



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Loc.	Vu	øVn	Tu	Av req.	Av prv.
7.170	10.72	131.67	0.71	0.23	0.27
7.172	10.73	131.67	0.71	0.23	0.27
8.099	15.31	131.67	0.71	0.23	0.27
9.028	19.90	131.67	0.71	0.23	0.27
9.957	24.49	131.67	0.71	0.23	0.27
10.382	26.59	131.67	0.71	0.23	0.27
10.753	28.43	131.67	0.71	0.23	0.27
10.757	28.45	131.67	0.71	0.23	0.27
10.886	29.08	131.67	0.71	0.23	0.27
11.815	33.68	131.67	0.71	0.23	0.27
12.744	38.27	131.67	0.71	0.23	0.27
13.673	42.86	92.17	0.71	0.00	0.00
14.340	42.86	92.17	0.71	0.00	0.00

TORSION CAPACITY:

0.75 Tn (kip-ft) _____ 29.48

Tu (kip-ft) _____ 0.71

DEFLECTIONS: (Camber = 0.000 in)

Type	Distance (ft)	Delta (in)	Ieff (in4)	Ieff/Ig	Ln/d	Status
Dead Load	5.09	0.001	135828.0	1.00	126955.7	
Live Load	9.25	0.000	135828.0	1.00	28921618.0	OK
Long Term + LL	5.09	0.002	135828.0	1.00	68237.4	OK
Net Total Load	5.09	0.004	135828.0	1.00	44382.4	

Mcr Tension Bot (kip-ft) = 285.85

Mcr Tension Top (kip-ft) = 285.85

Ig (in4) = 135828.00

λ = 1.86

Controlling Deflection Ratio (Long Term + LL) = 0.004 **OK**

Span Moments For Ieff

	Mlt (kip-ft)	Mmid (kip-ft)	Mrt(kip-ft)
Dead Load	0.01	24.85	-99.56
LL down defl	0.00	0.08	0.16
LL up defl	0.00	0.00	0.00



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BEAM INFORMATION:

Story Level _____ FIRST FLOOR
 Beam Number _____ 26 Grid Location _ (39.67ft--18.33ft)-(39.67ft-0.00ft)
 Beam Line Number _ 7 Span Number _ 2

Geometry

Size: _____ **42Hx22B**
 Depth (in) _____ 42.00 Web Width (in) _____ 22.00
 Flange Width (in) _____ NA Flange Thickness (in) _____ NA
 Length c-c (ft) _____ 18.33 Clear Length (ft) _____ 17.00
 Left Support Length (in) _____ 16.00 Right Support Length (in) _____ 16.00
 Left Support Width (in) _____ 16.00 Right Support Width (in) _____ 16.00

MATERIAL PROPERTIES:

f_c (ksi) _____ 5.00 f_y Longitudinal (ksi) _____ 60.00
 f_{ct} (ksi) _____ 0.00 f_{yt} Transverse (ksi) _____ 60.00
 Conc. Weight (pcf) _____ 145.00 Conc. Type _____ NWC
 Conc. Modulus (ksi) _____ 4074.28 Reinf. Modulus (ksi) _____ 29000.00

TOP LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
2	#6	3	39.500	Upper	2	-7.340	2	9.660	Splice	Splice
3	#6	3	39.500	Upper	3	-8.670	3	-0.003	Splice	Hooked

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Top: 1.500 Side: 1.500

BOTTOM LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
2	#6	4	39.500	Lower	2	-0.340	2	18.327	Splice	Hooked

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Bot.: 1.500 Side: 1.500

LONGITUDINAL BAR DESIGN DETAILS:

Loc. (ft)	Positive Moment			Negative Moment				
	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)
14.340	0.00	282.21	0.00	1.64	-158.64	-232.11	1.20	1.32
15.007	0.00	305.67	0.00	1.73	-158.64	-232.11	1.20	1.32
16.006	0.00	308.37	0.00	1.76	-103.20	-232.11	0.78	1.32
17.006	0.00	308.37	0.00	1.76	-52.70	-232.11	0.40	1.32
18.006	0.00	308.37	0.00	1.76	-7.14	-232.11	0.05	1.32



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Loc.	Mu	øMn	As req.	As	Mu	øMn	As req.	As
19.006	33.48	308.37	0.25	1.76	0.00	-232.11	0.00	1.32
20.006	69.16	308.37	0.52	1.76	0.00	-232.11	0.00	1.32
21.005	99.90	308.37	0.75	1.76	0.00	-232.11	0.00	1.32
22.005	125.71	308.37	0.95	1.76	0.00	-232.11	0.00	1.32
23.005	146.57	308.37	1.10	1.76	0.00	-232.11	0.00	1.29
24.005	162.49	308.37	1.22	1.76	0.00	-232.11	0.00	1.35
25.005	173.46	308.37	1.31	1.76	0.00	-232.11	0.00	1.30
26.005	179.50	308.37	1.35	1.76	0.00	-232.11	0.00	1.32
27.004	180.68	308.37	1.36	1.76	0.00	-232.11	0.00	1.32
27.668	178.89	308.37	1.35	1.76	0.00	-232.11	0.00	1.32
27.672	178.87	308.37	1.35	1.76	0.00	-232.11	0.00	1.32
28.004	170.20	308.37	1.28	1.76	0.00	-232.11	0.00	1.32
29.004	139.05	308.37	1.05	1.76	0.00	-232.11	0.00	1.32
30.004	100.30	308.37	0.75	1.76	0.00	-232.11	0.00	1.32
31.004	53.95	308.37	0.40	1.76	0.00	-232.11	0.00	1.32
32.003	0.00	308.37	0.00	1.76	0.00	-232.11	0.00	1.32
32.670	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

TRANSVERSE REINFORCEMENT:

Set	Size	Spacing	Num	Start		End		Stirrup	
				Supp.	Loc. (ft)	Supp.	Loc. (ft)	Legs	Type
2	#4	18.00	13	2	0.827	2	17.493	2	Closed

TRANSVERSE BAR DESIGN DETAILS AND TORSION FORCE:

Loc. (ft)	Vu (kip)	øVn (kip)	Tu (kip-ft)	Av req. (in ²)	Av prv. (in ²)
14.340	57.92	92.17	0.24	0.00	0.00
15.007	57.92	92.17	0.24	0.00	0.00
16.006	52.98	131.67	0.24	0.23	0.27
17.006	48.04	131.67	0.24	0.23	0.27
18.006	43.10	131.67	0.24	0.23	0.27
18.298	41.66	131.67	0.24	0.23	0.27
19.006	38.16	131.67	0.24	0.23	0.27
20.006	33.22	131.67	0.24	0.23	0.27
21.005	28.28	131.67	0.24	0.23	0.27
22.005	23.33	131.67	0.24	0.23	0.27
23.005	18.39	131.67	0.24	0.23	0.27
24.005	13.45	131.67	0.24	0.23	0.27
25.005	8.51	131.67	0.24	0.23	0.27
26.005	3.57	131.67	0.24	0.23	0.27
27.004	1.18	131.67	0.24	0.23	0.27
27.668	4.18	131.67	0.24	0.23	0.27
27.672	24.83	131.67	0.24	0.23	0.27



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Loc.	Vu	øVn	Tu	Av req.	Av prv.
28.004	27.36	131.67	0.24	0.23	0.27
28.712	32.74	131.67	0.24	0.23	0.27
29.004	34.96	131.67	0.24	0.23	0.27
30.004	42.56	131.67	0.24	0.23	0.27
31.004	50.16	131.67	0.24	0.23	0.27
32.003	57.76	92.17	0.24	0.00	0.00
32.670	57.76	92.17	0.24	0.00	0.00

TORSION CAPACITY:

0.75 Tn (kip-ft) _____ 29.48

Tu (kip-ft) _____ 0.24

DEFLECTIONS: (Camber = 0.000 in)

Type	Distance (ft)	Delta (in)	Ieff (in4)	Ieff/Ig	Ln/d	Status
Dead Load	10.37	0.011	135828.0	1.00	18577.8	
Live Load	6.99	0.000	135828.0	1.00	25617082.0	OK
Long Term + LL	10.37	0.021	135828.0	1.00	9807.8	OK
Net Total Load	10.37	0.032	135828.0	1.00	6419.0	

Mcr Tension Bot (kip-ft) = 285.85

Mcr Tension Top (kip-ft) = 285.85

Ig (in4) = 135828.00

λ = 1.89

Controlling Deflection Ratio (Long Term + LL) = 0.024 **OK**

Span Moments For Ieff

	Mlt (kip-ft)	Mmid (kip-ft)	Mrt(kip-ft)
Dead Load	-113.28	110.82	0.04
LL down defl	0.13	0.06	0.00
LL up defl	0.00	0.00	0.00



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BEAM INFORMATION:

Story Level _____ FIRST FLOOR

Beam Number _____ 28

Grid Location _ (17.00ft--34.67ft)-(17.00ft--18.33ft)

Beam Line Number _ 8

Span Number _ 1

Geometry

Size: _____ **42Hx22B**

Depth (in) _____ 42.00

Web Width (in) _____ 22.00

Flange Width (in) _____ NA

Flange Thickness (in) _____ NA

Length c-c (ft) _____ 16.34

Clear Length (ft) _____ 15.01

Left Support Length (in) _____ 16.00

Right Support Length (in) _____ 16.00

Left Support Width (in) _____ 16.00

Right Support Width (in) _____ 16.00

MATERIAL PROPERTIES:

f_c (ksi) _____ 5.00

f_y Longitudinal (ksi) _____ 60.00

f_{ct} (ksi) _____ 0.00

f_{yt} Transverse (ksi) _____ 60.00

Conc. Weight (pcf) _____ 145.00

Conc. Type _____ NWC

Conc. Modulus (ksi) _____ 4074.28

Reinf. Modulus (ksi) _____ 29000.00

TOP LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Supp.	Start		End		End-Condition	
						Loc. (ft)	Supp.	Loc. (ft)	Supp.	Start	End
1	#5	3	39.500	Upper	1	0.000	1	8.000	Hooked	Splice	
2	#6	3	39.500	Upper	2	-8.340	2	9.660	Splice	Splice	

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Top: 1.500 Side: 1.500

BOTTOM LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Supp.	Start		End		End-Condition	
						Loc. (ft)	Supp.	Loc. (ft)	Supp.	Start	End
1	#5	3	39.500	Lower	1	0.000	1	16.000	Hooked	Splice	

Max. Bar Depth Limit (in): _____ 39.688 Clear Bar Cover (in): _____ Bot.: 1.500 Side: 1.500

LONGITUDINAL BAR DESIGN DETAILS:

Loc. (ft)	Positive Moment				Negative Moment			
	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)
0.000	0.00	164.06	0.00	0.93	0.00	-164.06	0.00	0.93
0.667	0.00	164.06	0.00	0.93	0.00	-164.06	0.00	0.93
1.605	12.51	164.06	0.09	0.93	0.00	-164.06	0.00	0.93
2.542	22.31	164.06	0.17	0.93	0.00	-164.06	0.00	0.93
3.480	29.41	164.06	0.22	0.93	0.00	-164.06	0.00	0.93



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Loc.	Mu	øMn	As req.	As	Mu	øMn	As req.	As
4.083	32.54	164.06	0.24	0.93	0.00	-164.06	0.00	0.93
4.087	32.55	164.06	0.24	0.93	0.00	-164.06	0.00	0.93
4.418	33.80	164.06	0.25	0.93	0.00	-164.06	0.00	0.93
5.356	35.48	164.06	0.27	0.93	0.00	-164.06	0.00	0.93
6.294	34.46	164.06	0.26	0.93	0.00	-164.06	0.00	0.93
7.232	30.73	164.06	0.23	0.93	0.00	-173.97	0.00	0.81
8.168	24.32	164.06	0.18	0.93	0.00	-203.36	0.00	1.18
8.170	24.30	164.06	0.18	0.93	0.00	-203.43	0.00	1.18
8.172	24.28	164.06	0.18	0.93	0.00	-203.49	0.00	1.18
9.108	15.16	164.06	0.11	0.93	0.00	-232.11	0.00	1.32
10.046	3.32	164.06	0.02	0.93	0.00	-232.11	0.00	1.32
10.984	0.00	164.06	0.00	0.93	-11.23	-232.11	0.08	1.32
11.922	0.00	164.06	0.00	0.93	-28.49	-232.11	0.21	1.32
12.253	0.00	164.06	0.00	0.93	-35.23	-232.11	0.26	1.32
12.257	0.00	164.06	0.00	0.93	-35.32	-232.11	0.26	1.32
12.860	0.00	164.06	0.00	0.93	-48.45	-232.11	0.36	1.32
13.797	0.00	164.06	0.00	0.93	-71.12	-232.11	0.53	1.32
14.735	0.00	164.06	0.00	0.93	-96.49	-232.11	0.73	1.32
15.673	0.00	214.46	0.00	1.24	-124.57	-232.11	0.94	1.32
16.340	0.00	258.85	0.00	1.50	-124.57	-232.11	0.94	1.32

TRANSVERSE REINFORCEMENT:

Set	Size	Spacing	Num	Start		End		Stirrup	
				Supp.	Loc. (ft)	Supp.	Loc. (ft)	Legs	Type
1	#4	18.00	11	1	0.833	1	15.500	2	Closed

TRANSVERSE BAR DESIGN DETAILS AND TORSION FORCE:

Loc. (ft)	Vu (kip)	øVn (kip)	Tu (kip-ft)	Av req. (in ²)	Av prv. (in ²)
0.000	14.78	92.17	0.58	0.00	0.00
0.667	14.78	92.17	0.58	0.00	0.00
1.605	11.89	131.67	0.58	0.23	0.27
2.542	9.01	131.67	0.58	0.23	0.27
3.480	6.12	131.67	0.58	0.23	0.27
3.958	4.65	131.67	0.58	0.23	0.27
4.083	4.27	131.67	0.58	0.23	0.27
4.087	4.26	131.67	0.58	0.23	0.27
4.418	3.24	131.67	0.58	0.23	0.27
5.356	0.35	131.67	0.58	0.23	0.27
6.294	2.53	131.67	0.58	0.23	0.27
7.232	5.42	131.67	0.58	0.23	0.27
8.168	8.29	131.67	0.58	0.23	0.27
8.170	8.30	131.67	0.58	0.23	0.27



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Loc.	Vu	øVn	Tu	Av req.	Av prv.
8.172	8.31	131.67	0.58	0.23	0.27
9.108	11.19	131.67	0.58	0.23	0.27
10.046	14.07	131.67	0.58	0.23	0.27
10.984	16.96	131.67	0.58	0.23	0.27
11.922	19.84	131.67	0.58	0.23	0.27
12.253	20.86	131.67	0.58	0.23	0.27
12.257	20.87	131.67	0.58	0.23	0.27
12.382	21.26	131.67	0.58	0.23	0.27
12.860	22.73	131.67	0.58	0.23	0.27
13.797	25.61	131.67	0.58	0.23	0.27
14.735	28.50	131.67	0.58	0.23	0.27
15.673	31.38	92.17	0.58	0.00	0.00
16.340	31.38	92.17	0.58	0.00	0.00

TORSION CAPACITY:

0.75 Tn (kip-ft) _____ 29.48

Tu (kip-ft) _____ 0.58

DEFLECTIONS: (Camber = 0.000 in)

Type	Distance (ft)	Delta (in)	Ieff (in4)	Ieff/Ig	Ln/d	Status
Dead Load	5.38	0.001	135828.0	1.00	180491.8	
Live Load	10.10	0.000	135828.0	1.00	35981860.0	OK
Long Term + LL	5.38	0.002	135828.0	1.00	96130.2	OK
Net Total Load	5.38	0.003	135828.0	1.00	62723.6	

Mcr Tension Bot (kip-ft) = 285.85

Mcr Tension Top (kip-ft) = 285.85

Ig (in4) = 135828.00

λ = 1.87

Controlling Deflection Ratio (Long Term + LL) = 0.002 **OK**

Span Moments For Ieff

	Mlt (kip-ft)	Mmid (kip-ft)	Mrt(kip-ft)
Dead Load	0.01	17.36	-88.96
LL down defl	0.00	0.05	0.11
LL up defl	0.00	0.00	0.00



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BEAM INFORMATION:

Story Level _____ FIRST FLOOR
 Beam Number _____ 27 Grid Location _ (17.00ft--18.33ft)-(17.00ft-0.00ft)
 Beam Line Number _ 8 Span Number _ 2

Geometry

Size: _____ **42Hx22B**
 Depth (in) _____ 42.00 Web Width (in) _____ 22.00
 Flange Width (in) _____ NA Flange Thickness (in) _____ NA
 Length c-c (ft) _____ 18.33 Clear Length (ft) _____ 17.00
 Left Support Length (in) _____ 16.00 Right Support Length (in) _____ 16.00
 Left Support Width (in) _____ 16.00 Right Support Width (in) _____ 16.00

MATERIAL PROPERTIES:

f_c (ksi) _____ 5.00 f_y Longitudinal (ksi) _____ 60.00
 f_{ct} (ksi) _____ 0.00 f_{yt} Transverse (ksi) _____ 60.00
 Conc. Weight (pcf) _____ 145.00 Conc. Type _____ NWC
 Conc. Modulus (ksi) _____ 4074.28 Reinf. Modulus (ksi) _____ 29000.00

TOP LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
2	#6	3	39.500	Upper	2	-8.340	2	9.660	Splice	Splice
3	#5	3	39.500	Upper	3	-8.670	3	-0.003	Splice	Hooked

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Top: 1.500 Side: 1.500

BOTTOM LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
2	#6	4	39.500	Lower	2	-0.340	2	18.327	Splice	Hooked

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Bot.: 1.500 Side: 1.500

LONGITUDINAL BAR DESIGN DETAILS:

Loc. (ft)	Positive Moment				Negative Moment			
	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)
16.340	0.00	258.86	0.00	1.50	-142.42	-232.11	1.07	1.32
17.007	0.00	303.26	0.00	1.73	-142.42	-232.11	1.07	1.32
18.006	0.00	308.37	0.00	1.76	-90.74	-232.11	0.68	1.32
19.006	0.00	308.37	0.00	1.76	-43.63	-232.11	0.33	1.32
20.006	0.00	308.37	0.00	1.76	-1.12	-232.11	0.01	1.32



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Loc.	Mu	øMn	As req.	As	Mu	øMn	As req.	As
21.006	36.80	308.37	0.28	1.76	0.00	-232.11	0.00	1.32
22.006	70.13	308.37	0.53	1.76	0.00	-232.11	0.00	1.32
23.005	98.88	308.37	0.74	1.76	0.00	-232.11	0.00	1.32
24.005	123.03	308.37	0.93	1.76	0.00	-232.11	0.00	1.32
25.005	142.59	308.37	1.07	1.76	0.00	-229.34	0.00	1.29
26.005	157.56	308.37	1.19	1.76	0.00	-197.93	0.00	1.15
27.005	167.94	308.37	1.27	1.76	0.00	-166.53	0.00	0.91
28.005	173.73	308.37	1.31	1.76	0.00	-164.06	0.00	0.93
29.004	175.00	308.37	1.32	1.76	0.00	-164.06	0.00	0.93
29.668	173.47	308.37	1.31	1.76	0.00	-164.06	0.00	0.93
29.672	173.38	308.37	1.31	1.76	0.00	-164.06	0.00	0.93
30.004	164.91	308.37	1.24	1.76	0.00	-164.06	0.00	0.93
31.004	134.55	308.37	1.01	1.76	0.00	-164.06	0.00	0.93
32.004	96.95	308.37	0.73	1.76	0.00	-164.06	0.00	0.93
33.004	52.10	308.37	0.39	1.76	0.00	-164.06	0.00	0.93
34.003	0.00	308.37	0.00	1.76	0.00	-164.06	0.00	0.93
34.670	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

TRANSVERSE REINFORCEMENT:

Set	Size	Spacing	Num	Start		End		Stirrup	
				Supp.	Loc. (ft)	Supp.	Loc. (ft)	Legs	Type
2	#4	18.00	13	2	0.827	2	17.493	2	Closed

TRANSVERSE BAR DESIGN DETAILS AND TORSION FORCE:

Loc. (ft)	Vu (kip)	øVn (kip)	Tu (kip-ft)	Av req. (in ²)	Av prv. (in ²)
16.340	54.00	92.17	0.70	0.00	0.00
17.007	54.00	92.17	0.70	0.00	0.00
18.006	49.41	131.67	0.70	0.23	0.27
19.006	44.82	131.67	0.70	0.23	0.27
20.006	40.23	131.67	0.70	0.23	0.27
20.298	38.88	131.67	0.70	0.23	0.27
21.006	35.63	131.67	0.70	0.23	0.27
22.006	31.04	131.67	0.70	0.23	0.27
23.005	26.45	131.67	0.70	0.23	0.27
24.005	21.86	131.67	0.70	0.23	0.27
25.005	17.27	131.67	0.70	0.23	0.27
26.005	12.68	131.67	0.70	0.23	0.27
27.005	8.09	131.67	0.70	0.23	0.27
28.005	3.50	131.67	0.70	0.23	0.27
29.004	0.90	131.67	0.70	0.23	0.27
29.668	3.67	131.67	0.70	0.23	0.27
29.672	24.33	131.67	0.70	0.23	0.27



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Loc.	Vu	øVn	Tu	Av req.	Av prv.
30.004	26.73	131.67	0.70	0.23	0.27
30.712	31.86	131.67	0.70	0.23	0.27
31.004	33.98	131.67	0.70	0.23	0.27
32.004	41.23	131.67	0.70	0.23	0.27
33.004	48.48	131.67	0.70	0.23	0.27
34.003	55.73	92.17	0.70	0.00	0.00
34.670	55.73	92.17	0.70	0.00	0.00

TORSION CAPACITY:

0.75 Tn (kip-ft) _____ 29.48

Tu (kip-ft) _____ 0.70

DEFLECTIONS: (Camber = 0.000 in)

Type	Distance (ft)	Delta (in)	Ieff (in4)	Ieff/Ig	Ln/d	Status
Dead Load	10.37	0.011	135828.0	1.00	18988.8	
Live Load	6.99	0.000	135828.0	1.00	37586780.0	OK
Long Term + LL	10.37	0.020	135828.0	1.00	10026.4	OK
Net Total Load	10.37	0.031	135828.0	1.00	6561.7	

Mcr Tension Bot (kip-ft) = 285.85

Mcr Tension Top (kip-ft) = 285.85

Ig (in4) = 135828.00

λ = 1.89

Controlling Deflection Ratio (Long Term + LL) = 0.024 **OK**

Span Moments For Ieff

	Mlt (kip-ft)	Mmid (kip-ft)	Mrt(kip-ft)
Dead Load	-101.70	107.60	0.04
LL down defl	0.09	0.04	0.00
LL up defl	0.00	0.00	0.00



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BEAM INFORMATION: (Check Design Warnings)

GRADE BEAM LENGTH CLASSIFIES IT AS A DEEP BEAM

Story Level _____ FIRST FLOOR

Beam Number _____ 29

Beam Line Number ___ 9

Grid Location _ (8.33ft--34.67ft)-(17.00ft--34.67ft)

Span Number _ 1

Geometry

Size: _____ 42Hx22B

Depth (in) _____ 42.00

Flange Width (in) _____ NA

Length c-c (ft) _____ 8.67

Left Support Length (in) ___ 16.00

Left Support Width (in) ___ 16.00

Web Width (in) _____ 22.00

Flange Thickness (in) _____ NA

Clear Length (ft) _____ 7.34

Right Support Length (in) ___ 16.00

Right Support Width (in) ___ 16.00

MATERIAL PROPERTIES:

f_c (ksi) _____ 5.00

f_{ct} (ksi) _____ 0.00

Conc. Weight (pcf) _____ 145.00

Conc. Modulus (ksi) _____ 4074.28

f_y Longitudinal (ksi) _____ 60.00

f_{yt} Transverse (ksi) _____ 60.00

Conc. Type _____ NWC

Reinf. Modulus (ksi) _____ 29000.00

General Warning(s):

Section must be designed as a Deep Beam per ACI 318-11 for shear. Section must be designed as a Deep Beam per ACI 318-11 for flexural design.

TOP LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Supp.	Start	End	End-Condition		
						Loc. (ft)	Supp. Loc. (ft)	Start	End	
1	#6	3	39.500	Upper	1	0.000	1	4.000	Hooked	Splice
2	#6	3	39.500	Upper	2	-4.670	2	-0.003	Splice	Hooked

Max. Bar Depth Limit (in): ___ 39.625 Clear Bar Cover (in): _____ Top: 1.500 Side: 1.500

BOTTOM LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Supp.	Start	End	End-Condition		
						Loc. (ft)	Supp. Loc. (ft)	Start	End	
1	#6	3	39.500	Lower	1	0.000	1	8.667	Hooked	Hooked

Max. Bar Depth Limit (in): ___ 39.625 Clear Bar Cover (in): _____ Bot.: 1.500 Side: 1.500

LONGITUDINAL BAR DESIGN DETAILS:

Positive Moment					Negative Moment				
Loc. (ft)	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)	
0.000	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32	



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Loc.	Mu	øMn	As req.	As	Mu	øMn	As req.	As
0.667	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
1.482	4.95	232.11	0.04	1.32	0.00	-232.11	0.00	1.32
2.165	8.15	232.11	0.06	1.32	0.00	-232.11	0.00	1.32
2.170	8.16	232.11	0.06	1.32	0.00	-232.11	0.00	1.32
2.297	8.66	232.11	0.06	1.32	0.00	-232.11	0.00	1.32
3.112	11.14	232.11	0.08	1.32	0.00	-232.11	0.00	1.22
3.927	12.37	232.11	0.09	1.32	0.00	-232.11	0.00	1.35
4.333	12.53	232.11	0.09	1.32	0.00	-232.11	0.00	1.35
4.337	12.53	232.11	0.09	1.32	0.00	-232.11	0.00	1.35
4.743	12.37	232.11	0.09	1.32	0.00	-232.11	0.00	1.13
5.558	11.14	232.11	0.08	1.32	0.00	-232.11	0.00	1.32
6.373	8.66	232.11	0.06	1.32	0.00	-232.11	0.00	1.32
6.500	8.16	232.11	0.06	1.32	0.00	-232.11	0.00	1.32
6.505	8.15	232.11	0.06	1.32	0.00	-232.11	0.00	1.32
7.188	4.95	232.11	0.04	1.32	0.00	-232.11	0.00	1.32
8.003	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
8.670	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

TRANSVERSE REINFORCEMENT:

Set	Size	Spacing	Num	Start		End		Stirrup	
				Supp.	Loc. (ft)	Supp.	Loc. (ft)	Legs	Type
1	#4	18.00	6	1	0.833	1	7.833	2	Closed

TRANSVERSE BAR DESIGN DETAILS AND TORSION FORCE:

Loc. (ft)	Vu (kip)	øVn (kip)	Tu (kip-ft)	Av req. (in ²)	Av prv. (in ²)
0.000	6.83	92.17	0.53	0.00	0.00
0.667	6.83	92.17	0.53	0.00	0.00
1.482	5.31	131.67	0.53	0.23	0.27
2.165	4.04	131.67	0.53	0.23	0.27
2.170	4.03	131.67	0.53	0.23	0.27
2.297	3.80	131.67	0.53	0.23	0.27
3.112	2.28	131.67	0.53	0.23	0.27
3.927	0.76	131.67	0.53	0.23	0.27
3.958	0.70	131.67	0.53	0.23	0.27
4.333	0.00	131.67	0.53	0.23	0.27
4.337	0.00	131.67	0.53	0.23	0.27
4.712	0.70	131.67	0.53	0.23	0.27
4.743	0.76	131.67	0.53	0.23	0.27
5.558	2.28	131.67	0.53	0.23	0.27
6.373	3.79	131.67	0.53	0.23	0.27
6.500	4.03	131.67	0.53	0.23	0.27
6.505	4.04	131.67	0.53	0.23	0.27



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Loc.	Vu	øVn	Tu	Av req.	Av prv.
7.188	5.31	131.67	0.53	0.23	0.27
8.003	6.83	92.17	0.53	0.00	0.00
8.670	6.83	92.17	0.53	0.00	0.00

TORSION CAPACITY:

0.75 Tn (kip-ft) _____ 29.48

Tu (kip-ft) _____ 0.53

DEFLECTIONS: (Camber = 0.000 in)

Type	Distance (ft)	Delta (in)	Ieff (in4)	Ieff/Ig	Ln/d	Status
Dead Load	4.22	0.000	135828.0	1.00	345703.2	
Live Load	0.00	0.000	135828.0	1.00	374210528.0	OK
Long Term + LL	4.22	0.000	135828.0	1.00	186220.9	OK
Net Total Load	4.22	0.001	135828.0	1.00	121027.0	

Mcr Tension Bot (kip-ft) = 285.85

Mcr Tension Top (kip-ft) = 285.85

Ig (in4) = 135828.00

λ = 1.86

Controlling Deflection Ratio (Long Term + LL) = 0.001 **OK**

Span Moments For Ieff

	Mlt (kip-ft)	Mmid (kip-ft)	Mrt(kip-ft)
Dead Load	0.00	8.95	0.00
LL down defl	0.00	0.00	0.00
LL up defl	0.00	0.00	0.00



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BEAM INFORMATION:

Story Level _____ FIRST FLOOR
 Beam Number _____ 30 Grid Location _ (8.33ft--34.67ft)-(8.33ft--18.33ft)
 Beam Line Number _ 10 Span Number _ 1

Geometry

Size: _____	42Hx22B		
Depth (in) _____	42.00	Web Width (in) _____	22.00
Flange Width (in) _____	NA	Flange Thickness (in) _____	NA
Length c-c (ft) _____	16.34	Clear Length (ft) _____	14.76
Left Support Length (in) _____	16.00	Right Support Length (in) _____	22.00
Left Support Width (in) _____	16.00	Right Support Width (in) _____	NA

MATERIAL PROPERTIES:

f_c (ksi) _____	5.00	f_y Longitudinal (ksi) _____	60.00
f_{ct} (ksi) _____	0.00	f_{yt} Transverse (ksi) _____	60.00
Conc. Weight (pcf) _____	145.00	Conc. Type _____	NWC
Conc. Modulus (ksi) _____	4074.28	Reinf. Modulus (ksi) _____	29000.00

TOP LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
1	#6	3	39.500	Upper	1	0.000	1	8.000	Hooked	Splice
2	#6	3	39.500	Upper	2	-8.340	2	-0.007	Splice	Hooked

Max. Bar Depth Limit (in): ___ 39.625 Clear Bar Cover (in): _____ Top: 1.500 Side: 1.500

BOTTOM LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
1	#6	3	39.500	Lower	1	0.000	1	16.333	Hooked	Hooked

Max. Bar Depth Limit (in): ___ 39.625 Clear Bar Cover (in): _____ Bot.: 1.500 Side: 1.500

LONGITUDINAL BAR DESIGN DETAILS:

Loc. (ft)	Positive Moment				Negative Moment			
	M_u (kip-ft)	ϕM_n (kip-ft)	As req. (in ²)	As (in ²)	M_u (kip-ft)	ϕM_n (kip-ft)	As req. (in ²)	As (in ²)
0.000	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
0.667	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
1.650	22.21	232.11	0.17	1.32	0.00	-232.11	0.00	1.32
2.634	41.44	232.11	0.31	1.32	0.00	-232.11	0.00	1.32
3.618	57.69	232.11	0.43	1.32	0.00	-232.11	0.00	1.32



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Loc.	Mu	øMn	As req.	As	Mu	øMn	As req.	As
4.083	64.33	232.11	0.48	1.32	0.00	-232.11	0.00	1.32
4.087	64.39	232.11	0.48	1.32	0.00	-232.11	0.00	1.32
4.602	70.97	232.11	0.53	1.32	0.00	-232.11	0.00	1.32
5.586	81.27	232.11	0.61	1.32	0.00	-232.11	0.00	1.32
6.569	88.59	232.11	0.67	1.32	0.00	-232.11	0.00	1.32
7.553	92.93	232.11	0.70	1.32	0.00	-232.11	0.00	0.95
8.168	94.14	232.11	0.71	1.32	0.00	-232.11	0.00	1.35
8.172	94.14	232.11	0.71	1.32	0.00	-232.11	0.00	1.35
8.537	94.30	232.11	0.71	1.32	0.00	-232.11	0.00	1.01
9.521	92.70	232.11	0.70	1.32	0.00	-232.11	0.00	1.32
10.504	88.11	232.11	0.66	1.32	0.00	-232.11	0.00	1.32
11.488	80.55	232.11	0.60	1.32	0.00	-232.11	0.00	1.32
12.253	72.61	232.11	0.55	1.32	0.00	-232.11	0.00	1.32
12.257	72.57	232.11	0.54	1.32	0.00	-232.11	0.00	1.32
12.472	70.01	232.11	0.53	1.32	0.00	-232.11	0.00	1.32
13.456	56.49	232.11	0.42	1.32	0.00	-232.11	0.00	1.32
14.440	40.00	232.11	0.30	1.32	0.00	-232.11	0.00	1.32
15.423	20.57	232.11	0.15	1.32	0.00	-232.11	0.00	1.32
16.340	20.57	0.00	0.15	0.00	0.00	0.00	0.00	0.00

TRANSVERSE REINFORCEMENT:

Set	Size	Spacing	Num	Start		End		Stirrup	
				Supp.	Loc. (ft)	Supp.	Loc. (ft)	Legs	Type
1	#4	18.00	11	1	0.833	1	15.250	2	Closed

TRANSVERSE BAR DESIGN DETAILS AND TORSION FORCE:

Loc. (ft)	Vu (kip)	øVn (kip)	Tu (kip-ft)	Av req. (in ²)	Av prv. (in ²)
0.000	24.09	92.17	1.03	0.00	0.00
0.667	24.09	92.17	1.03	0.00	0.00
1.650	21.06	131.67	1.03	0.23	0.27
2.634	18.03	131.67	1.03	0.23	0.27
3.618	15.01	131.67	1.03	0.23	0.27
3.958	13.96	131.67	1.03	0.23	0.27
4.083	13.58	131.67	1.03	0.23	0.27
4.087	13.57	131.67	1.03	0.23	0.27
4.602	11.98	131.67	1.03	0.23	0.27
5.586	8.96	131.67	1.03	0.23	0.27
6.569	5.93	131.67	1.03	0.23	0.27
7.553	2.90	131.67	1.03	0.23	0.27
8.168	1.01	131.67	1.03	0.23	0.27
8.172	1.00	131.67	1.03	0.23	0.27
8.537	0.12	131.67	1.03	0.23	0.27



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Loc.	Vu	øVn	Tu	Av req.	Av prv.
9.521	3.15	131.67	1.03	0.23	0.27
10.504	6.17	131.67	1.03	0.23	0.27
11.488	9.20	131.67	1.03	0.23	0.27
12.132	11.18	131.67	1.03	0.23	0.27
12.253	11.55	131.67	1.03	0.23	0.27
12.257	11.56	131.67	1.03	0.23	0.27
12.472	12.23	131.67	1.03	0.23	0.27
13.456	15.25	131.67	1.03	0.23	0.27
14.440	18.28	131.67	1.03	0.23	0.27
15.423	21.18	92.17	1.03	0.00	0.00
16.340	21.18	92.17	1.03	0.00	0.00

TORSION CAPACITY:

0.75 Tn (kip-ft) _____ 29.48

Tu (kip-ft) _____ 1.03

DEFLECTIONS: (Camber = 0.000 in)

Type	Distance (ft)	Delta (in)	Ieff (in4)	Ieff/Ig	Ln/d	Status
Dead Load	8.39	0.005	135828.0	1.00	32484.4	
Live Load	0.00	-0.000	135828.0	1.00	155525968.0	OK
Long Term + LL	8.39	0.010	135828.0	1.00	17500.5	OK
Net Total Load	8.39	0.016	135828.0	1.00	11373.3	

Mcr Tension Bot (kip-ft) = 285.85

Mcr Tension Top (kip-ft) = 285.85

Ig (in4) = 135828.00

λ = 1.86

Controlling Deflection Ratio (Long Term + LL) = 0.014 **OK**

Span Moments For Ieff

	Mlt (kip-ft)	Mmid (kip-ft)	Mrt(kip-ft)
Dead Load	0.01	67.36	0.02
LL down defl	-0.00	-0.00	-0.00
LL up defl	0.00	0.00	0.00



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BEAM INFORMATION:

Story Level _____ FIRST FLOOR
 Beam Number _____ 31 Grid Location _ (-2.50ft--18.33ft)-(-17.00ft--18.33ft)
 Beam Line Number _ 11 Span Number _ 1

Geometry

Size: _____ **42Hx22B**
 Depth (in) _____ 42.00 Web Width (in) _____ 22.00
 Flange Width (in) _____ NA Flange Thickness (in) _____ NA
 Length c-c (ft) _____ 19.50 Clear Length (ft) _____ 18.17
 Left Support Length (in) _____ 16.00 Right Support Length (in) _____ 16.00
 Left Support Width (in) _____ 16.00 Right Support Width (in) _____ 16.00

MATERIAL PROPERTIES:

f_c (ksi) _____ 5.00 f_y Longitudinal (ksi) _____ 60.00
 f_{ct} (ksi) _____ 0.00 f_{yt} Transverse (ksi) _____ 60.00
 Conc. Weight (pcf) _____ 145.00 Conc. Type _____ NWC
 Conc. Modulus (ksi) _____ 4074.28 Reinf. Modulus (ksi) _____ 29000.00

TOP LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
1	#6	3	39.500	Upper	1	0.000	1	10.000	Hooked	Splice
2	#6	3	39.500	Upper	2	-9.500	2	0.000	Splice	Hooked

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Top: 1.500 Side: 1.500

BOTTOM LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
1	#6	3	39.500	Lower	1	0.000	1	19.500	Hooked	Hooked

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Bot.: 1.500 Side: 1.500

LONGITUDINAL BAR DESIGN DETAILS:

Loc. (ft)	Positive Moment				Negative Moment			
	M_u (kip-ft)	ϕM_n (kip-ft)	As req. (in ²)	As (in ²)	M_u (kip-ft)	ϕM_n (kip-ft)	As req. (in ²)	As (in ²)
0.000	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
0.667	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
1.623	24.13	232.11	0.18	1.32	0.00	-232.11	0.00	1.32
2.579	46.56	232.11	0.35	1.32	0.00	-232.11	0.00	1.32
3.535	67.28	232.11	0.51	1.32	0.00	-232.11	0.00	1.32



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Loc.	Mu	øMn	As req.	As	Mu	øMn	As req.	As
4.491	86.31	232.11	0.65	1.32	0.00	-232.11	0.00	1.32
5.447	103.63	232.11	0.78	1.32	0.00	-232.11	0.00	1.32
6.404	119.25	232.11	0.90	1.32	0.00	-232.11	0.00	1.32
7.360	133.17	232.11	1.00	1.32	0.00	-232.11	0.00	1.32
8.316	145.38	232.11	1.10	1.32	0.00	-232.11	0.00	1.32
9.272	155.90	232.11	1.18	1.32	0.00	-232.11	0.00	1.13
10.228	164.84	232.11	1.24	1.32	0.00	-232.11	0.00	1.35
10.828	169.72	232.11	1.28	1.32	0.00	-232.11	0.00	1.19
10.832	170.73	232.11	1.29	1.32	0.00	-232.11	0.00	1.19
11.184	165.03	232.11	1.24	1.32	0.00	-232.11	0.00	1.32
12.140	148.71	232.11	1.12	1.32	0.00	-232.11	0.00	1.32
13.096	131.16	232.11	0.99	1.32	0.00	-232.11	0.00	1.32
14.053	112.38	232.11	0.85	1.32	0.00	-232.11	0.00	1.32
15.009	92.37	232.11	0.69	1.32	0.00	-232.11	0.00	1.32
15.965	71.13	232.11	0.53	1.32	0.00	-232.11	0.00	1.32
16.921	48.65	232.11	0.36	1.32	0.00	-232.11	0.00	1.32
17.877	24.94	232.11	0.19	1.32	0.00	-232.11	0.00	1.32
18.833	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
19.500	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32

TRANSVERSE REINFORCEMENT:

Set	Size	Spacing	Num	Start		End		Stirrup	
				Supp.	Loc. (ft)	Supp.	Loc. (ft)	Legs	Type
1	#4	18.00	13	1	0.833	1	18.667	2	Closed

TRANSVERSE BAR DESIGN DETAILS AND TORSION FORCE:

Loc. (ft)	Vu (kip)	øVn (kip)	Tu (kip-ft)	Av req. (in ²)	Av prv. (in ²)
0.000	26.13	92.17	0.27	0.00	0.00
0.667	26.13	92.17	0.27	0.00	0.00
1.623	24.35	131.67	0.27	0.23	0.27
2.579	22.57	131.67	0.27	0.23	0.27
3.535	20.79	131.67	0.27	0.23	0.27
3.958	20.00	131.67	0.27	0.23	0.27
4.491	19.01	131.67	0.27	0.23	0.27
5.447	17.23	131.67	0.27	0.23	0.27
6.404	15.45	131.67	0.27	0.23	0.27
7.360	13.66	131.67	0.27	0.23	0.27
8.316	11.88	131.67	0.27	0.23	0.27
9.272	10.17	131.67	0.27	0.23	0.27
10.228	8.57	131.67	0.27	0.23	0.27
10.828	7.71	131.67	0.27	0.23	0.27
10.832	15.95	131.67	0.27	0.23	0.27



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Loc.	Vu	øVn	Tu	Av req.	Av prv.
11.184	16.42	131.67	0.27	0.23	0.27
12.140	17.71	131.67	0.27	0.23	0.27
13.096	19.00	131.67	0.27	0.23	0.27
14.053	20.29	131.67	0.27	0.23	0.27
15.009	21.57	131.67	0.27	0.23	0.27
15.542	22.29	131.67	0.27	0.23	0.27
15.965	22.86	131.67	0.27	0.23	0.27
16.921	24.15	131.67	0.27	0.23	0.27
17.877	25.44	131.67	0.27	0.23	0.27
18.833	26.73	92.17	0.27	0.00	0.00
19.500	26.73	92.17	0.27	0.00	0.00

TORSION CAPACITY:

0.75 Tn (kip-ft) _____ 29.48

Tu (kip-ft) _____ 0.27

DEFLECTIONS: (Camber = 0.000 in)

Type	Distance (ft)	Delta (in)	Ieff (in4)	Ieff/Ig	Ln/d	Status
Dead Load	10.01	0.012	135828.0	1.00	17930.6	
Live Load	0.00	-0.000	135828.0	1.00	281852384.0	OK
Long Term + LL	10.01	0.023	135828.0	1.00	9659.5	OK
Net Total Load	10.01	0.035	135828.0	1.00	6277.7	

Mcr Tension Bot (kip-ft) = 285.85

Mcr Tension Top (kip-ft) = 285.85

Ig (in4) = 135828.00

λ = 1.86

Controlling Deflection Ratio (Long Term + LL) = 0.025 **OK**

Span Moments For Ieff

	Mlt (kip-ft)	Mmid (kip-ft)	Mrt(kip-ft)
Dead Load	0.01	114.69	0.02
LL down defl	0.00	0.00	-0.00
LL up defl	0.00	0.00	0.00



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BEAM INFORMATION:

Story Level _____ FIRST FLOOR
 Beam Number _____ 32 Grid Location _ (-2.50ft--18.33ft)-(-2.50ft--0.00ft)
 Beam Line Number _ 12 Span Number _ 1

Geometry

Size: _____ **42Hx22B**
 Depth (in) _____ 42.00 Web Width (in) _____ 22.00
 Flange Width (in) _____ NA Flange Thickness (in) _____ NA
 Length c-c (ft) _____ 18.33 Clear Length (ft) _____ 16.33
 Left Support Length (in) _____ 16.00 Right Support Length (in) _____ 32.00
 Left Support Width (in) _____ 16.00 Right Support Width (in) _____ 16.00

MATERIAL PROPERTIES:

f_c (ksi) _____ 5.00 f_y Longitudinal (ksi) _____ 60.00
 f_{ct} (ksi) _____ 0.00 f_{yt} Transverse (ksi) _____ 60.00
 Conc. Weight (pcf) _____ 145.00 Conc. Type _____ NWC
 Conc. Modulus (ksi) _____ 4074.28 Reinf. Modulus (ksi) _____ 29000.00

TOP LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
1	#6	3	39.500	Upper	1	0.000	1	9.000	Hooked	Splice
2	#6	3	39.500	Upper	2	-9.330	2	0.003	Splice	Hooked

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Top: 1.500 Side: 1.500

BOTTOM LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
1	#6	3	39.500	Lower	1	0.000	1	18.333	Hooked	Hooked

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Bot.: 1.500 Side: 1.500

LONGITUDINAL BAR DESIGN DETAILS:

Loc. (ft)	Positive Moment				Negative Moment			
	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)
0.000	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
0.667	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
1.627	33.90	232.11	0.25	1.32	0.00	-232.11	0.00	1.32
2.588	63.56	232.11	0.48	1.32	0.00	-232.11	0.00	1.32
3.548	88.98	232.11	0.67	1.32	0.00	-232.11	0.00	1.32



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Loc.	Mu	øMn	As req.	As	Mu	øMn	As req.	As
4.509	110.17	232.11	0.83	1.32	0.00	-232.11	0.00	1.32
4.580	111.57	232.11	0.84	1.32	0.00	-232.11	0.00	1.32
4.585	111.65	232.11	0.84	1.32	0.00	-232.11	0.00	1.32
5.470	127.12	232.11	0.96	1.32	0.00	-232.11	0.00	1.32
6.430	139.83	232.11	1.05	1.32	0.00	-232.11	0.00	1.32
7.391	148.30	232.11	1.12	1.32	0.00	-232.11	0.00	1.32
8.351	152.54	232.11	1.15	1.32	0.00	-232.11	0.00	1.08
9.163	152.82	232.11	1.15	1.32	0.00	-232.11	0.00	1.35
9.167	152.81	232.11	1.15	1.32	0.00	-232.11	0.00	1.35
9.312	152.54	232.11	1.15	1.32	0.00	-232.11	0.00	1.35
10.273	148.30	232.11	1.12	1.32	0.00	-232.11	0.00	1.32
11.233	139.83	232.11	1.05	1.32	0.00	-232.11	0.00	1.32
12.194	127.12	232.11	0.96	1.32	0.00	-232.11	0.00	1.32
13.154	110.17	232.11	0.83	1.32	0.00	-232.11	0.00	1.32
13.745	97.63	232.11	0.73	1.32	0.00	-232.11	0.00	1.32
13.750	97.54	232.11	0.73	1.32	0.00	-232.11	0.00	1.32
14.115	88.98	232.11	0.67	1.32	0.00	-232.11	0.00	1.32
15.075	63.56	232.11	0.48	1.32	0.00	-232.11	0.00	1.32
16.036	33.90	232.11	0.25	1.32	0.00	-232.11	0.00	1.32
16.997	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32
18.330	0.00	232.11	0.00	1.32	0.00	-232.11	0.00	1.32

TRANSVERSE REINFORCEMENT:

Set	Size	Spacing	Num	Start		End		Stirrup	
				Supp.	Loc. (ft)	Supp.	Loc. (ft)	Legs	Type
1	#4	18.00	12	1	0.833	1	16.833	2	Closed

TRANSVERSE BAR DESIGN DETAILS AND TORSION FORCE:

Loc. (ft)	Vu (kip)	øVn (kip)	Tu (kip-ft)	Av req. (in ²)	Av prv. (in ²)
0.000	37.49	92.17	0.62	0.00	0.00
0.667	37.49	92.17	0.62	0.00	0.00
1.627	33.08	131.67	0.62	0.23	0.27
2.588	28.67	131.67	0.62	0.23	0.27
3.548	24.26	131.67	0.62	0.23	0.27
3.958	22.38	131.67	0.62	0.23	0.27
4.509	19.85	131.67	0.62	0.23	0.27
4.580	19.52	131.67	0.62	0.23	0.27
4.585	19.50	131.67	0.62	0.23	0.27
5.470	15.44	131.67	0.62	0.23	0.27
6.430	11.03	131.67	0.62	0.23	0.27
7.391	6.62	131.67	0.62	0.23	0.27
8.351	2.21	131.67	0.62	0.23	0.27



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Loc.	Vu	øVn	Tu	Av req.	Av prv.
9.163	1.52	131.67	0.62	0.23	0.27
9.167	1.54	131.67	0.62	0.23	0.27
9.312	2.20	131.67	0.62	0.23	0.27
10.273	6.62	131.67	0.62	0.23	0.27
11.233	11.03	131.67	0.62	0.23	0.27
12.194	15.44	131.67	0.62	0.23	0.27
13.154	19.85	131.67	0.62	0.23	0.27
13.705	22.38	131.67	0.62	0.23	0.27
13.745	22.56	131.67	0.62	0.23	0.27
13.750	22.58	131.67	0.62	0.23	0.27
14.115	24.26	131.67	0.62	0.23	0.27
15.075	28.67	131.67	0.62	0.23	0.27
16.036	33.08	131.67	0.62	0.23	0.27
16.997	37.49	92.17	0.62	0.00	0.00
18.330	37.49	92.17	0.62	0.00	0.00

TORSION CAPACITY:

0.75 Tn (kip-ft) _____ 29.48

Tu (kip-ft) _____ 0.62

DEFLECTIONS: (Camber = 0.000 in)

Type	Distance (ft)	Delta (in)	Ieff (in4)	Ieff/Ig	Ln/d	Status
Dead Load	8.92	0.010	135828.0	1.00	19327.6	
Live Load	18.33	-0.000	135828.0	1.00	195923920.0	OK
Long Term + LL	8.92	0.019	135828.0	1.00	10412.2	OK
Net Total Load	8.92	0.029	135828.0	1.00	6766.8	

Mcr Tension Bot (kip-ft) = 285.85

Mcr Tension Top (kip-ft) = 285.85

Ig (in4) = 135828.00

λ = 1.86

Controlling Deflection Ratio (Long Term + LL) = 0.023 **OK**

Span Moments For Ieff

	Mlt (kip-ft)	Mmid (kip-ft)	Mrt(kip-ft)
Dead Load	0.02	109.34	0.02
LL down defl	0.00	0.00	-0.00
LL up defl	0.00	0.00	0.00



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BEAM INFORMATION:

Story Level _____ FIRST FLOOR
 Beam Number _____ 20 Grid Location _ (17.00ft-0.00ft)-(39.67ft-0.00ft)
 Beam Line Number _ 13 Span Number _ 1

Geometry

Size: _____ **42Hx22B**
 Depth (in) _____ 42.00 Web Width (in) _____ 22.00
 Flange Width (in) _____ NA Flange Thickness (in) _____ NA
 Length c-c (ft) _____ 22.67 Clear Length (ft) _____ 21.34
 Left Support Length (in) _____ 16.00 Right Support Length (in) _____ 16.00
 Left Support Width (in) _____ 16.00 Right Support Width (in) _____ 16.00

MATERIAL PROPERTIES:

f_c (ksi) _____ 5.00 f_y Longitudinal (ksi) _____ 60.00
 f_{ct} (ksi) _____ 0.00 f_{yt} Transverse (ksi) _____ 60.00
 Conc. Weight (pcf) _____ 145.00 Conc. Type _____ NWC
 Conc. Modulus (ksi) _____ 4074.28 Reinf. Modulus (ksi) _____ 29000.00

TOP LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
1	#6	3	39.500	Upper	1	0.000	1	11.000	Hooked	Splice
2	#6	3	39.500	Upper	2	-11.670	2	-0.003	Splice	Hooked

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Top: 1.500 Side: 1.500

BOTTOM LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
1	#6	3	39.500	Lower	1	0.000	1	22.667	Hooked	Hooked

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Bot.: 1.500 Side: 1.500

LONGITUDINAL BAR DESIGN DETAILS:

Loc. (ft)	Positive Moment				Negative Moment			
	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)
0.000	0.00	232.11	0.00	1.32	-63.66	-232.11	0.48	1.32
0.667	0.00	232.11	0.00	1.32	-63.66	-232.11	0.48	1.32
1.637	0.00	232.11	0.00	1.32	-45.77	-232.11	0.34	1.32
2.606	0.00	232.11	0.00	1.32	-29.64	-232.11	0.22	1.32
3.576	0.00	232.11	0.00	1.32	-15.25	-232.11	0.11	1.32



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Loc.	Mu	øMn	As req.	As	Mu	øMn	As req.	As
4.546	0.00	232.11	0.00	1.32	-2.62	-232.11	0.02	1.32
5.516	8.26	232.11	0.06	1.32	0.00	-232.11	0.00	1.32
5.665	9.78	232.11	0.07	1.32	0.00	-232.11	0.00	1.32
5.670	9.82	232.11	0.07	1.32	0.00	-232.11	0.00	1.32
6.486	17.39	232.11	0.13	1.32	0.00	-232.11	0.00	1.32
7.456	24.77	232.11	0.19	1.32	0.00	-232.11	0.00	1.32
8.425	30.39	232.11	0.23	1.32	0.00	-232.11	0.00	1.32
9.395	34.27	232.11	0.26	1.32	0.00	-232.11	0.00	1.32
10.365	36.39	232.11	0.27	1.32	0.00	-232.11	0.00	1.07
11.333	36.76	232.11	0.28	1.32	0.00	-232.11	0.00	1.35
11.335	36.76	232.11	0.28	1.32	0.00	-232.11	0.00	1.35
11.337	36.76	232.11	0.28	1.32	0.00	-232.11	0.00	1.35
12.305	35.38	232.11	0.27	1.32	0.00	-232.11	0.00	1.32
13.275	32.25	232.11	0.24	1.32	0.00	-232.11	0.00	1.32
14.245	27.37	232.11	0.21	1.32	0.00	-232.11	0.00	1.32
15.214	20.73	232.11	0.16	1.32	0.00	-232.11	0.00	1.32
16.184	12.34	232.11	0.09	1.32	0.00	-232.11	0.00	1.32
17.000	3.93	232.11	0.03	1.32	0.00	-232.11	0.00	1.32
17.005	3.88	232.11	0.03	1.32	0.00	-232.11	0.00	1.32
17.154	2.21	232.11	0.02	1.32	0.00	-232.11	0.00	1.32
18.124	0.00	232.11	0.00	1.32	-9.68	-232.11	0.07	1.32
19.094	0.00	232.11	0.00	1.32	-23.32	-232.11	0.17	1.32
20.064	0.00	232.11	0.00	1.32	-38.72	-232.11	0.29	1.32
21.033	0.00	232.11	0.00	1.32	-55.86	-232.11	0.42	1.32
22.003	0.00	232.11	0.00	1.32	-74.76	-232.11	0.56	1.32
22.670	0.00	0.00	0.00	0.00	-74.76	0.00	0.56	0.00

TRANSVERSE REINFORCEMENT:

Set	Size	Spacing	Num	Start		End		Stirrup	
				Supp.	Loc. (ft)	Supp.	Loc. (ft)	Legs	Type
1	#4	18.00	15	1	0.833	1	21.833	2	Closed

TRANSVERSE BAR DESIGN DETAILS AND TORSION FORCE:

Loc. (ft)	Vu (kip)	øVn (kip)	Tu (kip-ft)	Av req. (in ²)	Av prv. (in ²)
0.000	19.35	92.17	0.05	0.00	0.00
0.667	19.35	92.17	0.05	0.00	0.00
1.637	17.54	131.67	0.05	0.23	0.27
2.606	15.73	131.67	0.05	0.23	0.27
3.576	13.93	131.67	0.05	0.23	0.27
3.958	13.22	131.67	0.05	0.23	0.27
4.546	12.12	131.67	0.05	0.23	0.27
5.516	10.32	131.67	0.05	0.23	0.27



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Loc.	Vu	øVn	Tu	Av req.	Av prv.
5.665	10.04	131.67	0.05	0.23	0.27
5.670	10.03	131.67	0.05	0.23	0.27
6.486	8.51	131.67	0.05	0.23	0.27
7.456	6.70	131.67	0.05	0.23	0.27
8.425	4.90	131.67	0.05	0.23	0.27
9.395	3.09	131.67	0.05	0.23	0.27
10.365	1.29	131.67	0.05	0.23	0.27
11.333	0.52	131.67	0.05	0.23	0.27
11.335	0.52	131.67	0.05	0.23	0.27
11.337	0.52	131.67	0.05	0.23	0.27
12.305	2.33	131.67	0.05	0.23	0.27
13.275	4.13	131.67	0.05	0.23	0.27
14.245	5.94	131.67	0.05	0.23	0.27
15.214	7.74	131.67	0.05	0.23	0.27
16.184	9.55	131.67	0.05	0.23	0.27
17.000	11.07	131.67	0.05	0.23	0.27
17.005	11.08	131.67	0.05	0.23	0.27
17.154	11.36	131.67	0.05	0.23	0.27
18.124	13.16	131.67	0.05	0.23	0.27
18.712	14.26	131.67	0.05	0.23	0.27
19.094	14.97	131.67	0.05	0.23	0.27
20.064	16.77	131.67	0.05	0.23	0.27
21.033	18.58	131.67	0.05	0.23	0.27
22.003	20.39	92.17	0.05	0.00	0.00
22.670	20.39	92.17	0.05	0.00	0.00

TORSION CAPACITY:

0.75 Tn (kip-ft) _____ 29.48

Tu (kip-ft) _____ 0.05

DEFLECTIONS: (Camber = 0.000 in)

Type	Distance (ft)	Delta (in)	Ieff (in4)	Ieff/Ig	Ln/d	Status
Dead Load	11.04	0.003	135828.0	1.00	95252.1	
Live Load	11.04	0.000	135828.0	1.00	125231296.0	OK
Long Term + LL	11.04	0.005	135828.0	1.00	51281.4	OK
Net Total Load	11.04	0.008	135828.0	1.00	33334.8	

Mc_r Tension Bot (kip-ft) = 285.85

Mc_r Tension Top (kip-ft) = 285.85

Ig (in4) = 135828.00

λ = 1.86

Controlling Deflection Ratio (Long Term + LL) = 0.005 **OK**

Span Moments For Ieff

	Mlt (kip-ft)	Mmid (kip-ft)	Mrt(kip-ft)
Dead Load	-45.46	26.26	-53.39
LL down defl	0.01	0.01	0.01



Bentley

Beam Design

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	Mlt (kip-ft)	Mmid (kip-ft)	Mrt(kip-ft)
LL up defl	0.00	0.00	0.00



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BEAM INFORMATION:

Story Level _____ FIRST FLOOR
 Beam Number _____ 33 Grid Location _ (17.00ft--5.00ft)-(39.67ft--5.00ft)
 Beam Line Number _ 14 Span Number _ 1

Geometry

Size: _____ **42Hx22B**
 Depth (in) _____ 42.00 Web Width (in) _____ 22.00
 Flange Width (in) _____ NA Flange Thickness (in) _____ NA
 Length c-c (ft) _____ 22.67 Clear Length (ft) _____ 20.84
 Left Support Length (in) _____ 22.00 Right Support Length (in) _____ 22.00
 Left Support Width (in) _____ NA Right Support Width (in) _____ NA

MATERIAL PROPERTIES:

f_c (ksi) _____ 5.00 f_y Longitudinal (ksi) _____ 60.00
 f_{ct} (ksi) _____ 0.00 f_{yt} Transverse (ksi) _____ 60.00
 Conc. Weight (pcf) _____ 145.00 Conc. Type _____ NWC
 Conc. Modulus (ksi) _____ 4074.28 Reinf. Modulus (ksi) _____ 29000.00

TOP LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
1	#6	3	39.500	Upper	1	0.000	1	11.000	Hooked	Splice
2	#6	3	39.500	Upper	2	-11.670	2	-0.003	Splice	Hooked

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Top: 1.500 Side: 1.500

BOTTOM LONGITUDINAL REINFORCEMENT:

Set	Size	Num	Depth (in)	Layer	Start		End		End-Condition	
					Supp.	Loc. (ft)	Supp.	Loc. (ft)	Start	End
1	#6	3	39.500	Lower	1	0.000	1	22.667	Hooked	Hooked

Max. Bar Depth Limit (in): _____ 39.625 Clear Bar Cover (in): _____ Bot.: 1.500 Side: 1.500

LONGITUDINAL BAR DESIGN DETAILS:

Loc. (ft)	Positive Moment				Negative Moment			
	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)	Mu (kip-ft)	øMn (kip-ft)	As req. (in ²)	As (in ²)
0.000	18.31	232.11	0.14	1.32	0.00	-232.11	0.00	1.32
0.917	18.31	232.11	0.14	1.32	0.00	-232.11	0.00	1.32
1.909	36.61	232.11	0.27	1.32	0.00	-232.11	0.00	1.32
2.901	53.11	232.11	0.40	1.32	0.00	-232.11	0.00	1.32
3.893	67.77	232.11	0.51	1.32	0.00	-232.11	0.00	1.32



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Loc.	Mu	øMn	As req.	As	Mu	øMn	As req.	As
4.886	80.61	232.11	0.61	1.32	0.00	-232.11	0.00	1.32
5.665	89.41	232.11	0.67	1.32	0.00	-232.11	0.00	1.32
5.670	89.45	232.11	0.67	1.32	0.00	-232.11	0.00	1.32
5.878	91.61	232.11	0.69	1.32	0.00	-232.11	0.00	1.32
6.870	100.77	232.11	0.76	1.32	0.00	-232.11	0.00	1.32
7.862	108.11	232.11	0.81	1.32	0.00	-232.11	0.00	1.32
8.854	113.61	232.11	0.85	1.32	0.00	-232.11	0.00	1.32
9.847	117.27	232.11	0.88	1.32	0.00	-232.11	0.00	1.32
10.839	119.11	232.11	0.90	1.32	0.00	-232.11	0.00	1.35
11.333	119.34	232.11	0.90	1.32	0.00	-232.11	0.00	1.35
11.337	119.34	232.11	0.90	1.32	0.00	-232.11	0.00	1.35
11.831	119.11	232.11	0.90	1.32	0.00	-232.11	0.00	1.19
12.823	117.28	232.11	0.88	1.32	0.00	-232.11	0.00	1.32
13.816	113.61	232.11	0.85	1.32	0.00	-232.11	0.00	1.32
14.808	108.11	232.11	0.81	1.32	0.00	-232.11	0.00	1.32
15.800	100.78	232.11	0.76	1.32	0.00	-232.11	0.00	1.32
16.792	91.61	232.11	0.69	1.32	0.00	-232.11	0.00	1.32
17.000	89.45	232.11	0.67	1.32	0.00	-232.11	0.00	1.32
17.005	89.41	232.11	0.67	1.32	0.00	-232.11	0.00	1.32
17.784	80.61	232.11	0.61	1.32	0.00	-232.11	0.00	1.32
18.777	67.78	232.11	0.51	1.32	0.00	-232.11	0.00	1.32
19.769	53.11	232.11	0.40	1.32	0.00	-232.11	0.00	1.32
20.761	36.61	232.11	0.27	1.32	0.00	-232.11	0.00	1.32
21.753	18.31	232.11	0.14	1.32	0.00	-232.11	0.00	1.32
22.670	18.31	0.00	0.14	0.00	0.00	0.00	0.00	0.00

TRANSVERSE REINFORCEMENT:

Set	Size	Spacing	Num	Start		End		Stirrup	
				Supp.	Loc. (ft)	Supp.	Loc. (ft)	Legs	Type
1	#4	18.00	15	1	1.083	1	21.583	2	Closed

TRANSVERSE BAR DESIGN DETAILS AND TORSION FORCE:

Loc. (ft)	Vu (kip)	øVn (kip)	Tu (kip-ft)	Av req. (in ²)	Av prv. (in ²)
0.000	19.28	92.17	0.03	0.00	0.00
0.917	19.28	92.17	0.03	0.00	0.00
1.909	17.55	131.67	0.03	0.23	0.27
2.901	15.71	131.67	0.03	0.23	0.27
3.893	13.86	131.67	0.03	0.23	0.27
4.208	13.27	131.67	0.03	0.23	0.27
4.886	12.01	131.67	0.03	0.23	0.27
5.665	10.56	131.67	0.03	0.23	0.27
5.670	10.55	131.67	0.03	0.23	0.27



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Loc.	Vu	øVn	Tu	Av req.	Av prv.
5.878	10.16	131.67	0.03	0.23	0.27
6.870	8.31	131.67	0.03	0.23	0.27
7.862	6.47	131.67	0.03	0.23	0.27
8.854	4.62	131.67	0.03	0.23	0.27
9.847	2.77	131.67	0.03	0.23	0.27
10.839	0.92	131.67	0.03	0.23	0.27
11.333	0.00	131.67	0.03	0.23	0.27
11.337	0.00	131.67	0.03	0.23	0.27
11.831	0.92	131.67	0.03	0.23	0.27
12.823	2.77	131.67	0.03	0.23	0.27
13.816	4.62	131.67	0.03	0.23	0.27
14.808	6.47	131.67	0.03	0.23	0.27
15.800	8.31	131.67	0.03	0.23	0.27
16.792	10.16	131.67	0.03	0.23	0.27
17.000	10.55	131.67	0.03	0.23	0.27
17.005	10.56	131.67	0.03	0.23	0.27
17.784	12.01	131.67	0.03	0.23	0.27
18.462	13.27	131.67	0.03	0.23	0.27
18.777	13.86	131.67	0.03	0.23	0.27
19.769	15.71	131.67	0.03	0.23	0.27
20.761	17.55	131.67	0.03	0.23	0.27
21.753	19.28	92.17	0.03	0.00	0.00
22.670	19.28	92.17	0.03	0.00	0.00

TORSION CAPACITY:

0.75 Tn (kip-ft) _____ 29.48

Tu (kip-ft) _____ 0.03

DEFLECTIONS: (Camber = 0.000 in)

Type	Distance (ft)	Delta (in)	Ieff (in4)	Ieff/Ig	Ln/d	Status
Dead Load	11.63	0.015	135828.0	1.00	17239.3	
Live Load	15.81	0.000	135828.0	1.00	7503292404	OK
					2297344.0	
Long Term + LL	11.63	0.027	135828.0	1.00	9287.2	OK
Net Total Load	11.63	0.041	135828.0	1.00	6035.6	

Mcr Tension Bot (kip-ft) = 285.85

Mcr Tension Top (kip-ft) = 285.85

Ig (in4) = 135828.00

λ = 1.86

Controlling Deflection Ratio (Long Term + LL) = 0.026 **OK**

Span Moments For Ieff

	Mlt (kip-ft)	Mmid (kip-ft)	Mrt(kip-ft)
Dead Load	0.01	85.24	0.01
LL down defl	-0.00	-0.00	0.00
LL up defl	0.00	0.00	0.00

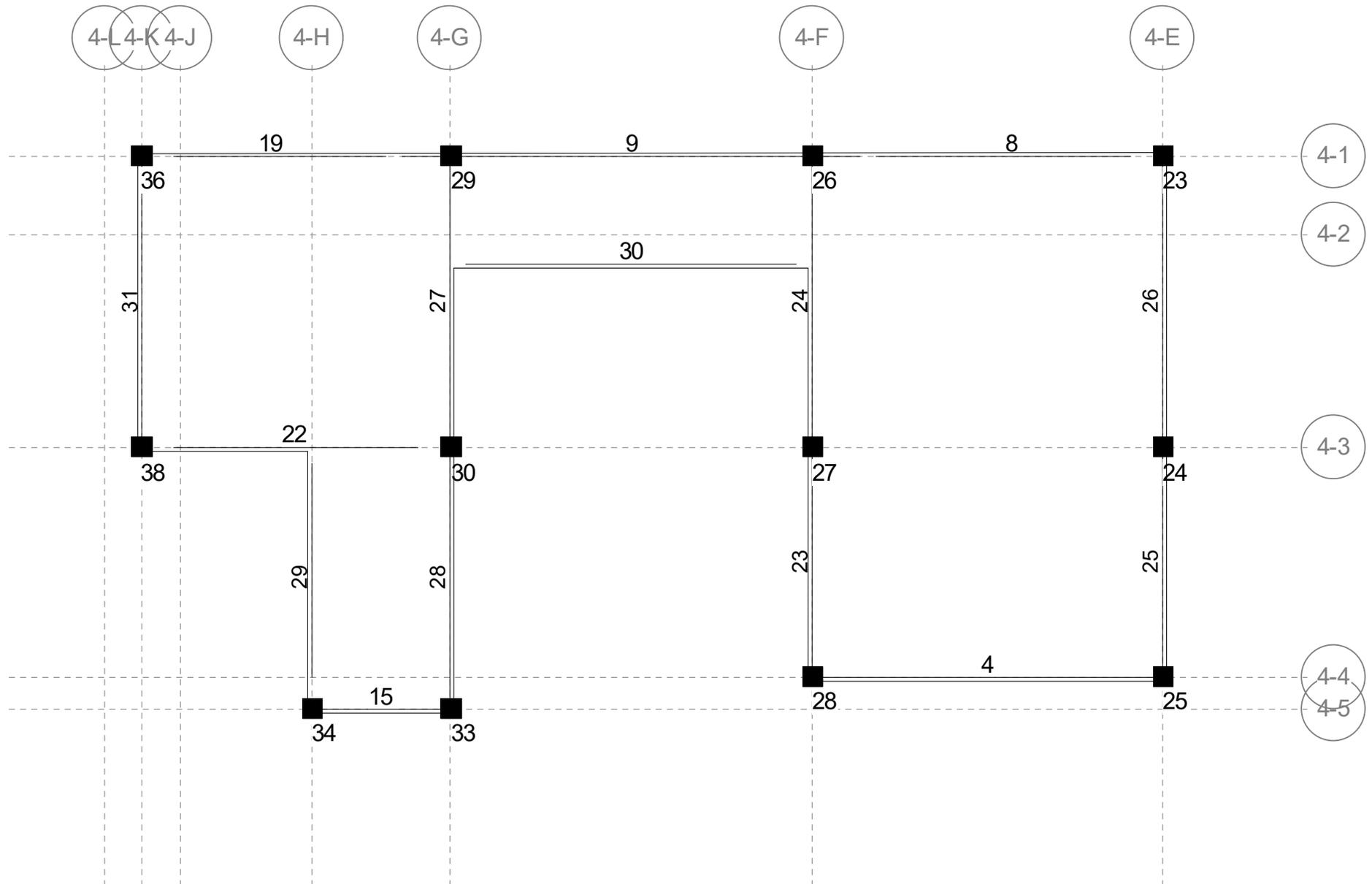
Building 4 Lateral Design



Floor Map

Floor Type: ROOF

Beam Numbers





Member Code Check

RAM Frame 17.04.02.12
DataBase: 30479 Building 4
Building Code: IBC

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Steel Code: AISC360-16 LRFD

BEAM INFORMATION:

Story Level = ROOF Frame Number = 0 Beam Number = 4
Fy (ksi) = 50.00
Beam Size = W10X33

INPUT DESIGN PARAMETERS:

	X-Axis	Y-Axis
Lu for Axial (ft) _____	22.00	22.00
Lu for Bending (ft) _____	22.00	22.00
K _____	1.00	1.00
Top Flange Continuously Braced _____	No	
Bottom Flange Continuously Braced _____	No	

CONTROLLING BEAM SEGMENT FORCES - SHEAR

Load Combination: 1.200 D + 0.500 Rfp + 1.000 W1

Segment distance (ft) i - end _____ 0.00
j - end _____ 22.00

SHEAR CHECK:

Vux (kip) = -1.78	1.00Vnx (kip) = 84.65	Vux/1.00Vnx = 0.021
Vuy (kip) = -0.01	0.90Vny (kip) = 186.98	Vuy/0.90Vny = 0.000

CONTROLLING BEAM SEGMENT FORCES - AXIAL

Load Combination: 1.200 D + 1.000 W1

Segment distance (ft) i - end _____ 0.00
j - end _____ 22.00

AXIAL CHECK:

Pu (kip) = 0.73	0.90Pnx (kip) = 327.16	Pu/0.90Pnx = 0.002
	0.90Pny (kip) = 118.64	Pu/0.90Pny = 0.006
	0.90Pn (kip) = 118.64	Pu/0.90Pn = 0.006

CONTROLLING BEAM SEGMENT FORCES - FLEXURE

Load Combination: 1.200 D + 0.500 Rfp + 1.000 W1

Segment distance (ft) i - end _____ 0.00
j - end _____ 22.00

CALCULATED PARAMETERS:

Pu (kip) = 0.73	0.90Pnx (kip) = 327.16
	0.90Pny (kip) = 118.64
Mux (kip-ft) = -7.55	0.90Mnx (kip-ft) = 145.50
Muy(kip-ft) = -0.03	0.90Mny (kip-ft) = 52.50
	Mcx (kip-ft) = 90.83
KL/Rx = 62.91	KL/Ry = 135.98
Cbx = 2.77	

INTERACTION EQUATION:

Pu/0.90*Pn=0.002
Eq H1-3: 0.009 + 0.001 = 0.010
Eq H1-1b Per H1.3: 0.001 + 0.052 + 0.000 = 0.053



Member Code Check

RAM Frame 17.04.02.12
DataBase: 30479 Building 4
Building Code: IBC

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Steel Code: AISC360-16 LRFD

BEAM INFORMATION:

Story Level = ROOF Frame Number = 0 Beam Number = 9
Fy (ksi) = 50.00
Beam Size = W10X33

INPUT DESIGN PARAMETERS:

	X-Axis	Y-Axis
Lu for Axial (ft) _____	22.67	22.67
Lu for Bending (ft) _____	22.67	22.67
K _____	1.00	1.00
Top Flange Continuously Braced _____	No	
Bottom Flange Continuously Braced _____	No	

CONTROLLING BEAM SEGMENT FORCES - SHEAR

Load Combination: 1.200 D + 0.500 Rfp - 1.000 W1

Segment distance (ft) i - end _____ 3.00
j - end _____ 25.67

SHEAR CHECK:

Vux (kip) = 2.56	1.00Vnx (kip) = 84.65	Vux/1.00Vnx = 0.030
Vuy (kip) = -0.01	0.90Vny (kip) = 186.98	Vuy/0.90Vny = 0.000

CONTROLLING BEAM SEGMENT FORCES - AXIAL

Load Combination: 1.200 D + 0.500 Rfp - 1.000 W2

Segment distance (ft) i - end _____ 3.00
j - end _____ 25.67

AXIAL CHECK:

Pu (kip) = 4.59	0.90Pnx (kip) = 321.36	Pu/0.90Pnx = 0.014
	0.90Pny (kip) = 111.73	Pu/0.90Pny = 0.041
	0.90Pn (kip) = 111.73	Pu/0.90Pn = 0.041

CONTROLLING BEAM SEGMENT FORCES - FLEXURE

Load Combination: 0.900 D + 1.000 W8

Segment distance (ft) i - end _____ 3.00
j - end _____ 25.67

CALCULATED PARAMETERS:

Pu (kip) = 3.46	0.90Pn (kip) = 111.73
Mux (kip-ft) = -7.27	0.90Mnx (kip-ft) = 145.50
Muy(kip-ft) = 0.05	0.90Mny (kip-ft) = 52.50
KL/Rx = 64.83	KL/Ry = 140.12
Cbx = 2.95	

INTERACTION EQUATION:

Pu/0.90*Pn=0.031
Eq H1-1b: 0.015 + 0.050 + 0.001 = 0.066



Member Code Check

RAM Frame 17.04.02.12
DataBase: 30479 Building 4
Building Code: IBC

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Steel Code: AISC360-16 LRFD

BEAM INFORMATION:

Story Level = ROOF Frame Number = 0 Beam Number = 15
Fy (ksi) = 50.00
Beam Size = W10X33

INPUT DESIGN PARAMETERS:

	X-Axis	Y-Axis
Lu for Axial (ft) _____	8.67	8.67
Lu for Bending (ft) _____	8.67	8.67
K _____	1.00	1.00
Top Flange Continuously Braced _____	No	
Bottom Flange Continuously Braced _____	No	

CONTROLLING BEAM SEGMENT FORCES - SHEAR

Load Combination: 1.200 D + 0.500 Rfp + 1.000 W1

Segment distance (ft) i - end _____ 0.00
j - end _____ 8.67

SHEAR CHECK:

Vux (kip) = -2.10	1.00Vnx (kip) = 84.65	Vux/1.00Vnx = 0.025
Vuy (kip) = -0.04	0.90Vny (kip) = 186.98	Vuy/0.90Vny = 0.000

CONTROLLING BEAM SEGMENT FORCES - AXIAL

Load Combination: 0.900 D + 1.000 W10

Segment distance (ft) i - end _____ 0.00
j - end _____ 8.67

AXIAL CHECK:

Pu (kip) = 0.84	0.90Pnx (kip) = 417.75	Pu/0.90Pnx = 0.002
	0.90Pny (kip) = 354.20	Pu/0.90Pny = 0.002
	0.90Pn (kip) = 354.20	Pu/0.90Pn = 0.002

CONTROLLING BEAM SEGMENT FORCES - FLEXURE

Load Combination: 1.200 D + 0.500 Rfp - 1.000 W7

Segment distance (ft) i - end _____ 0.00
j - end _____ 8.67

CALCULATED PARAMETERS:

Pu (kip) = -0.92	0.90Pn (kip) = 354.20
Mux (kip-ft) = 7.90	0.90Mnx (kip-ft) = 145.50
Muy(kip-ft) = -0.09	0.90Mny (kip-ft) = 52.50
L/r = 53.59	
Cbx = 2.50	

INTERACTION EQUATION:

Pu/0.90*Pn=0.002
Eq H1-1b: 0.001 + 0.054 + 0.002 = 0.057



Member Code Check

RAM Frame 17.04.02.12
DataBase: 30479 Building 4
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BEAM INFORMATION:

Story Level = ROOF Frame Number = 0 Beam Number = 23
Fy (ksi) = 50.00
Beam Size = W10X49

INPUT DESIGN PARAMETERS:

	X-Axis	Y-Axis
Lu for Axial (ft) _____	14.34	14.34
Lu for Bending (ft) _____	14.34	14.34
K _____	1.00	1.00
Top Flange Continuously Braced _____	No	
Bottom Flange Continuously Braced _____	No	

CONTROLLING BEAM SEGMENT FORCES - SHEAR

Load Combination: 1.200 D + 1.600 Rfp + 0.500 W2

Segment distance (ft) i - end _____ 0.00
j - end _____ 14.34

SHEAR CHECK:

Vux (kip) = -10.38	1.00Vnx (kip) = 102.00	Vux/1.00Vnx = 0.102
Vuy (kip) = 0.00	0.90Vny (kip) = 302.40	Vuy/0.90Vny = 0.000

CONTROLLING BEAM SEGMENT FORCES - AXIAL

Load Combination: 1.200 D + 0.500 Rfp + 1.000 W8

Segment distance (ft) i - end _____ 0.00
j - end _____ 14.34

AXIAL CHECK:

Pu (kip) = 1.16	0.90Pnx (kip) = 577.82	Pu/0.90Pnx = 0.002
	0.90Pny (kip) = 464.09	Pu/0.90Pny = 0.002
	0.90Pn (kip) = 464.09	Pu/0.90Pn = 0.002

CONTROLLING BEAM SEGMENT FORCES - FLEXURE

Load Combination: 1.200 D + 0.500 Rfp + 1.000 W2

Segment distance (ft) i - end _____ 0.00
j - end _____ 14.34

CALCULATED PARAMETERS:

Pu (kip) = -0.18	0.90Pn (kip) = 464.09
Mux (kip-ft) = -29.13	0.90Mnx (kip-ft) = 226.50
Muy (kip-ft) = -0.03	0.90Mny (kip-ft) = 106.13
L/r = 67.57	
Cbx = 2.46	

INTERACTION EQUATION:

Pu/0.90*Pn=0.000
Eq H1-1b: 0.000 + 0.129 + 0.000 = 0.129



Member Code Check

RAM Frame 17.04.02.12
DataBase: 30479 Building 4
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BEAM INFORMATION:

Story Level = ROOF Frame Number = 0 Beam Number = 24
Fy (ksi) = 50.00
Beam Size = W10X49

INPUT DESIGN PARAMETERS:

	X-Axis	Y-Axis
Lu for Axial (ft) _____	18.33	11.50
Lu for Bending (ft) _____	18.33	11.50
K _____	1.00	1.00
Top Flange Continuously Braced _____	No	
Bottom Flange Continuously Braced _____	No	

CONTROLLING BEAM SEGMENT FORCES - SHEAR

Load Combination: 1.200 D + 1.600 Rfp - 0.500 W2

Segment distance (ft) i - end _____ 0.00
j - end _____ 11.50

SHEAR CHECK:

Vux (kip) = 12.22	1.00Vnx (kip) = 102.00	Vux/1.00Vnx = 0.120
Vuy (kip) = -0.02	0.90Vny (kip) = 302.40	Vuy/0.90Vny = 0.000

CONTROLLING BEAM SEGMENT FORCES - AXIAL

Load Combination: 1.200 D + 0.500 Rfp + 1.000 W5

Segment distance (ft) i - end _____ 11.50
j - end _____ 18.33

AXIAL CHECK:

Pu (kip) = 1.99	0.90Pnx (kip) = 537.33	Pu/0.90Pnx = 0.004
	0.90Pny (kip) = 600.74	Pu/0.90Pny = 0.003
	0.90Pn (kip) = 537.33	Pu/0.90Pn = 0.004

CONTROLLING BEAM SEGMENT FORCES - FLEXURE

Load Combination: 1.200 D + 1.600 Rfp - 0.500 W2

Segment distance (ft) i - end _____ 0.00
j - end _____ 11.50

CALCULATED PARAMETERS:

Pu (kip) = 1.18	0.90Pnx (kip) = 537.33
	0.90Pny (kip) = 522.81
Mux (kip-ft) = -38.81	0.90Mnx (kip-ft) = 226.50
Muy(kip-ft) = -0.04	0.90Mny (kip-ft) = 106.13
	Mcx (kip-ft) = 217.28
KL/Rx = 50.61	KL/Ry = 54.19
Cbx = 2.08	

INTERACTION EQUATION:

Pu/0.90*Pn=0.002

Eq H1-3: 0.003 + 0.007 = 0.011

Eq H1-1b Per H1.3: 0.001 + 0.171 + 0.000 = 0.172



Member Code Check

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BEAM INFORMATION:

Story Level = ROOF Frame Number = 0 Beam Number = 25
Fy (ksi) = 50.00
Beam Size = W10X33

INPUT DESIGN PARAMETERS:

	X-Axis	Y-Axis
Lu for Axial (ft) _____	14.34	14.34
Lu for Bending (ft) _____	14.34	14.34
K _____	1.00	1.00
Top Flange Continuously Braced _____	No	
Bottom Flange Continuously Braced _____	No	

CONTROLLING BEAM SEGMENT FORCES - SHEAR

Load Combination: 1.200 D + 1.600 Rfp + 0.500 W5

Segment distance (ft) i - end _____ 0.00
j - end _____ 14.34

SHEAR CHECK:

Vux (kip) = -9.07	1.00Vnx (kip) = 84.65	Vux/1.00Vnx = 0.107
Vuy (kip) = 0.01	0.90Vny (kip) = 186.98	Vuy/0.90Vny = 0.000

CONTROLLING BEAM SEGMENT FORCES - AXIAL

Load Combination: 1.200 D + 0.500 Rfp - 1.000 W10

Segment distance (ft) i - end _____ 0.00
j - end _____ 14.34

AXIAL CHECK:

Pu (kip) = 1.07	0.90Pnx (kip) = 386.40	Pu/0.90Pnx = 0.003
	0.90Pny (kip) = 246.02	Pu/0.90Pny = 0.004
	0.90Pn (kip) = 246.02	Pu/0.90Pn = 0.004

CONTROLLING BEAM SEGMENT FORCES - FLEXURE

Load Combination: 1.200 D + 0.500 Rfp + 1.000 W5

Segment distance (ft) i - end _____ 0.00
j - end _____ 14.34

CALCULATED PARAMETERS:

Pu (kip) = -0.15	0.90Pn (kip) = 246.02
Mux (kip-ft) = -23.13	0.90Mnx (kip-ft) = 145.50
Muy (kip-ft) = 0.04	0.90Mny (kip-ft) = 52.50
L/r = 88.63	
Cbx = 2.44	

INTERACTION EQUATION:

Pu/0.90*Pn=0.000
Eq H1-1b: 0.000 + 0.159 + 0.001 = 0.160



Member Code Check

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BEAM INFORMATION:

Story Level = ROOF Frame Number = 0 Beam Number = 26
Fy (ksi) = 50.00
Beam Size = W10X33

INPUT DESIGN PARAMETERS:

	X-Axis	Y-Axis
Lu for Axial (ft) _____	18.33	18.33
Lu for Bending (ft) _____	18.33	18.33
K _____	1.00	1.00
Top Flange Continuously Braced _____	No	
Bottom Flange Continuously Braced _____	No	

CONTROLLING BEAM SEGMENT FORCES - SHEAR

Load Combination: 1.200 D + 1.600 Rfp - 0.500 W5

Segment distance (ft) i - end _____ 0.00
j - end _____ 18.33

SHEAR CHECK:

Vux (kip) = 10.15	1.00Vnx (kip) = 84.65	Vux/1.00Vnx = 0.120
Vuy (kip) = 0.02	0.90Vny (kip) = 186.98	Vuy/0.90Vny = 0.000

CONTROLLING BEAM SEGMENT FORCES - AXIAL

Load Combination: 1.200 D + 0.500 Rfp + 1.000 W5

Segment distance (ft) i - end _____ 0.00
j - end _____ 18.33

AXIAL CHECK:

Pu (kip) = 1.70	0.90Pnx (kip) = 357.43	Pu/0.90Pnx = 0.005
	0.90Pny (kip) = 170.94	Pu/0.90Pny = 0.010
	0.90Pn (kip) = 170.94	Pu/0.90Pn = 0.010

CONTROLLING BEAM SEGMENT FORCES - FLEXURE

Load Combination: 1.200 D + 1.600 Rfp - 0.500 W5

Segment distance (ft) i - end _____ 0.00
j - end _____ 18.33

CALCULATED PARAMETERS:

Pu (kip) = 0.78	0.90Pnx (kip) = 357.43
	0.90Pny (kip) = 170.94
Mux (kip-ft) = -29.27	0.90Mnx (kip-ft) = 145.50
Muy(kip-ft) = -0.03	0.90Mny (kip-ft) = 52.50
	Mcx (kip-ft) = 104.40
KL/Rx = 52.41	KL/Ry = 113.30
Cbx = 1.77	

INTERACTION EQUATION:

Pu/0.90*Pn=0.002
Eq H1-3: 0.007 + 0.025 = 0.032
Eq H1-1b Per H1.3: 0.001 + 0.201 + 0.000 = 0.202



Member Code Check

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Steel Code: AISC360-16 LRFD

BEAM INFORMATION:

Story Level = ROOF Frame Number = 0 Beam Number = 27
Fy (ksi) = 50.00
Beam Size = W10X49

INPUT DESIGN PARAMETERS:

	X-Axis	Y-Axis
Lu for Axial (ft) _____	18.33	11.50
Lu for Bending (ft) _____	18.33	11.50
K _____	1.00	1.00
Top Flange Continuously Braced _____	No	
Bottom Flange Continuously Braced _____	No	

CONTROLLING BEAM SEGMENT FORCES - SHEAR

Load Combination: 1.200 D + 1.600 Rfp - 0.500 W2

Segment distance (ft) i - end _____ 0.00
j - end _____ 11.50

SHEAR CHECK:

Vux (kip) = 10.61	1.00Vnx (kip) = 102.00	Vux/1.00Vnx = 0.104
Vuy (kip) = 0.04	0.90Vny (kip) = 302.40	Vuy/0.90Vny = 0.000

CONTROLLING BEAM SEGMENT FORCES - AXIAL

Load Combination: 1.200 D + 0.500 Rfp - 1.000 W7

Segment distance (ft) i - end _____ 0.00
j - end _____ 11.50

AXIAL CHECK:

Pu (kip) = 3.82	0.90Pnx (kip) = 537.33	Pu/0.90Pnx = 0.007
	0.90Pny (kip) = 522.81	Pu/0.90Pny = 0.007
	0.90Pn (kip) = 522.81	Pu/0.90Pn = 0.007

CONTROLLING BEAM SEGMENT FORCES - FLEXURE

Load Combination: 1.200 D + 1.600 Rfp - 0.500 W2

Segment distance (ft) i - end _____ 0.00
j - end _____ 11.50

CALCULATED PARAMETERS:

Pu (kip) = 2.43	0.90Pnx (kip) = 537.33
	0.90Pny (kip) = 522.81
Mux (kip-ft) = -32.61	0.90Mnx (kip-ft) = 226.50
Muy(kip-ft) = -0.07	0.90Mny (kip-ft) = 106.13
	Mcx (kip-ft) = 217.28
KL/Rx = 50.61	KL/Ry = 54.19
Cbx = 1.95	

INTERACTION EQUATION:

Pu/0.90*Pn=0.005

Eq H1-3: 0.007 + 0.006 = 0.013

Eq H1-1b Per H1.3: 0.002 + 0.144 + 0.000 = 0.146



Member Code Check

RAM Frame 17.04.02.12
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BEAM INFORMATION:

Story Level = ROOF Frame Number = 0 Beam Number = 28
Fy (ksi) = 50.00
Beam Size = W10X49

INPUT DESIGN PARAMETERS:

	X-Axis	Y-Axis
Lu for Axial (ft) _____	16.34	16.34
Lu for Bending (ft) _____	16.34	16.34
K _____	1.00	1.00
Top Flange Continuously Braced _____	No	
Bottom Flange Continuously Braced _____	No	

CONTROLLING BEAM SEGMENT FORCES - SHEAR

Load Combination: 1.200 D + 1.600 Rfp + 0.500 W2

Segment distance (ft) i - end _____ 0.00
j - end _____ 16.34

SHEAR CHECK:

Vux (kip) = -4.64	1.00Vnx (kip) = 102.00	Vux/1.00Vnx = 0.046
Vuy (kip) = 0.01	0.90Vny (kip) = 302.40	Vuy/0.90Vny = 0.000

CONTROLLING BEAM SEGMENT FORCES - AXIAL

Load Combination: 1.200 D + 0.500 Rfp - 1.000 W7

Segment distance (ft) i - end _____ 0.00
j - end _____ 16.34

AXIAL CHECK:

Pu (kip) = 2.50	0.90Pnx (kip) = 558.39	Pu/0.90Pnx = 0.004
	0.90Pny (kip) = 420.09	Pu/0.90Pny = 0.006
	0.90Pn (kip) = 420.09	Pu/0.90Pn = 0.006

CONTROLLING BEAM SEGMENT FORCES - FLEXURE

Load Combination: 1.200 D + 0.500 Rfp + 1.000 W2

Segment distance (ft) i - end _____ 0.00
j - end _____ 16.34

CALCULATED PARAMETERS:

Pu (kip) = -1.23	0.90Pn (kip) = 648.00
Mux (kip-ft) = -21.28	0.90Mnx (kip-ft) = 226.50
Muy(kip-ft) = 0.08	0.90Mny (kip-ft) = 106.13
L/r = 76.99	
Cbx = 2.51	

INTERACTION EQUATION:

Pu/0.90*Pn=0.002
Eq H1-1b: 0.001 + 0.094 + 0.001 = 0.096



Member Code Check

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BEAM INFORMATION:

Story Level = ROOF Frame Number = 0 Beam Number = 31
Fy (ksi) = 50.00
Beam Size = W10X33

INPUT DESIGN PARAMETERS:

	X-Axis	Y-Axis
Lu for Axial (ft) _____	18.33	18.33
Lu for Bending (ft) _____	18.33	18.33
K _____	1.00	1.00
Top Flange Continuously Braced _____	No	
Bottom Flange Continuously Braced _____	No	

CONTROLLING BEAM SEGMENT FORCES - SHEAR

Load Combination: 1.200 D + 1.600 Rfp - 0.500 W6

Segment distance (ft) i - end _____ 0.00
j - end _____ 18.33

SHEAR CHECK:

Vux (kip) = 8.63	1.00Vnx (kip) = 84.65	Vux/1.00Vnx = 0.102
Vuy (kip) = -0.02	0.90Vny (kip) = 186.98	Vuy/0.90Vny = 0.000

CONTROLLING BEAM SEGMENT FORCES - AXIAL

Load Combination: 1.200 D + 0.500 Rfp + 1.000 W6

Segment distance (ft) i - end _____ 0.00
j - end _____ 18.33

AXIAL CHECK:

Pu (kip) = 3.69	0.90Pnx (kip) = 357.43	Pu/0.90Pnx = 0.010
	0.90Pny (kip) = 170.94	Pu/0.90Pny = 0.022
	0.90Pn (kip) = 170.94	Pu/0.90Pn = 0.022

CONTROLLING BEAM SEGMENT FORCES - FLEXURE

Load Combination: 1.200 D + 0.500 Rfp + 1.000 W6

Segment distance (ft) i - end _____ 0.00
j - end _____ 18.33

CALCULATED PARAMETERS:

Pu (kip) = 3.69	0.90Pnx (kip) = 357.43
	0.90Pny (kip) = 170.94
Mux (kip-ft) = -20.79	0.90Mnx (kip-ft) = 145.50
Muy(kip-ft) = 0.09	0.90Mny (kip-ft) = 52.50
	Mcx (kip-ft) = 104.40
KL/Rx = 52.41	KL/Ry = 113.30
Cbx = 1.75	

INTERACTION EQUATION:

Pu/0.90*Pn=0.010
Eq H1-3: 0.032 + 0.013 = 0.045
Eq H1-1b Per H1.3: 0.005 + 0.143 + 0.000 = 0.148



Concrete Column Design

RAM Concrete Column v17.04.02.12

Database: 30479 Building 4

Building Code: IBC

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Concrete Code: ACI 318-11

COLUMN INFORMATION:

Level _____	ROOF	Frame Number: _____	0
Column Number: _____	23	Grid Location: _____	(61.67ft-0.00ft)
Size: _____	16x16	Depth x Width (in) _____	16.00x16.00

Reinforcement

Longitudinal: _____	8-#6 (3 x 1)	As (in ²) _____	3.52 (1.37%)
Transverse: _____	#4@ 12.0" 0'-0"-12'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _{yt} Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	15.00	15.00
K _____	1.91	1.91
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (31) 1.200 D + 0.500 R_{fp} + 1.000 W₅

Axial	Load (kip) _____	19.58
Moment Top	Major(kip-ft) _____	-8.98
	Minor(kip-ft) _____	-1.76
Moment Bottom	Major(kip-ft) _____	31.61
	Minor(kip-ft) _____	5.98

Calculated Parameters (Angle = 10.71 degrees): L_d/Cap = 0.28

0.90 P _n (kip): _____	19.58		
0.90 M _n Major(kip-ft): _____	111.61	0.90 M _n Minor(kip-ft): _____	21.10
	Major	Minor	
K _l /r _____	74.44	74.44	
Slender _____	Yes	Yes	

Slenderness:

P _u (kip) _____	19.58	19.58
Combination _____	31	31
C _m _____	0.49	0.54
K _____	1.00	1.00
δ _{ns} _____	1.00	1.00
β _d _____	0.92	0.92
P _c (kip) _____	1414.97	1414.97
I _g (in ⁴) _____	5461.33	5461.33

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (31) 1.200 D + 0.500 R_{fp} + 1.000 W₅



Concrete Column Design

RAM Concrete Column v17.04.02.12

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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	31	2.70	32.01	27.25	0.75	44.44	0.06
1 Minor:	39	1.52	31.93	27.25	0.75	44.38	0.03

TORSION CAPACITY:

Controlling Load Combination: (98) 0.900 D - 1.000 W12

0.75 Tn (kip-ft) _____ 4.93

Tu (kip-ft) _____ 0.01



Concrete Column Design

RAM Concrete Column v17.04.02.12
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Concrete Code: ACI 318-11

COLUMN INFORMATION:

Level _____	ROOF	Frame Number: _____	0
Column Number: _____	24	Grid Location: _____	(61.67ft--18.33ft)
Size: _____	16x16	Depth x Width (in) _____	16.00x16.00
Reinforcement			
Longitudinal: _____	8-#6 (3 x 1)	As (in ²) _____	3.52 (1.37%)
Transverse: _____	#4@ 12.0" 0'-0"-12'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _y Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	14.59	15.00
K _____	1.43	1.91
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (43) 1.200 D + 0.500 R_{fp} - 1.000 W₅

Axial	Load (kip) _____	42.70
Moment Top	Major(kip-ft) _____	33.07
	Minor(kip-ft) _____	3.84
Moment Bottom	Major(kip-ft) _____	-23.75
	Minor(kip-ft) _____	-3.84

Calculated Parameters (Angle = 6.63 degrees): L_d/Cap = 0.31

0.77 P _n (kip): _____	42.70	0.77 M _n Major(kip-ft): _____	108.05	0.77 M _n Minor(kip-ft): _____	12.56
0.77 M _n Major(kip-ft): _____	108.05				
K _l /r _____	Major 54.36	Minor 74.44			
Slender _____	Yes	Yes			

Slenderness:

P _u (kip) _____	42.70	42.70
Combination _____	43	43
C _m _____	0.31	0.36
K _____	1.00	1.00
δ _{ns} _____	1.00	1.00
β _d _____	0.95	0.95
P _c (kip) _____	1465.52	1387.37
I _g (in ⁴) _____	5461.33	5461.33

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (43) 1.200 D + 0.500 R_{fp} - 1.000 W₅



Concrete Column Design

RAM Concrete Column v17.04.02.12

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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	43	3.88	33.40	27.25	0.75	45.49	0.09
1 Minor:	87	1.87	32.61	27.25	0.75	44.90	0.04

TORSION CAPACITY:

Controlling Load Combination: (98) 0.900 D - 1.000 W12

0.75 Tn (kip-ft) _____ 5.38

Tu (kip-ft) _____ 0.03



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COLUMN INFORMATION:

Level _____	ROOF	Frame Number: _____	0
Column Number: _____	25	Grid Location: _____	(61.67ft--32.67ft)
Size: _____	16x16	Depth x Width (in) _____	16.00x16.00
Reinforcement			
Longitudinal: _____	8-#6 (3 x 1)	As (in ²) _____	3.52 (1.37%)
Transverse: _____	#4@ 12.0" 0'-0"-12'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _{yt} Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	15.00	14.59
K _____	1.91	1.69
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (36) 1.200 D + 0.500 R_{fp} + 1.000 W₁₀

Axial	Load (kip) _____	14.86	
Moment	Top	Major(kip-ft) _____	-7.41
		Minor(kip-ft) _____	11.99
Moment	Bottom	Major(kip-ft) _____	28.19
		Minor(kip-ft) _____	-17.79

Calculated Parameters (Angle = 32.26 degrees): L_d/Cap = 0.30

0.89 P _n (kip): _____	14.86		
0.89 M _n Major(kip-ft): _____	95.46	0.89 M _n Minor(kip-ft): _____	60.24
	Major	Minor	
K _l /r _____	74.44	63.96	
Slender _____	Yes	Yes	
Slenderness:			
P _u (kip) _____	14.86	14.86	
Combination _____	36	36	
C _m _____	0.49	0.33	
K _____	1.00	1.00	
δ _{ns} _____	1.00	1.00	
β _d _____	1.00	1.00	
P _c (kip) _____	1358.27	1434.78	
I _g (in ⁴) _____	5461.33	5461.33	

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (31) 1.200 D + 0.500 R_{fp} + 1.000 W₅



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	31	2.69	31.68	27.25	0.75	44.20	0.06
1 Minor:	27	2.60	31.80	27.25	0.75	44.29	0.06

TORSION CAPACITY:

Controlling Load Combination: (85) 0.900 D + 1.000 W11

0.75 Tn (kip-ft) _____ 4.90

Tu (kip-ft) _____ 0.02



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COLUMN INFORMATION:

Level _____	ROOF	Frame Number: _____	0
Column Number: _____	26	Grid Location: _____	(39.67ft-0.00ft)
Size: _____	16x16	Depth x Width (in) _____	16.00x16.00
Reinforcement			
Longitudinal: _____	8-#6 (3 x 1)	As (in ²) _____	3.52 (1.37%)
Transverse: _____	#4@ 12.0" 0'-0"-12'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _{yt} Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	15.00	14.59
K _____	1.91	1.70
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (46) 1.200 D + 0.500 R_{fp} - 1.000 W₈

Axial	Load (kip) _____	28.72
Moment Top	Major(kip-ft) _____	-9.13
	Minor(kip-ft) _____	-10.93
Moment Bottom	Major(kip-ft) _____	23.37
	Minor(kip-ft) _____	19.27

Calculated Parameters (Angle = 39.51 degrees): L_d/Cap = 0.29

0.76 P _n (kip): _____	28.72	0.76 M _n Major(kip-ft): _____	80.34	0.76 M _n Minor(kip-ft): _____	66.24
	Major		Minor		
K _l /r _____	74.44		64.29		
Slender _____	Yes		Yes		

Slenderness:

P _u (kip) _____	28.72	28.72
Combination _____	46	46
C _m _____	0.44	0.37
K _____	1.00	1.00
δ _{ns} _____	1.00	1.00
β _d _____	0.93	0.93
P _c (kip) _____	1407.24	1486.51
I _g (in ⁴) _____	5461.33	5461.33

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (28) 1.200 D + 0.500 R_{fp} + 1.000 W₂



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	28	2.76	32.59	27.25	0.75	44.88	0.06
1 Minor:	39	2.38	32.50	27.25	0.75	44.81	0.05

TORSION CAPACITY:

Controlling Load Combination: (98) 0.900 D - 1.000 W12

0.75 Tn (kip-ft) _____ 5.12

Tu (kip-ft) _____ 0.01



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COLUMN INFORMATION:

Level _____	ROOF	Frame Number: _____	0
Column Number: _____	27	Grid Location: _____	(39.67ft--18.33ft)
Size: _____	16x16	Depth x Width (in) _____	16.00x16.00
Reinforcement			
Longitudinal: _____	8-#6 (3 x 1)	As (in ²) _____	3.52 (1.37%)
Transverse: _____	#4@ 12.0" 0'-0"-12'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _y Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	14.58	15.00
K _____	1.35	1.91
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (40) 1.200 D + 0.500 R_{fp} - 1.000 W₂

Axial	Load (kip) _____	44.92
Moment Top	Major(kip-ft) _____	41.46
	Minor(kip-ft) _____	4.04
Moment Bottom	Major(kip-ft) _____	-29.53
	Minor(kip-ft) _____	-4.04

Calculated Parameters (Angle = 5.57 degrees): L_d/Cap = 0.35

0.84 P _n (kip): _____	44.92	0.84 M _n Major(kip-ft): _____	117.57	0.84 M _n Minor(kip-ft): _____	11.46
	Major		Minor		
Kl/r _____	51.16		74.44		
Slender _____	Yes		Yes		
Slenderness:					
P _u (kip) _____	44.92		44.92		
Combination _____	40		40		
C _m _____	0.32		0.37		
K _____	1.00		1.00		
δ _{ns} _____	1.00		1.00		
β _d _____	0.95		0.95		
P _c (kip) _____	1472.66		1391.99		
I _g (in ⁴) _____	5461.33		5461.33		

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (40) 1.200 D + 0.500 R_{fp} - 1.000 W₂



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	40	4.86	33.53	27.25	0.75	45.59	0.11
1 Minor:	87	1.91	32.81	27.25	0.75	45.05	0.04

TORSION CAPACITY:

Controlling Load Combination: (72) 1.200 D - 1.000 W10

0.75 Tn (kip-ft) _____ 5.72

Tu (kip-ft) _____ 0.02



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COLUMN INFORMATION:

Level _____	ROOF	Frame Number: _____	0
Column Number: _____	28	Grid Location: _____	(39.67ft--32.67ft)
Size: _____	16x16	Depth x Width (in) _____	16.00x16.00
Reinforcement			
Longitudinal: _____	8-#6 (3 x 1)	As (in ²) _____	3.52 (1.37%)
Transverse: _____	#4@ 12.0" 0'-0"-12'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _{yt} Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	15.00	14.59
K _____	1.91	1.69
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (28) 1.200 D + 0.500 R_{fp} + 1.000 W₂

Axial	Load (kip) _____	12.55
Moment Top	Major(kip-ft) _____	-8.40
	Minor(kip-ft) _____	-3.45
Moment Bottom	Major(kip-ft) _____	27.09
	Minor(kip-ft) _____	1.13

Calculated Parameters (Angle = 2.39 degrees): L_d/Cap = 0.25

0.90 P _n (kip): _____	12.55		
0.90 M _n Major(kip-ft): _____	110.49	0.90 M _n Minor(kip-ft): _____	4.61
	Major	Minor	
K _l /r _____	74.44	63.96	
Slender _____	Yes	Yes	

Slenderness:

P _u (kip) _____	12.55	12.55
Combination _____	28	28
C _m _____	0.48	0.52
K _____	1.00	1.00
δ _{ns} _____	1.00	1.00
β _d _____	1.06	1.06
P _c (kip) _____	1318.61	1392.89
I _g (in ⁴) _____	5461.33	5461.33

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (28) 1.200 D + 0.500 R_{fp} + 1.000 W₂



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	28	2.36	31.59	27.25	0.75	44.13	0.05
1 Minor:	63	2.10	31.68	27.25	0.75	44.20	0.05

TORSION CAPACITY:

Controlling Load Combination: (98) 0.900 D - 1.000 W12

0.75 Tn (kip-ft) _____ 4.83

Tu (kip-ft) _____ 0.04



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COLUMN INFORMATION:

Level _____	ROOF	Frame Number: _____	0
Column Number: _____	29	Grid Location: _____	(17.00ft-0.00ft)
Size: _____	16x16	Depth x Width (in) _____	16.00x16.00
Reinforcement			
Longitudinal: _____	8-#6 (3 x 1)	As (in ²) _____	3.52 (1.37%)
Transverse: _____	#4@ 12.0" 0'-0"-12'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _{yt} Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	15.00	14.59
K _____	1.91	1.70
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (46) 1.200 D + 0.500 R_{fp} - 1.000 W₈

Axial	Load (kip) _____	27.52
Moment Top	Major(kip-ft) _____	-8.26
	Minor(kip-ft) _____	-12.34
Moment Bottom	Major(kip-ft) _____	18.37
	Minor(kip-ft) _____	20.29

Calculated Parameters (Angle = 47.85 degrees): L_d/Cap = 0.27

0.75 P _n (kip): _____	27.52		
0.75 M _n Major(kip-ft): _____	68.70	0.75 M _n Minor(kip-ft): _____	75.90
	Major	Minor	
K _l /r _____	74.44	64.29	
Slender _____	Yes	Yes	
Slenderness:			
P _u (kip) _____	27.52	27.52	
Combination _____	46	46	
C _m _____	0.42	0.36	
K _____	1.00	1.00	
δ _{ns} _____	1.00	1.00	
β _d _____	0.92	0.92	
P _c (kip) _____	1411.14	1490.63	
I _g (in ⁴) _____	5461.33	5461.33	

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (39) 1.200 D + 0.500 R_{fp} - 1.000 W₁



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	28	2.22	32.50	27.25	0.75	44.81	0.05
1 Minor:	39	2.53	32.44	27.25	0.75	44.77	0.06

TORSION CAPACITY:

Controlling Load Combination: (82) 0.900 D + 1.000 W8

0.75 Tn (kip-ft) _____ 5.06

Tu (kip-ft) _____ 0.00



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COLUMN INFORMATION:

Level _____	ROOF	Frame Number: _____	0
Column Number: _____	30	Grid Location: _____	(17.00ft--18.33ft)
Size: _____	16x16	Depth x Width (in) _____	16.00x16.00
Reinforcement			
Longitudinal: _____	8-#6 (3 x 1)	As (in ²) _____	3.52 (1.37%)
Transverse: _____	#4@ 12.0" 0'-0"-12'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _{yt} Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	14.58	15.00
K _____	1.36	1.91
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (40) 1.200 D + 0.500 R_{fp} - 1.000 W₂

Axial	Load (kip) _____	38.03
Moment Top	Major(kip-ft) _____	48.63
	Minor(kip-ft) _____	-3.42
Moment Bottom	Major(kip-ft) _____	-33.45
	Minor(kip-ft) _____	3.42

Calculated Parameters (Angle = 4.03 degrees): L_d/Cap = 0.40

0.90 P _n (kip): _____	38.03	0.90 M _n Major(kip-ft): _____	121.57	0.90 M _n Minor(kip-ft): _____	8.56
	Major		Minor		
K _l /r _____	51.59		74.44		
Slender _____	Yes		Yes		

Slenderness:

P _u (kip) _____	38.03	38.03
Combination _____	40	40
C _m _____	0.32	0.30
K _____	1.00	1.00
δ _{ns} _____	1.00	1.00
β _d _____	0.95	0.95
P _c (kip) _____	1470.65	1390.08
I _g (in ⁴) _____	5461.33	5461.33

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (40) 1.200 D + 0.500 R_{fp} - 1.000 W₂



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	40	5.62	33.12	27.25	0.75	45.28	0.12
1 Minor:	87	1.97	32.40	27.25	0.75	44.74	0.04

TORSION CAPACITY:

Controlling Load Combination: (40) 1.200 D + 0.500 Rfp - 1.000 W2

0.75 Tn (kip-ft) _____ 5.59

Tu (kip-ft) _____ 0.00



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COLUMN INFORMATION:

Level _____	ROOF	Frame Number: _____	0
Column Number: _____	33	Grid Location: _____	(17.00ft--34.67ft)
Size: _____	16x16	Depth x Width (in) _____	16.00x16.00
Reinforcement			
Longitudinal: _____	8-#6 (3 x 1)	As (in ²) _____	3.52 (1.37%)
Transverse: _____	#4@ 12.0" 0'-0"-12'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _{yt} Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	15.00	14.59
K _____	1.91	1.45
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (33) 1.200 D + 0.500 R_{fp} + 1.000 W₇

Axial	Load (kip) _____	10.87
Moment Top	Major(kip-ft) _____	-4.27
	Minor(kip-ft) _____	13.98
Moment Bottom	Major(kip-ft) _____	16.06
	Minor(kip-ft) _____	-22.28

Calculated Parameters (Angle = 54.21 degrees): L_d/Cap = 0.25

0.89 P _n (kip): _____	10.87	0.89 M _n Minor(kip-ft): _____	90.63
0.89 M _n Major(kip-ft): _____	65.33		
	Major	Minor	
K _l /r _____	74.44	54.95	
Slender _____	Yes	Yes	
Slenderness:			
P _u (kip) _____	10.87	10.87	
Combination _____	33	33	
C _m _____	0.49	0.35	
K _____	1.00	1.00	
δ _{ns} _____	1.00	1.00	
β _d _____	0.76	0.76	
P _c (kip) _____	1541.56	1628.40	
I _g (in ⁴) _____	5461.33	5461.33	

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (27) 1.200 D + 0.500 R_{fp} + 1.000 W₁



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	28	1.75	31.34	27.25	0.75	43.94	0.04
1 Minor:	27	2.58	31.53	27.25	0.75	44.09	0.06

TORSION CAPACITY:

Controlling Load Combination: (82) 0.900 D + 1.000 W8

0.75 Tn (kip-ft) _____ 4.79

Tu (kip-ft) _____ 0.02



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COLUMN INFORMATION:

Level _____	ROOF	Frame Number: _____	0
Column Number: _____	34	Grid Location: _____	(8.33ft--34.67ft)
Size: _____	16x16	Depth x Width (in) _____	16.00x16.00
Reinforcement			
Longitudinal: _____	8-#6 (3 x 1)	As (in ²) _____	3.52 (1.37%)
Transverse: _____	#4@ 12.0" 0'-0"-12'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _{yt} Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	15.00	14.59
K _____	1.91	1.45
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (33) 1.200 D + 0.500 R_{fp} + 1.000 W₇

Axial	Load (kip) _____	6.70
Moment Top	Major(kip-ft) _____	-3.33
	Minor(kip-ft) _____	13.55
Moment Bottom	Major(kip-ft) _____	13.55
	Minor(kip-ft) _____	-22.05

Calculated Parameters (Angle = 58.43 degrees): L_d/Cap = 0.23

0.90 P _n (kip): _____	6.70	0.90 M _n Minor(kip-ft): _____	93.98
0.90 M _n Major(kip-ft): _____	57.76		
	Major	Minor	
K _l /r _____	74.44	54.95	
Slender _____	Yes	Yes	
Slenderness:			
P _u (kip) _____	6.70	6.70	
Combination _____	33	33	
C _m _____	0.50	0.35	
K _____	1.00	1.00	
δ _{ns} _____	1.00	1.00	
β _d _____	1.45	1.45	
P _c (kip) _____	1107.91	1170.31	
I _g (in ⁴) _____	5461.33	5461.33	

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (27) 1.200 D + 0.500 R_{fp} + 1.000 W₁



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	28	1.36	31.37	27.25	0.75	43.96	0.03
1 Minor:	27	2.51	31.23	27.25	0.75	43.86	0.06

TORSION CAPACITY:

Controlling Load Combination: (82) 0.900 D + 1.000 W8

0.75 Tn (kip-ft) _____ 4.70

Tu (kip-ft) _____ 0.00



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COLUMN INFORMATION:

Level _____	ROOF	Frame Number: _____	0
Column Number: _____	38	Grid Location: _____	(-2.50ft--18.33ft)
Size: _____	16x16	Depth x Width (in) _____	16.00x16.00
Reinforcement			
Longitudinal: _____	8-#6 (3 x 1)	As (in ²) _____	3.52 (1.37%)
Transverse: _____	#4@ 12.0" 0'-0"-12'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _{yt} Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	14.59	15.00
K _____	1.64	1.91
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (20) 1.200 D + 1.600 R_{fp} - 0.500 W₆

Axial	Load (kip) _____	24.08
Moment Top	Major(kip-ft) _____	42.59
	Minor(kip-ft) _____	-2.17
Moment Bottom	Major(kip-ft) _____	-24.66
	Minor(kip-ft) _____	2.17

Calculated Parameters (Angle = 2.91 degrees): L_d/Cap = 0.37

0.90 P _n (kip): _____	24.08	0.90 M _n Minor(kip-ft): _____	5.89
0.90 M _n Major(kip-ft): _____	115.72		
	Major	Minor	
K _l /r _____	62.01	74.44	
Slender _____	Yes	Yes	

Slenderness:

P _u (kip) _____	24.08	24.08
Combination _____	20	20
C _m _____	0.37	0.47
K _____	1.00	1.00
δ _{ns} _____	1.00	1.00
β _d _____	0.84	0.84
P _c (kip) _____	1552.46	1469.68
I _g (in ⁴) _____	5461.33	5461.33

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (44) 1.200 D + 0.500 R_{fp} - 1.000 W₆



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	44	4.92	32.18	27.25	0.75	44.57	0.11
1 Minor:	87	1.45	31.79	27.25	0.75	44.28	0.03

TORSION CAPACITY:

Controlling Load Combination: (40) 1.200 D + 0.500 Rfp - 1.000 W2

0.75 Tn (kip-ft) _____ 5.18

Tu (kip-ft) _____ 0.02



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COLUMN INFORMATION:

Level _____	ROOF	Frame Number: _____	0
Column Number: _____	36	Grid Location: _____	(-2.50ft--0.00ft)
Size: _____	16X32	Depth x Width (in) _____	32.00x16.00
Reinforcement			
Longitudinal: _____	14-#6 (4 x 3)	As (in ²) _____	6.16 (1.20%)
Transverse: _____	#4@ 12.0" 0'-0"-12'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

fc (ksi): _____	5.00	fy Long (ksi): _____	60.00
fc _t (ksi): _____	0.00	fy _t Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	14.59	15.00
K _____	2.16	1.91
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (32) 1.200 D + 0.500 R_{fp} + 1.000 W₆

Axial	Load (kip) _____	24.96
Moment Top	Major(kip-ft) _____	-55.51
	Minor(kip-ft) _____	-2.25
Moment Bottom	Major(kip-ft) _____	123.38
	Minor(kip-ft) _____	4.32

Calculated Parameters (Angle = 2.00 degrees): L_d/Cap = 0.30

0.90 P _n (kip): _____	24.96	0.90 M _n Major(kip-ft): _____	416.24	0.90 M _n Minor(kip-ft): _____	14.56
	Major	Minor			
Kl/r _____	41.01	74.44			
Slender _____	Yes	Yes			
Slenderness:					
P _u (kip) _____	24.96	24.96			
Combination _____	32	32			
C _m _____	0.42	0.59			
K _____	1.00	1.00			
δ _{ns} _____	1.00	1.00			
β _d _____	0.92	0.92			
P _c (kip) _____	11926.55	2822.64			
I _g (in ⁴) _____	43690.67	10922.67			

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (32) 1.200 D + 0.500 R_{fp} + 1.000 W₆



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	32	12.25	68.67	59.25	0.75	95.94	0.13
1 Minor:	39	2.63	63.14	27.25	0.75	67.79	0.04

TORSION CAPACITY:

Controlling Load Combination: (61) 1.200 D + 1.000 W11

0.75 Tn (kip-ft) _____ 12.96

Tu (kip-ft) _____ 0.11



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COLUMN INFORMATION:

Level _____	FIRST FLOOR	Frame Number: _____	0
Column Number: _____	33	Grid Location: _____	(61.67ft-0.00ft)
Size: _____	16x16	Depth x Width (in) _____	16.00x16.00
Reinforcement			
Longitudinal: _____	8-#6 (3 x 1)	As (in ²) _____	3.52 (1.37%)
Transverse: _____	#4@ 12.0" 0'-0"-3'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _{yt} Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	15.00	15.00
K _____	1.91	1.91
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (31) 1.200 D + 0.500 R_{fp} + 1.000 W₅

Axial	Load (kip) _____	20.54
Moment Top	Major(kip-ft) _____	-8.98
	Minor(kip-ft) _____	-1.85
Moment Bottom	Major(kip-ft) _____	31.61
	Minor(kip-ft) _____	5.98

Calculated Parameters (Angle = 10.71 degrees): L_d/Cap = 0.28

0.90 P _n (kip): _____	20.54	0.90 M _n Minor(kip-ft): _____	21.18
0.90 M _n Major(kip-ft): _____	112.04		
	Major	Minor	
K _l /r _____	74.44	74.44	
Slender _____	Yes	Yes	
Slenderness:			
P _u (kip) _____	20.54	20.54	
Combination _____	31	31	
C _m _____	0.49	0.54	
K _____	1.00	1.00	
δ _{ns} _____	1.00	1.00	
β _d _____	0.92	0.92	
P _c (kip) _____	1412.08	1412.08	
I _g (in ⁴) _____	5461.33	5461.33	

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (31) 1.200 D + 0.500 R_{fp} + 1.000 W₅



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	31	2.70	32.07	27.25	0.75	44.49	0.06
1 Minor:	39	1.52	31.99	27.25	0.75	44.43	0.03

TORSION CAPACITY:

Controlling Load Combination: (22) 1.200 D + 1.600 Rfp - 0.500 W8

0.75 Tn (kip-ft) _____ 5.15

Tu (kip-ft) _____ 0.02



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COLUMN INFORMATION:

Level _____	FIRST FLOOR	Frame Number: _____	0
Column Number: _____	34	Grid Location: _____	(61.67ft--18.33ft)
Size: _____	16x16	Depth x Width (in) _____	16.00x16.00
Reinforcement			
Longitudinal: _____	8-#6 (3 x 1)	As (in ²) _____	3.52 (1.37%)
Transverse: _____	#4@ 12.0" 0'-0"-3'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _{yt} Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	14.59	15.00
K _____	1.43	1.91
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (43) 1.200 D + 0.500 R_{fp} - 1.000 W₅

Axial	Load (kip) _____	43.66
Moment Top	Major(kip-ft) _____	33.07
	Minor(kip-ft) _____	3.93
Moment Bottom	Major(kip-ft) _____	-23.75
	Minor(kip-ft) _____	-3.93

Calculated Parameters (Angle = 6.78 degrees): L_d/Cap = 0.31

0.76 P _n (kip): _____	43.66	0.76 M _n Minor(kip-ft): _____	12.78
0.76 M _n Major(kip-ft): _____	107.51		
	Major	Minor	
K _l /r _____	54.36	74.44	
Slender _____	Yes	Yes	
Slenderness:			
P _u (kip) _____	43.66	43.66	
Combination _____	43	43	
C _m _____	0.31	0.36	
K _____	1.00	1.00	
δ _{ns} _____	1.00	1.00	
β _d _____	0.96	0.96	
P _c (kip) _____	1464.76	1386.65	
I _g (in ⁴) _____	5461.33	5461.33	

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (43) 1.200 D + 0.500 R_{fp} - 1.000 W₅



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	43	3.88	33.46	27.25	0.75	45.53	0.09
1 Minor:	87	1.87	32.65	27.25	0.75	44.93	0.04

TORSION CAPACITY:

Controlling Load Combination: (10) 1.200 D + 1.600 Rfp + 0.500 W8

0.75 Tn (kip-ft) _____ 5.86

Tu (kip-ft) _____ 0.01



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COLUMN INFORMATION:

Level _____ FIRST FLOOR Frame Number: _____ 0
 Column Number: _____ 35 Grid Location: _____ (61.67ft--32.67ft)
 Size: _____ 16x16 Depth x Width (in) _____ 16.00x16.00

Reinforcement

Longitudinal: _____ 8-#6 (3 x 1) As (in²) _____ 3.52 (1.37%)
 Transverse: _____ #4@ 12.0" 0'-0"-3'-0"
 Confinement _____ Tie Clear Cover (in) _____ 1.50
 Shear Legs Major _____ 2 Shear Legs Minor _____ 2
 Longitudinal Bars Max Tension Stress Ratio: 1.00

MATERIAL PROPERTIES:

f_c (ksi): _____ 5.00 f_y Long (ksi): _____ 60.00
 f_{ct} (ksi): _____ 0.00 f_{yt} Trans (ksi): _____ 60.00
 Conc. Weight (pcf): _____ 145.00 Conc. Type: _____ NWC
 Conc. Modulus (ksi): _____ 4074.28 Reinf. Modulus (ksi): _____ 29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	15.00	14.59
K _____	1.91	1.69
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (36) 1.200 D + 0.500 R_{fp} + 1.000 W₁₀

Axial	Load (kip) _____	15.82
Moment Top	Major(kip-ft) _____	-7.41
	Minor(kip-ft) _____	11.99
Moment Bottom	Major(kip-ft) _____	28.19
	Minor(kip-ft) _____	-17.79

Calculated Parameters (Angle = 32.26 degrees): L_d/Cap = 0.30

0.89 P _n (kip): _____	15.82		
0.89 M _n Major(kip-ft): _____	95.01	0.89 M _n Minor(kip-ft): _____	59.96
	Major	Minor	
K _l /r _____	74.44	63.96	
Slender _____	Yes	Yes	
Slenderness:			
P _u (kip) _____	15.82	15.82	
Combination _____	36	36	
C _m _____	0.49	0.33	
K _____	1.00	1.00	
δ _{ns} _____	1.00	1.00	
β _d _____	1.00	1.00	
P _c (kip) _____	1358.11	1434.61	
I _g (in ⁴) _____	5461.33	5461.33	

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (31) 1.200 D + 0.500 R_{fp} + 1.000 W₅



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	31	2.69	31.74	27.25	0.75	44.24	0.06
1 Minor:	27	2.60	31.86	27.25	0.75	44.33	0.06

TORSION CAPACITY:

Controlling Load Combination: (3) 1.200 D + 1.600 Rfp + 0.500 W1

0.75 Tn (kip-ft) _____ 5.06

Tu (kip-ft) _____ 0.01



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COLUMN INFORMATION:

Level _____	FIRST FLOOR	Frame Number: _____	0
Column Number: _____	36	Grid Location: _____	(39.67ft-0.00ft)
Size: _____	16x16	Depth x Width (in) _____	16.00x16.00
Reinforcement			
Longitudinal: _____	8-#6 (3 x 1)	As (in ²) _____	3.52 (1.37%)
Transverse: _____	#4@ 12.0" 0'-0"-3'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _{yt} Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	15.00	14.59
K _____	1.91	1.70
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (46) 1.200 D + 0.500 R_{fp} - 1.000 W₈

Axial	Load (kip) _____	29.68	
Moment	Top	Major(kip-ft) _____	-9.13
		Minor(kip-ft) _____	-10.93
Moment	Bottom	Major(kip-ft) _____	23.37
		Minor(kip-ft) _____	19.27

Calculated Parameters (Angle = 39.50 degrees): L_d/Cap = 0.29

0.76 P _n (kip): _____	29.68	0.76 M _n Major(kip-ft): _____	80.13	0.76 M _n Minor(kip-ft): _____	66.07
	Major	Minor			
K _l /r _____	74.44	64.29			
Slender _____	Yes	Yes			
Slenderness:					
P _u (kip) _____	29.68	29.68			
Combination _____	46	46			
C _m _____	0.44	0.37			
K _____	1.00	1.00			
δ _{ns} _____	1.00	1.00			
β _d _____	0.93	0.93			
P _c (kip) _____	1405.51	1484.68			
I _g (in ⁴) _____	5461.33	5461.33			

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (28) 1.200 D + 0.500 R_{fp} + 1.000 W₂



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	28	2.76	32.65	27.25	0.75	44.92	0.06
1 Minor:	39	2.38	32.56	27.25	0.75	44.86	0.05

TORSION CAPACITY:

Controlling Load Combination: (22) 1.200 D + 1.600 Rfp - 0.500 W8

0.75 Tn (kip-ft) _____ 5.44

Tu (kip-ft) _____ 0.04



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COLUMN INFORMATION:

Level _____ FIRST FLOOR Frame Number: _____ 0
 Column Number: _____ 37 Grid Location: _____ (39.67ft--18.33ft)
 Size: _____ 16x16 Depth x Width (in) _____ 16.00x16.00

Reinforcement
 Longitudinal: _____ 8-#6 (3 x 1) As (in²) _____ 3.52 (1.37%)
 Transverse: _____ #4@ 12.0" 0'-0"-3'-0"
 Confinement _____ Tie Clear Cover (in) _____ 1.50
 Shear Legs Major _____ 2 Shear Legs Minor _____ 2
 Longitudinal Bars Max Tension Stress Ratio: 1.00

MATERIAL PROPERTIES:

f_c (ksi): _____ 5.00 f_y Long (ksi): _____ 60.00
 f_{ct} (ksi): _____ 0.00 f_y Trans (ksi): _____ 60.00
 Conc. Weight (pcf): _____ 145.00 Conc. Type: _____ NWC
 Conc. Modulus (ksi): _____ 4074.28 Reinf. Modulus (ksi): _____ 29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	14.58	15.00
K _____	1.35	1.91
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (43) 1.200 D + 0.500 R_{fp} - 1.000 W₅

Axial	Load (kip) _____	45.91
Moment Top	Major(kip-ft) _____	39.33
	Minor(kip-ft) _____	4.13
Moment Bottom	Major(kip-ft) _____	-26.66
	Minor(kip-ft) _____	-4.13

Calculated Parameters (Angle = 6.00 degrees): L_d/Cap = 0.35

0.81 P _n (kip): _____	45.91	0.81 M _n Major(kip-ft): _____	113.97	0.81 M _n Minor(kip-ft): _____	11.97
0.81 M _n Major(kip-ft): _____	113.97				
K _l /r _____	Major 51.16	Minor 74.44			
Slender _____	Yes	Yes			

Slenderness:

P _u (kip) _____	45.91	45.91
Combination _____	43	43
C _m _____	0.33	0.36
K _____	1.00	1.00
δ _{ns} _____	1.00	1.00
β _d _____	0.95	0.95
P _c (kip) _____	1472.43	1391.76
I _g (in ⁴) _____	5461.33	5461.33

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (40) 1.200 D + 0.500 R_{fp} - 1.000 W₂



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	40	4.86	33.59	27.25	0.75	45.63	0.11
1 Minor:	87	1.91	32.86	27.25	0.75	45.08	0.04

TORSION CAPACITY:

Controlling Load Combination: (22) 1.200 D + 1.600 Rfp - 0.500 W8

0.75 Tn (kip-ft) _____ 5.93

Tu (kip-ft) _____ 0.01



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COLUMN INFORMATION:

Level _____	FIRST FLOOR	Frame Number: _____	0
Column Number: _____	38	Grid Location: _____	(39.67ft--32.67ft)
Size: _____	16x16	Depth x Width (in) _____	16.00x16.00
Reinforcement			
Longitudinal: _____	8-#6 (3 x 1)	As (in ²) _____	3.52 (1.37%)
Transverse: _____	#4@ 12.0" 0'-0"-3'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _{yt} Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	15.00	14.59
K _____	1.91	1.69
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (28) 1.200 D + 0.500 R_{fp} + 1.000 W₂

Axial	Load (kip) _____	13.51
Moment Top	Major(kip-ft) _____	-8.40
	Minor(kip-ft) _____	-3.45
Moment Bottom	Major(kip-ft) _____	27.09
	Minor(kip-ft) _____	1.22

Calculated Parameters (Angle = 2.57 degrees): L_d/Cap = 0.24

0.90 P _n (kip): _____	13.51	0.90 M _n Major(kip-ft): _____	110.91	0.90 M _n Minor(kip-ft): _____	4.98
	Major		Minor		
K _l /r _____	74.44		63.96		
Slender _____	Yes		Yes		

Slenderness:

P _u (kip) _____	13.51	13.51
Combination _____	28	28
C _m _____	0.48	0.52
K _____	1.00	1.00
δ _{ns} _____	1.00	1.00
β _d _____	1.05	1.05
P _c (kip) _____	1321.18	1395.60
I _g (in ⁴) _____	5461.33	5461.33

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (28) 1.200 D + 0.500 R_{fp} + 1.000 W₂



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	28	2.36	31.64	27.25	0.75	44.17	0.05
1 Minor:	63	2.10	31.74	27.25	0.75	44.24	0.05

TORSION CAPACITY:

Controlling Load Combination: (15) 1.200 D + 1.600 Rfp - 0.500 W1

0.75 Tn (kip-ft) _____ 5.01

Tu (kip-ft) _____ 0.01



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COLUMN INFORMATION:

Level _____	FIRST FLOOR	Frame Number: _____	0
Column Number: _____	39	Grid Location: _____	(17.00ft-0.00ft)
Size: _____	16x16	Depth x Width (in) _____	16.00x16.00
Reinforcement			
Longitudinal: _____	8-#6 (3 x 1)	As (in ²) _____	3.52 (1.37%)
Transverse: _____	#4@ 12.0" 0'-0"-3'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _{yt} Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	15.00	14.59
K _____	1.91	1.70
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (46) 1.200 D + 0.500 R_{fp} - 1.000 W₈

Axial	Load (kip) _____	28.48
Moment Top	Major(kip-ft) _____	-8.26
	Minor(kip-ft) _____	-12.34
Moment Bottom	Major(kip-ft) _____	18.37
	Minor(kip-ft) _____	20.29

Calculated Parameters (Angle = 47.85 degrees): L_d/Cap = 0.27

0.75 P _n (kip): _____	28.48		
0.75 M _n Major(kip-ft): _____	68.47	0.75 M _n Minor(kip-ft): _____	75.64
	Major	Minor	
K _l /r _____	74.44	64.29	
Slender _____	Yes	Yes	
Slenderness:			
P _u (kip) _____	28.48	28.48	
Combination _____	46	46	
C _m _____	0.42	0.36	
K _____	1.00	1.00	
δ _{ns} _____	1.00	1.00	
β _d _____	0.92	0.92	
P _c (kip) _____	1409.19	1488.57	
I _g (in ⁴) _____	5461.33	5461.33	

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (39) 1.200 D + 0.500 R_{fp} - 1.000 W₁



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	28	2.22	32.55	27.25	0.75	44.85	0.05
1 Minor:	39	2.53	32.50	27.25	0.75	44.81	0.06

TORSION CAPACITY:

Controlling Load Combination: (11) 1.200 D + 1.600 Rfp + 0.500 W9

0.75 Tn (kip-ft) _____ 5.40

Tu (kip-ft) _____ 0.02



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COLUMN INFORMATION:

Level _____	FIRST FLOOR	Frame Number: _____	0
Column Number: _____	40	Grid Location: _____	(17.00ft--18.33ft)
Size: _____	16x16	Depth x Width (in) _____	16.00x16.00
Reinforcement			
Longitudinal: _____	8-#6 (3 x 1)	As (in ²) _____	3.52 (1.37%)
Transverse: _____	#4@ 12.0" 0'-0"-3'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _{yt} Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	14.58	15.00
K _____	1.36	1.91
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (40) 1.200 D + 0.500 R_{fp} - 1.000 W₂

Axial	Load (kip) _____	38.99	
Moment	Top	Major(kip-ft) _____	48.63
		Minor(kip-ft) _____	-3.51
Moment	Bottom	Major(kip-ft) _____	-33.45
		Minor(kip-ft) _____	3.51

Calculated Parameters (Angle = 4.13 degrees): L_d/Cap = 0.40

0.90 P _n (kip): _____	38.99	0.90 M _n Major(kip-ft): _____	122.00	0.90 M _n Minor(kip-ft): _____	8.80
			Major		Minor
K _l /r _____	51.59		74.44		
Slender _____	Yes		Yes		

Slenderness:

P _u (kip) _____	38.99	38.99
Combination _____	40	40
C _m _____	0.32	0.30
K _____	1.00	1.00
δ _{ns} _____	1.00	1.00
β _d _____	0.95	0.95
P _c (kip) _____	1469.73	1389.22
I _g (in ⁴) _____	5461.33	5461.33

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (40) 1.200 D + 0.500 R_{fp} - 1.000 W₂



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	40	5.62	33.18	27.25	0.75	45.32	0.12
1 Minor:	87	1.97	32.45	27.25	0.75	44.77	0.04

TORSION CAPACITY:

Controlling Load Combination: (3) 1.200 D + 1.600 Rfp + 0.500 W1

0.75 Tn (kip-ft) _____ 5.74

Tu (kip-ft) _____ 0.03



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COLUMN INFORMATION:

Level _____ FIRST FLOOR Frame Number: _____ 0
 Column Number: _____ 41 Grid Location: _____ (17.00ft--34.67ft)
 Size: _____ 16x16 Depth x Width (in) _____ 16.00x16.00

Reinforcement
 Longitudinal: _____ 8-#6 (3 x 1) As (in²) _____ 3.52 (1.37%)
 Transverse: _____ #4@ 12.0" 0'-0"-3'-0"
 Confinement _____ Tie Clear Cover (in) _____ 1.50
 Shear Legs Major _____ 2 Shear Legs Minor _____ 2
 Longitudinal Bars Max Tension Stress Ratio: 1.00

MATERIAL PROPERTIES:

f_c (ksi): _____ 5.00 f_y Long (ksi): _____ 60.00
 f_{ct} (ksi): _____ 0.00 f_{yt} Trans (ksi): _____ 60.00
 Conc. Weight (pcf): _____ 145.00 Conc. Type: _____ NWC
 Conc. Modulus (ksi): _____ 4074.28 Reinf. Modulus (ksi): _____ 29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	15.00	14.59
K _____	1.91	1.45
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (33) 1.200 D + 0.500 R_{fp} + 1.000 W₇

Axial	Load (kip) _____	11.83
Moment Top	Major(kip-ft) _____	-4.27
	Minor(kip-ft) _____	13.98
Moment Bottom	Major(kip-ft) _____	16.06
	Minor(kip-ft) _____	-22.28

Calculated Parameters (Angle = 54.21 degrees): L_d/Cap = 0.25

0.88 P _n (kip): _____	11.83		
0.88 M _n Major(kip-ft): _____	64.99	0.88 M _n Minor(kip-ft): _____	90.16
	Major	Minor	
K _l /r _____	74.44	54.95	
Slender _____	Yes	Yes	

Slenderness:

P _u (kip) _____	11.83	11.83
Combination _____	33	33
C _m _____	0.49	0.35
K _____	1.00	1.00
δ _{ns} _____	1.00	1.00
β _d _____	0.78	0.78
P _c (kip) _____	1524.59	1610.46
I _g (in ⁴) _____	5461.33	5461.33

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (27) 1.200 D + 0.500 R_{fp} + 1.000 W₁



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	28	1.75	31.40	27.25	0.75	43.99	0.04
1 Minor:	27	2.58	31.59	27.25	0.75	44.13	0.06

TORSION CAPACITY:

Controlling Load Combination: (20) 1.200 D + 1.600 Rfp - 0.500 W6

0.75 Tn (kip-ft) _____ 4.83

Tu (kip-ft) _____ 0.03



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COLUMN INFORMATION:

Level _____ FIRST FLOOR Frame Number: _____ 0
 Column Number: _____ 42 Grid Location: _____ (8.33ft--34.67ft)
 Size: _____ 16x16 Depth x Width (in) _____ 16.00x16.00

Reinforcement
 Longitudinal: _____ 8-#6 (3 x 1) As (in²) _____ 3.52 (1.37%)
 Transverse: _____ #4@ 12.0" 0'-0"-3'-0"
 Confinement _____ Tie Clear Cover (in) _____ 1.50
 Shear Legs Major _____ 2 Shear Legs Minor _____ 2
 Longitudinal Bars Max Tension Stress Ratio: 1.00

MATERIAL PROPERTIES:

f_c (ksi): _____ 5.00 f_y Long (ksi): _____ 60.00
 f_{ct} (ksi): _____ 0.00 f_{yt} Trans (ksi): _____ 60.00
 Conc. Weight (pcf): _____ 145.00 Conc. Type: _____ NWC
 Conc. Modulus (ksi): _____ 4074.28 Reinf. Modulus (ksi): _____ 29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	15.00	14.59
K _____	1.91	1.45
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (33) 1.200 D + 0.500 R_{fp} + 1.000 W₇

Axial	Load (kip) _____	7.66
Moment Top	Major(kip-ft) _____	-3.33
	Minor(kip-ft) _____	13.55
Moment Bottom	Major(kip-ft) _____	13.55
	Minor(kip-ft) _____	-22.05

Calculated Parameters (Angle = 58.43 degrees): L_d/Cap = 0.23

0.90 P _n (kip): _____	7.66		
0.90 M _n Major(kip-ft): _____	57.96	0.90 M _n Minor(kip-ft): _____	94.31
	Major	Minor	
K _l /r _____	74.44	54.95	
Slender _____	Yes	Yes	
Slenderness:			
P _u (kip) _____	7.66	7.66	
Combination _____	33	33	
C _m _____	0.50	0.35	
K _____	1.00	1.00	
δ _{ns} _____	1.00	1.00	
β _d _____	1.39	1.39	
P _c (kip) _____	1133.88	1197.75	
I _g (in ⁴) _____	5461.33	5461.33	

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (27) 1.200 D + 0.500 R_{fp} + 1.000 W₁



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	28	1.36	31.42	27.25	0.75	44.01	0.03
1 Minor:	27	2.51	31.29	27.25	0.75	43.91	0.06

TORSION CAPACITY:

Controlling Load Combination: (26) 1.200 D + 1.600 Rfp - 0.500 W12

0.75 Tn (kip-ft) _____ 4.90

Tu (kip-ft) _____ 0.02



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COLUMN INFORMATION:

Level _____	FIRST FLOOR	Frame Number: _____	0
Column Number: _____	43	Grid Location: _____	(-2.50ft--18.33ft)
Size: _____	16x16	Depth x Width (in) _____	16.00x16.00
Reinforcement			
Longitudinal: _____	8-#6 (3 x 1)	As (in ²) _____	3.52 (1.37%)
Transverse: _____	#4@ 12.0" 0'-0"-3'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _{yt} Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	14.59	15.00
K _____	1.64	1.91
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (20) 1.200 D + 1.600 R_{fp} - 0.500 W₆

Axial	Load (kip) _____	25.04
Moment Top	Major(kip-ft) _____	42.59
	Minor(kip-ft) _____	-2.25
Moment Bottom	Major(kip-ft) _____	-24.66
	Minor(kip-ft) _____	2.25

Calculated Parameters (Angle = 3.03 degrees): L_d/Cap = 0.37

0.90 P _n (kip): _____	25.04	0.90 M _n Minor(kip-ft): _____	6.13
0.90 M _n Major(kip-ft): _____	115.76		
	Major	Minor	
K _l /r _____	62.01	74.44	
Slender _____	Yes	Yes	
Slenderness:			
P _u (kip) _____	25.04	25.04	
Combination _____	20	20	
C _m _____	0.37	0.47	
K _____	1.00	1.00	
δ _{ns} _____	1.00	1.00	
β _d _____	0.85	0.85	
P _c (kip) _____	1547.47	1464.95	
I _g (in ⁴) _____	5461.33	5461.33	

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (44) 1.200 D + 0.500 R_{fp} - 1.000 W₆



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	44	4.92	32.24	27.25	0.75	44.61	0.11
1 Minor:	87	1.45	31.83	27.25	0.75	44.31	0.03

TORSION CAPACITY:

Controlling Load Combination: (23) 1.200 D + 1.600 Rfp - 0.500 W9

0.75 Tn (kip-ft) _____ 5.25

Tu (kip-ft) _____ 0.00



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COLUMN INFORMATION:

Level _____	FIRST FLOOR	Frame Number: _____	0
Column Number: _____	46	Grid Location: _____	(-2.50ft--0.00ft)
Size: _____	16X32	Depth x Width (in) _____	32.00x16.00
Reinforcement			
Longitudinal: _____	14-#6 (4 x 3)	As (in ²) _____	6.16 (1.20%)
Transverse: _____	#4@ 12.0" 0'-0"-3'-0"		
Confinement _____	Tie	Clear Cover (in) _____	1.50
Shear Legs Major _____	2	Shear Legs Minor _____	2
Longitudinal Bars Max Tension Stress Ratio: 1.00			

MATERIAL PROPERTIES:

f _c (ksi): _____	5.00	f _y Long (ksi): _____	60.00
f _{ct} (ksi): _____	0.00	f _{yt} Trans (ksi): _____	60.00
Conc. Weight (pcf): _____	145.00	Conc. Type: _____	NWC
Conc. Modulus (ksi): _____	4074.28	Reinf. Modulus (ksi): _____	29000.00

DESIGN PARAMETERS:

	Major	Minor
Unbraced Length (ft) _____	14.59	15.00
K _____	2.16	1.91
Braced Against Sidesway _____	No	No

LONGITUDINAL REINFORCEMENT:

Controlling Load Combination: (32) 1.200 D + 0.500 R_{fp} + 1.000 W₆

Axial	Load (kip) _____	26.88	
Moment	Top	Major(kip-ft) _____	-55.51
		Minor(kip-ft) _____	-2.42
Moment	Bottom	Major(kip-ft) _____	123.38
		Minor(kip-ft) _____	4.32

Calculated Parameters (Angle = 2.00 degrees): L_d/Cap = 0.30

0.90 P _n (kip): _____	26.88	0.90 M _n Major(kip-ft): _____	418.17	0.90 M _n Minor(kip-ft): _____	14.63
	Major	Minor			
Kl/r _____	41.01	74.44			
Slender _____	Yes	Yes			
Slenderness:					
P _u (kip) _____	26.88	26.88			
Combination _____	32	32			
C _m _____	0.42	0.59			
K _____	1.00	1.00			
δ _{ns} _____	1.00	1.00			
β _d _____	0.93	0.93			
P _c (kip) _____	11891.65	2814.38			
I _g (in ⁴) _____	43690.67	10922.67			

TRANSVERSE REINFORCEMENT:

Controlling Load Combination: (32) 1.200 D + 0.500 R_{fp} + 1.000 W₆



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	LC	Vu (kip)	Vc (kip)	Vs (kip)	ϕ	$\phi (Vc + Vs)$ (kip)	Ld/Cap
1 Major:	32	12.25	68.79	59.25	0.75	96.03	0.13
1 Minor:	39	2.63	63.26	27.25	0.75	67.88	0.04

TORSION CAPACITY:

Controlling Load Combination: (26) 1.200 D + 1.600 Rfp - 0.500 W12

0.75 Tn (kip-ft) _____ 13.20

Tu (kip-ft) _____ 0.05

Concrete Column

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

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DESCRIPTION: Building 4 Coastal Column Check - Typical 16x16

Code References

Calculations per ACI 318-14, IBC 2018, CBC 2019, ASCE 7-16
 Load Combinations Used : ASCE 7-16

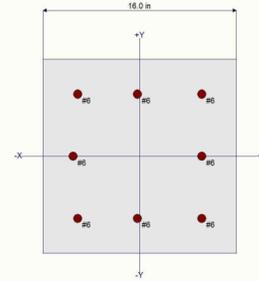
General Information

f'_c : Concrete 28 day streng = 5.0 ksi
 E = 4,030.51 ksi
 Density = 150.0 pcf
 β = 0.80
 f_y - Main Rebar = 60.0 ksi
 E - Main Rebar = 29,000.0 ksi
 Allow. Reinforcing Limits *ASTM A615 Bars Used*
 Min. Reinf. = 1 %
 Max. Reinf. = 8.0 %

Overall Column Height = 12.0 ft
 End Fixity Top Free, Bottom Fixed
 Brace condition for deflection (buckling) along column
 X-X (width) axis :
 Unbraced Length for buckling ABOUT Y-Y Axis = 12.0 ft, K = 2.0
 Y-Y (depth) axis :
 Unbraced Length for buckling ABOUT X-X Axis = 12.0 ft, K = 2.0

Column Cross Section

Column Dimensions : 16.0in Square Column, Column
 Edge to Rebar Edge Cover = 2.50in
 Column Reinforcing : 4 - #6 bars @ corners,, 1 - #6 bars
 top & bottom between corner bars, 1
 - #6 bars left & right between corner



Entered loads are factored per load combinations specified by user.

Applied Loads

Column self weight included : 3,200.0 lbs * Dead Load Factor
 BENDING LOADS . . .
 Wave Load: Lat. Point Load at 3.90 ft creating Mx-x, LR = 1.240 k
 Impact Load: Lat. Point Load at 3.90 ft creating Mx-x, D = 8.90 k

DESIGN SUMMARY

Load Combination +1.20D+2.0Lr+L+1.60H
 Location of max.above base 11.919 ft
Maximum Stress Ratio 0.497 : 1
 Ratio = $(P_u^2 + M_u^2)^{.5} / (\Phi P_n^2 + \Phi M_n^2)^{.5}$
 $P_u = 3.840$ k $\Phi * P_n = 7.239$ k
 $M_{u-x} = -51.728$ k-ft $\Phi * M_{n-x} = 105.347$ k-ft
 $M_{u-y} = 0.3456$ k-ft $\Phi * M_{n-y} = 1.151$ k-ft
 $\Phi = 0.90$
 M_u Angle = 0.0 deg
 M_u at Angle = 51.730 k-ft ΦM_n at Angle = 104.068 k-ft

Maximum SERVICE Load Reactions .

Top along Y-Y 0.0 k Bottom along Y-Y 0.0 k
 Top along X-X 0.0 k Bottom along X-X 10.140 k

Maximum SERVICE Load Deflections . .

Along Y-Y 0.06454 in at 12.0 ft above base
 for load combination : +D+Lr+H
 Along X-X 0.0in at 0.0 ft above base
 for load combination :

P_n & M_n values located at P_u-M_u vector intersection with capacity curve

Column Capacities . .

P_{nmax} : Nominal Max. Compressive Axial Capacity 1,284.24 k
 P_{nmin} : Nominal Min. Tension Axial Capacity k
 ΦP_n , max : Usable Compressive Axial Capacity 491.105 k
 ΦP_n , min : Usable Tension Axial Capacity k

General Section Information

$\beta = 0.80$ $\theta = 0.80$
 ρ : % Reinforcing 1.375 % Rebar % Ok
 Reinforcing Area 3.520 in²
 Concrete Area 256.0 in²

Governing Load Combination Results

Governing Factored Load Combination	Moment		Dist. from base ft	Axial Load k		Bending Analysis k-ft						Utilization	
	X-X	Y-Y		P_u	$\Phi * P_n$	δ_x	$\delta_x * M_{ux}$	δ_y	$\delta_y * M_{uy}$	Alpha (deg)	δM_u	ΦM_n	Ratio
+1.40D+1.60H	Actual M2,min	11.92	4.48	7.24	1.009	-49.04	1.000	0.40	0.000	49.04	104.07	0.471	
+1.20D+0.50Lr+1.60L+1.60H	Actual M2,min	11.92	3.84	7.24	1.008	-44.42	1.000	0.35	0.000	44.42	104.07	0.427	

Concrete Column

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

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DESCRIPTION: Building 4 Coastal Column Check - Typical 16x16

Governing Load Combination Results

Governing Factored Load Combination	Moment		Dist. from base ft	Axial Load k			Bending Analysis k-ft					Utilization	
	X-X	Y-Y		Pu	ϕ	* Pn	δx	δx * Mux	δy	δy * Muy	Alpha (deg)	δ Mu	ϕ Mn
+1.20D+1.60L+0.50S+1.60H	Actual M2,min		11.92	3.84	7.24	1.008	-41.98	1.000	0.35	0.000	41.98	104.07	0.403
+1.20D+2.0Lr+L+1.60H	Actual M2,min		11.92	3.84	7.24	1.008	-51.73	1.000	0.35	0.000	51.73	104.07	0.497
+1.20D+L+1.60S+1.60H	Actual M2,min		11.92	3.84	7.24	1.008	-41.98	1.000	0.35	0.000	41.98	104.07	0.403
+1.20D+1.60S+0.50W+1.60H	Actual M2,min		11.92	3.84	7.24	1.008	-41.98	1.000	0.35	0.000	41.98	104.07	0.403
+1.20D+0.50Lr+L+W+1.60H	Actual M2,min		11.92	3.84	7.24	1.008	-44.42	1.000	0.35	0.000	44.42	104.07	0.427
+1.20D+L+0.50S+W+1.60H	Actual M2,min		11.92	3.84	7.24	1.008	-41.98	1.000	0.35	0.000	41.98	104.07	0.403
+0.90D+W+1.60H	Actual M2,min		11.92	2.88	7.24	1.006	-31.42	1.000	0.26	0.000	31.42	104.07	0.302
+1.20D+L+0.20S+E+1.60H	Actual M2,min		11.92	3.84	7.24	1.008	-41.98	1.000	0.35	0.000	41.98	104.07	0.403
+0.90D+E+0.90H	Actual M2,min		11.92	2.88	7.24	1.006	-31.42	1.000	0.26	0.000	31.42	104.07	0.302

Maximum Reactions

Note: Only non-zero reactions are listed.

Load Combination	X-X Axis Reaction k		Y-Y Axis Reaction k		Axial Reaction k	Mx - End Moments k-ft		My - End Moments k-ft	
	@ Base	@ Top	@ Base	@ Top		@ Base	@ Top	@ Base	@ Top
+D+H			8.900		3.200	-34.710			
+D+L+H			8.900		3.200	-34.710			
+D+Lr+H			10.140		3.200	-39.546			
+D+S+H			8.900		3.200	-34.710			
+D+0.750Lr+0.750L+H			9.830		3.200	-38.337			
+D+0.750L+0.750S+H			8.900		3.200	-34.710			
+D+0.60W+H			8.900		3.200	-34.710			
+D+0.750Lr+0.750L+0.450W+H			9.830		3.200	-38.337			
+D+0.750L+0.750S+0.450W+H			8.900		3.200	-34.710			
+0.60D+0.60W+0.60H			5.340		1.920	-20.826			
+D+0.70E+0.60H			8.900		3.200	-34.710			
+D+0.750L+0.750S+0.5250E+H			8.900		3.200	-34.710			
+0.60D+0.70E+H			5.340		1.920	-20.826			
D Only			8.900		3.200	-34.710			
Lr Only			1.240			-4.836			
L Only									
S Only									
W Only									
E Only									
H Only									

Maximum Moment Reactions

Note: Only non-zero reactions are listed.

Load Combination	Moment About X-X Axis k-ft		Moment About Y-Y Axis k-ft	
	@ Base	@ Top	@ Base	@ Top
+D+H	-34.710			k-ft
+D+L+H	-34.710			k-ft
+D+Lr+H	-39.546			k-ft
+D+S+H	-34.710			k-ft
+D+0.750Lr+0.750L+H	-38.337			k-ft
+D+0.750L+0.750S+H	-34.710			k-ft
+D+0.60W+H	-34.710			k-ft
+D+0.750Lr+0.750L+0.450W+H	-38.337			k-ft
+D+0.750L+0.750S+0.450W+H	-34.710			k-ft
+0.60D+0.60W+0.60H	-20.826			k-ft
+D+0.70E+0.60H	-34.710			k-ft
+D+0.750L+0.750S+0.5250E+H	-34.710			k-ft
+0.60D+0.70E+H	-20.826			k-ft
D Only	-34.710			k-ft
Lr Only	-4.836			k-ft
L Only				k-ft
S Only				k-ft
W Only				k-ft
E Only				k-ft
H Only				k-ft

Concrete Column

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

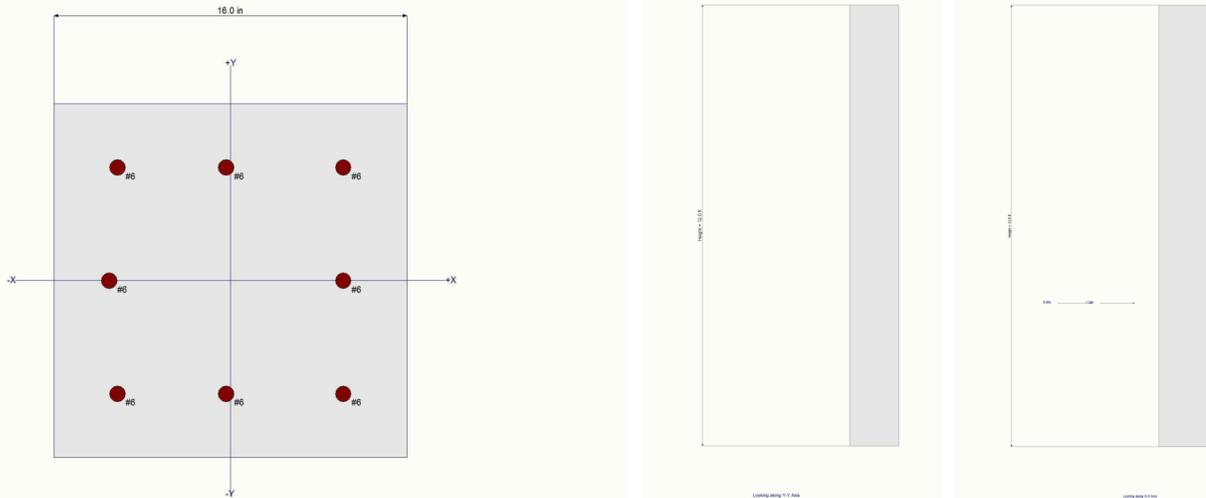
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DESCRIPTION: Building 4 Coastal Column Check - Typical 16x16

Maximum Deflections for Load Combinations

Load Combination	Max. X-X Deflection	Distance	Max. Y-Y Deflection	Distance
+D+H	0.0000 in	0.000 ft	0.057 in	12.000 ft
+D+L+H	0.0000 in	0.000 ft	0.057 in	12.000 ft
+D+Lr+H	0.0000 in	0.000 ft	0.065 in	12.000 ft
+D+S+H	0.0000 in	0.000 ft	0.057 in	12.000 ft
+D+0.750Lr+0.750L+H	0.0000 in	0.000 ft	0.063 in	12.000 ft
+D+0.750L+0.750S+H	0.0000 in	0.000 ft	0.057 in	12.000 ft
+D+0.60W+H	0.0000 in	0.000 ft	0.057 in	12.000 ft
+D+0.750Lr+0.750L+0.450W+H	0.0000 in	0.000 ft	0.063 in	12.000 ft
+D+0.750L+0.750S+0.450W+H	0.0000 in	0.000 ft	0.057 in	12.000 ft
+0.60D+0.60W+0.60H	0.0000 in	0.000 ft	0.034 in	12.000 ft
+D+0.70E+0.60H	0.0000 in	0.000 ft	0.057 in	12.000 ft
+D+0.750L+0.750S+0.5250E+H	0.0000 in	0.000 ft	0.057 in	12.000 ft
+0.60D+0.70E+H	0.0000 in	0.000 ft	0.034 in	12.000 ft
D Only	0.0000 in	0.000 ft	0.057 in	12.000 ft
Lr Only	0.0000 in	0.000 ft	0.008 in	12.000 ft
L Only	0.0000 in	0.000 ft	0.000 in	0.000 ft
S Only	0.0000 in	0.000 ft	0.000 in	0.000 ft
W Only	0.0000 in	0.000 ft	0.000 in	0.000 ft
E Only	0.0000 in	0.000 ft	0.000 in	0.000 ft
H Only	0.0000 in	0.000 ft	0.000 in	0.000 ft

Sketches



Interaction Diagrams

Concrete Column

LIC# : KW-06011269, Build:20.23.06.01

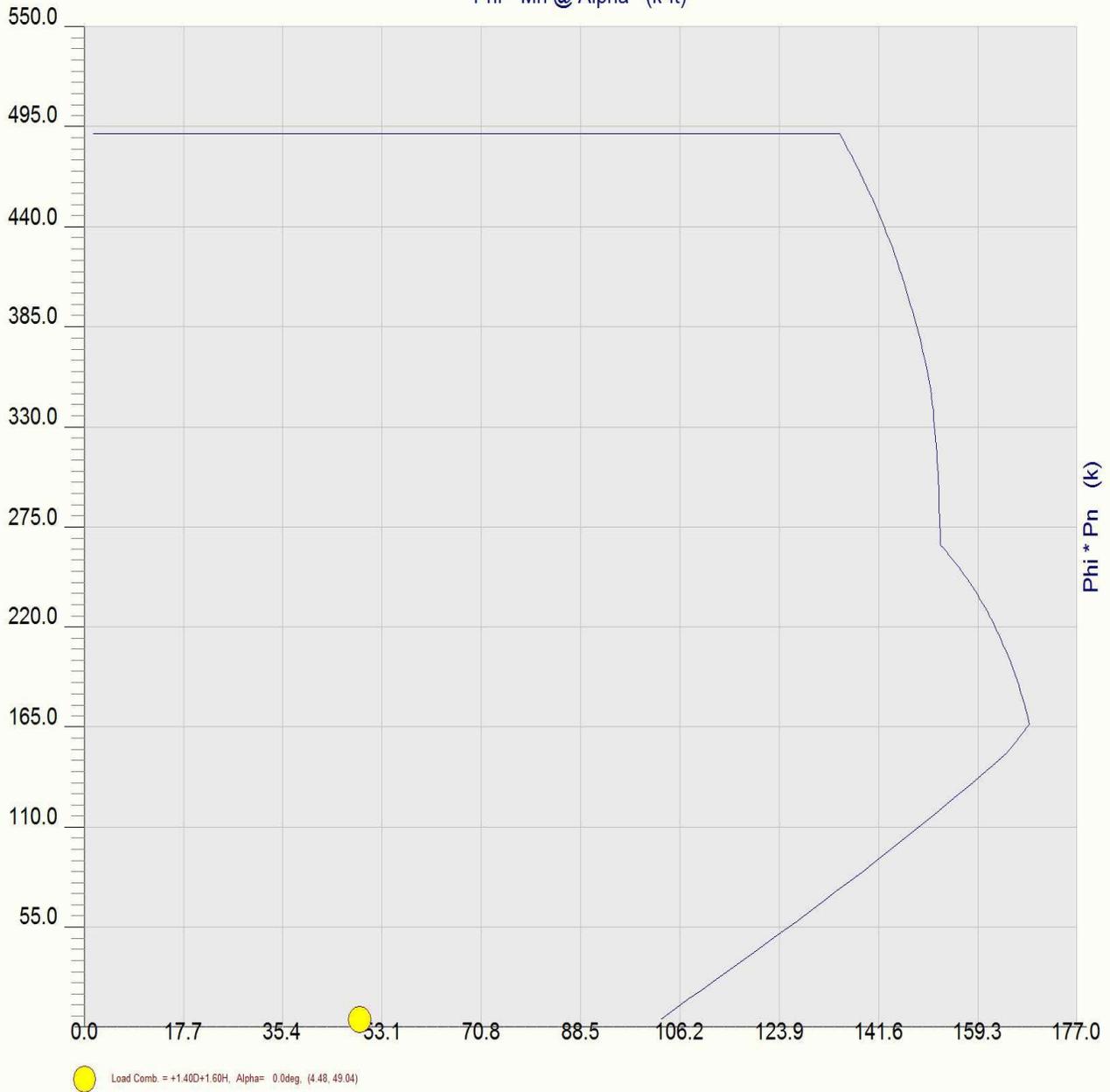
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DESCRIPTION: Building 4 Coastal Column Check - Typical 16x16

Concrete Column P-M Interaction Diagram

Phi * Mn @ Alpha (k-ft)



Concrete Column

LIC# : KW-06011269, Build:20.23.06.01

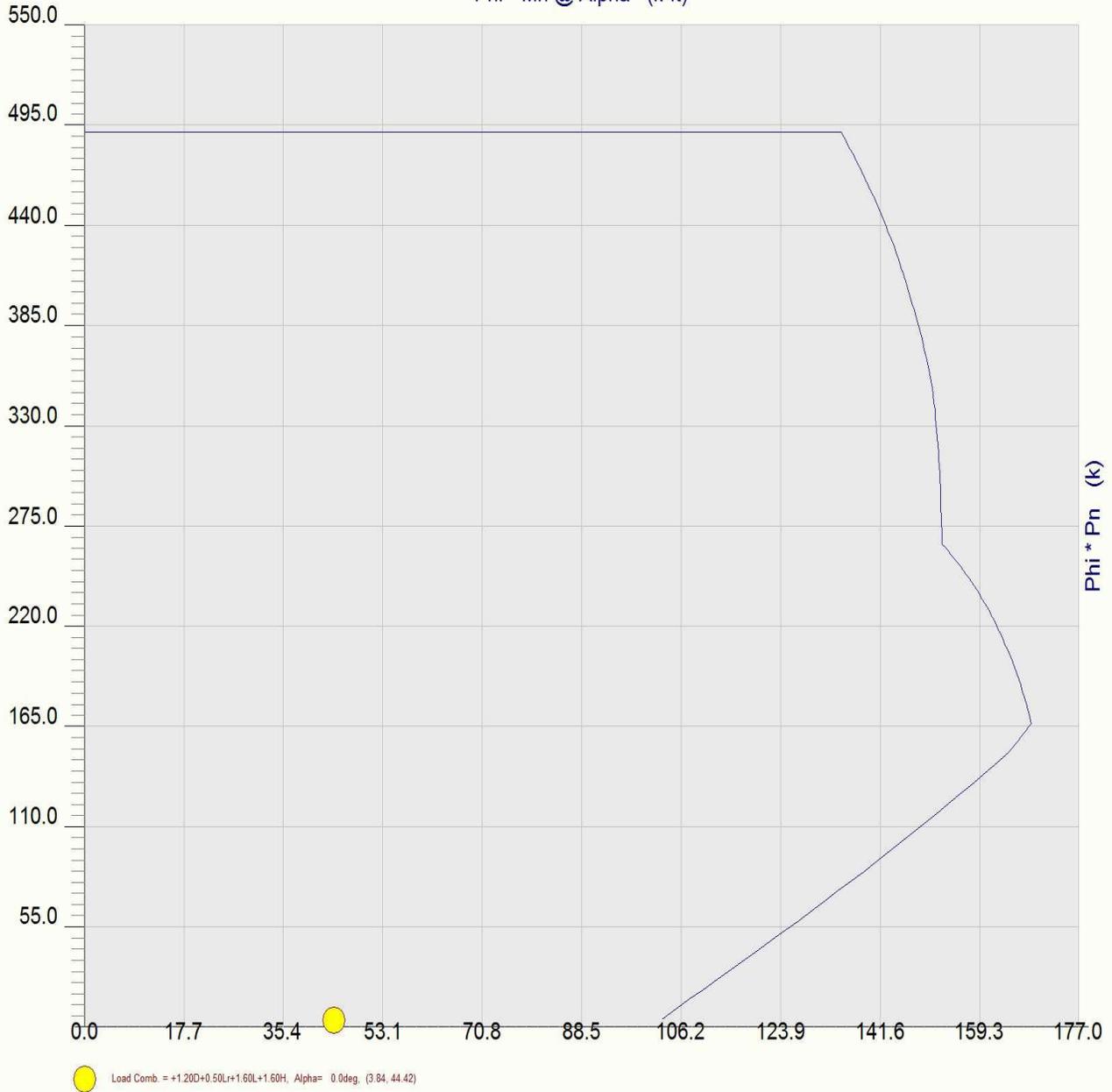
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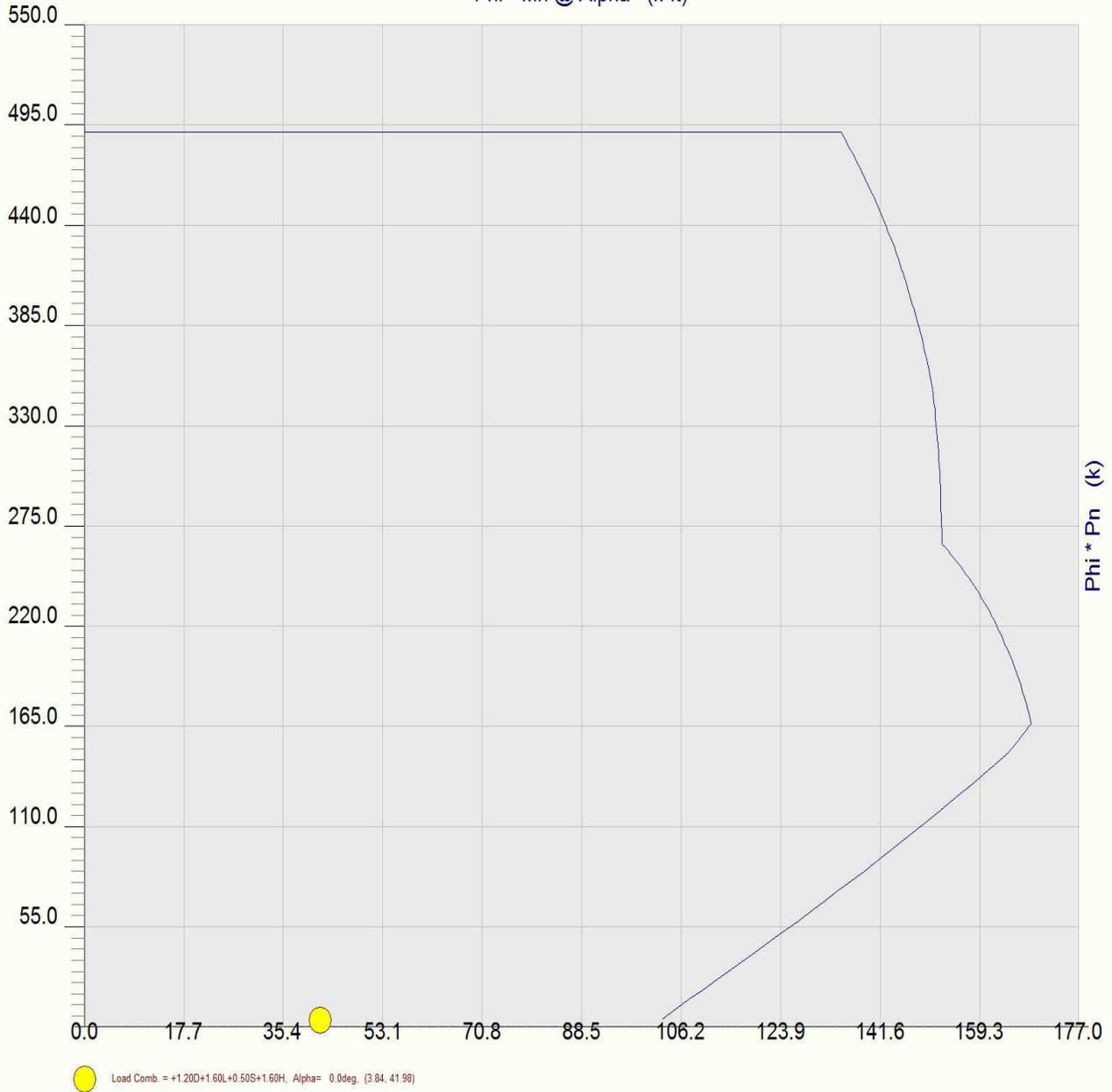
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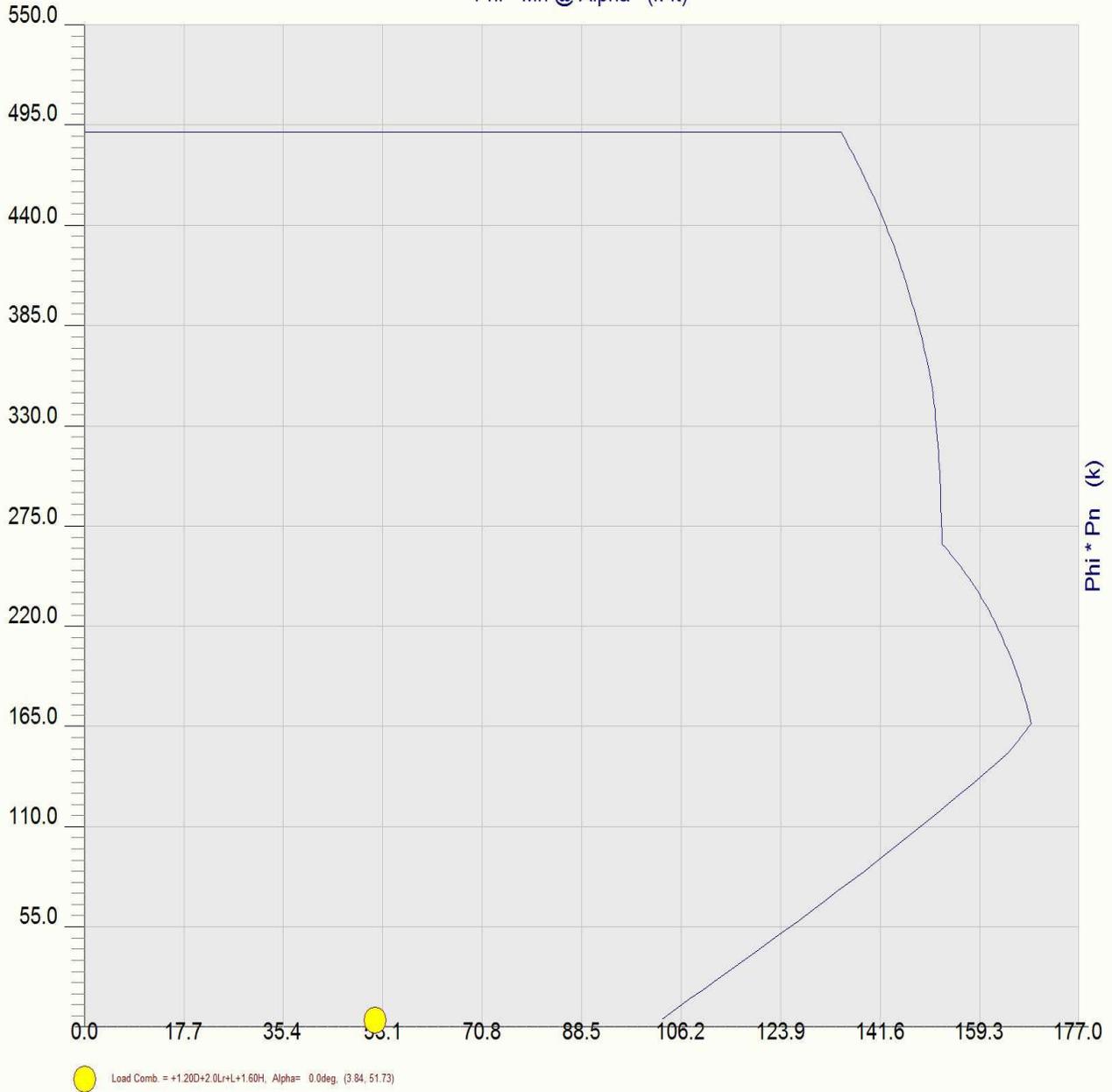
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Phi * Mn @ Alpha (k-ft)



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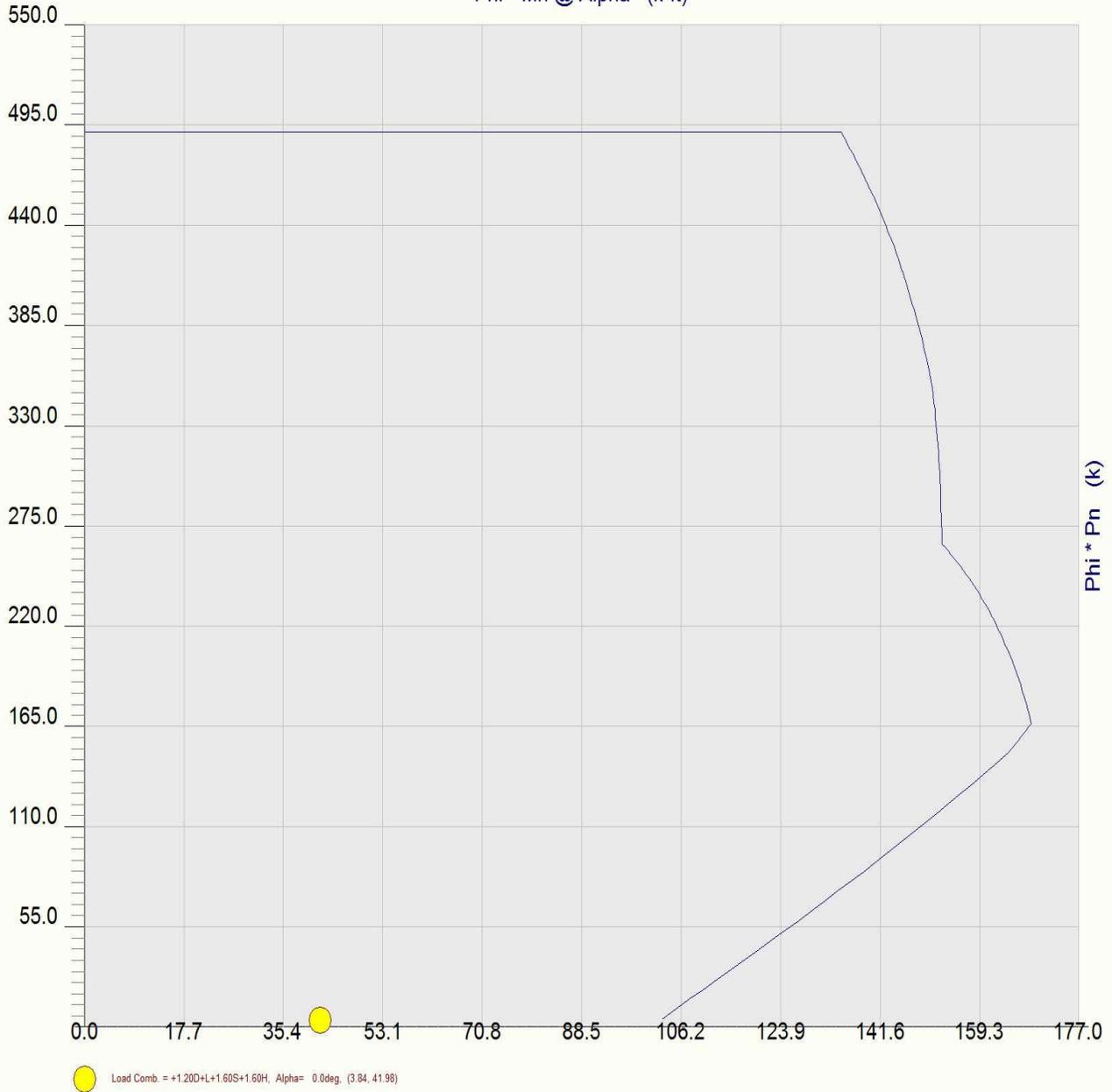
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Concrete Column P-M Interaction Diagram

Phi * Mn @ Alpha (k-ft)



Concrete Column

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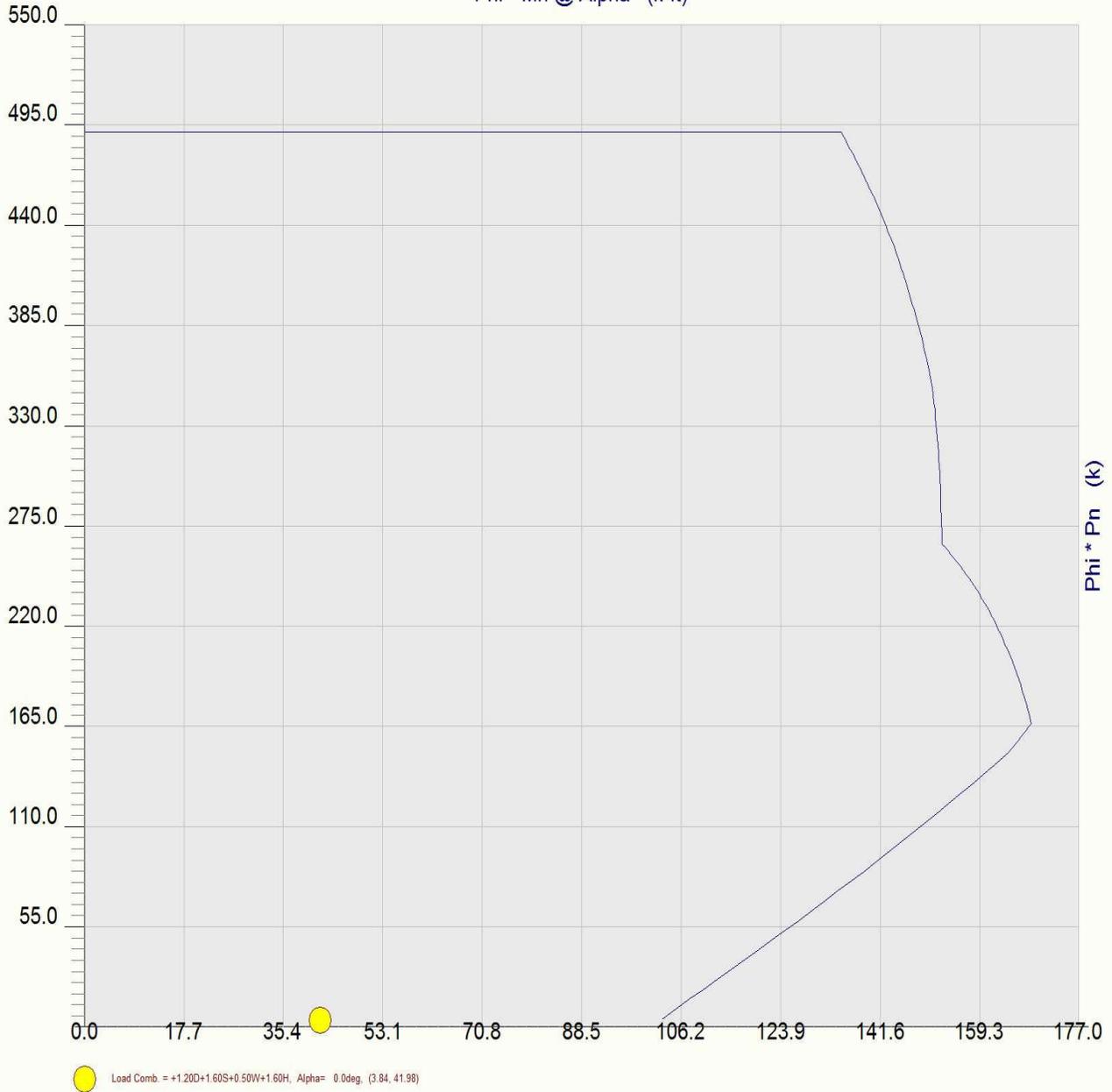
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Concrete Column P-M Interaction Diagram

Phi * Mn @ Alpha (k-ft)



Concrete Column

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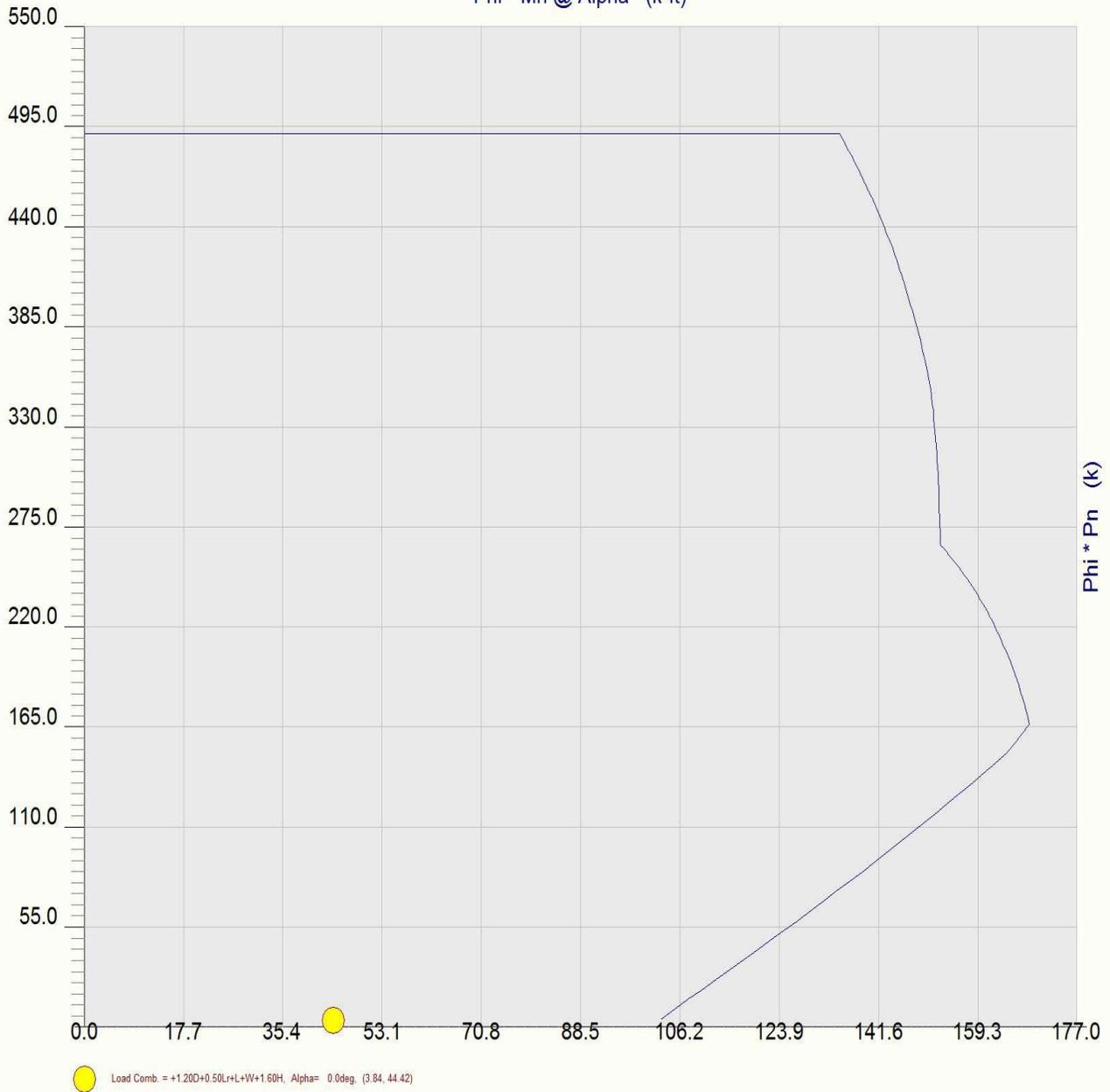
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DESCRIPTION: Building 4 Coastal Column Check - Typical 16x16

Concrete Column P-M Interaction Diagram

Phi * Mn @ Alpha (k-ft)



Concrete Column

LIC# : KW-06011269, Build:20.23.06.01

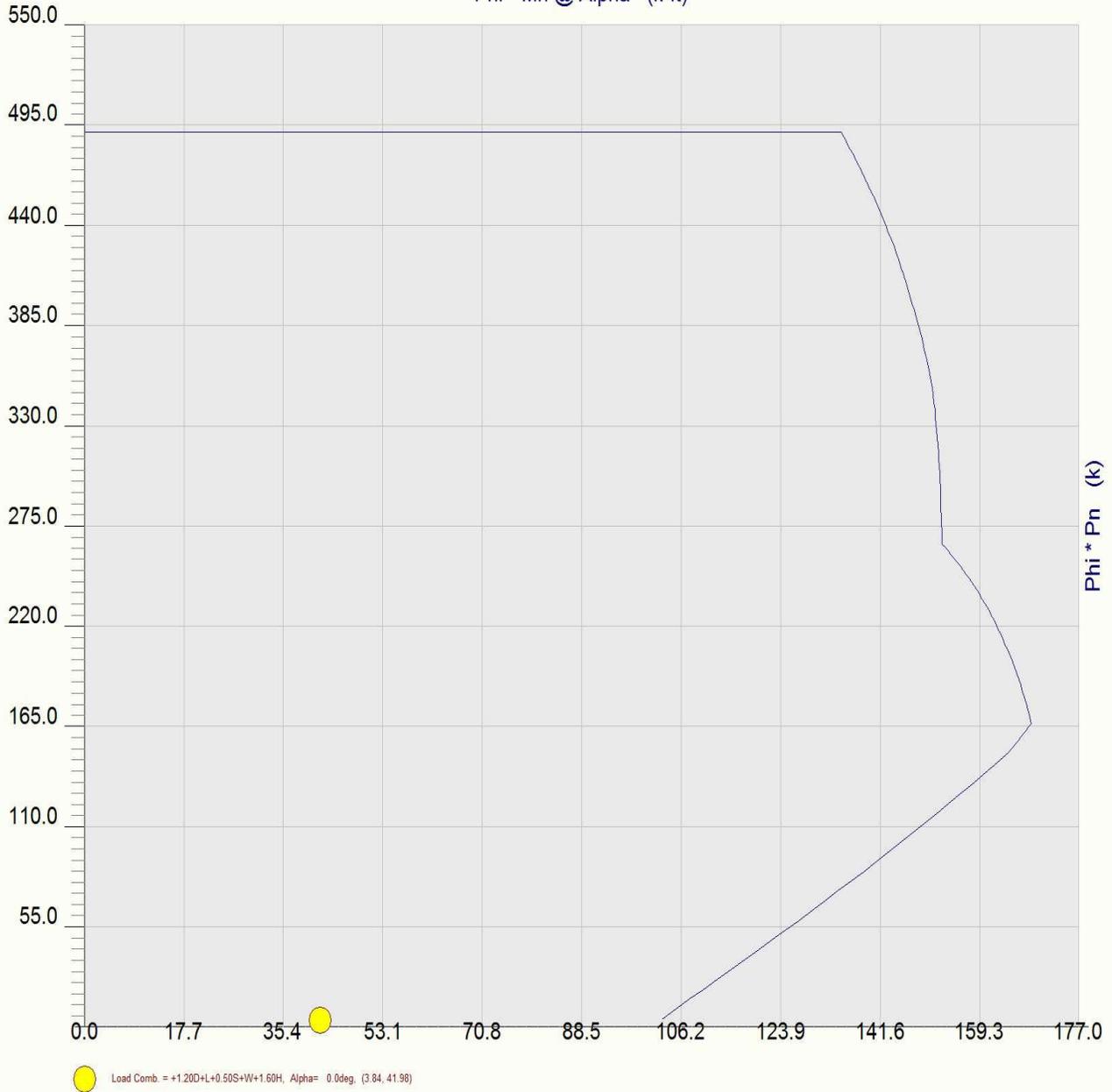
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Concrete Column P-M Interaction Diagram

Phi * Mn @ Alpha (k-ft)



Concrete Column

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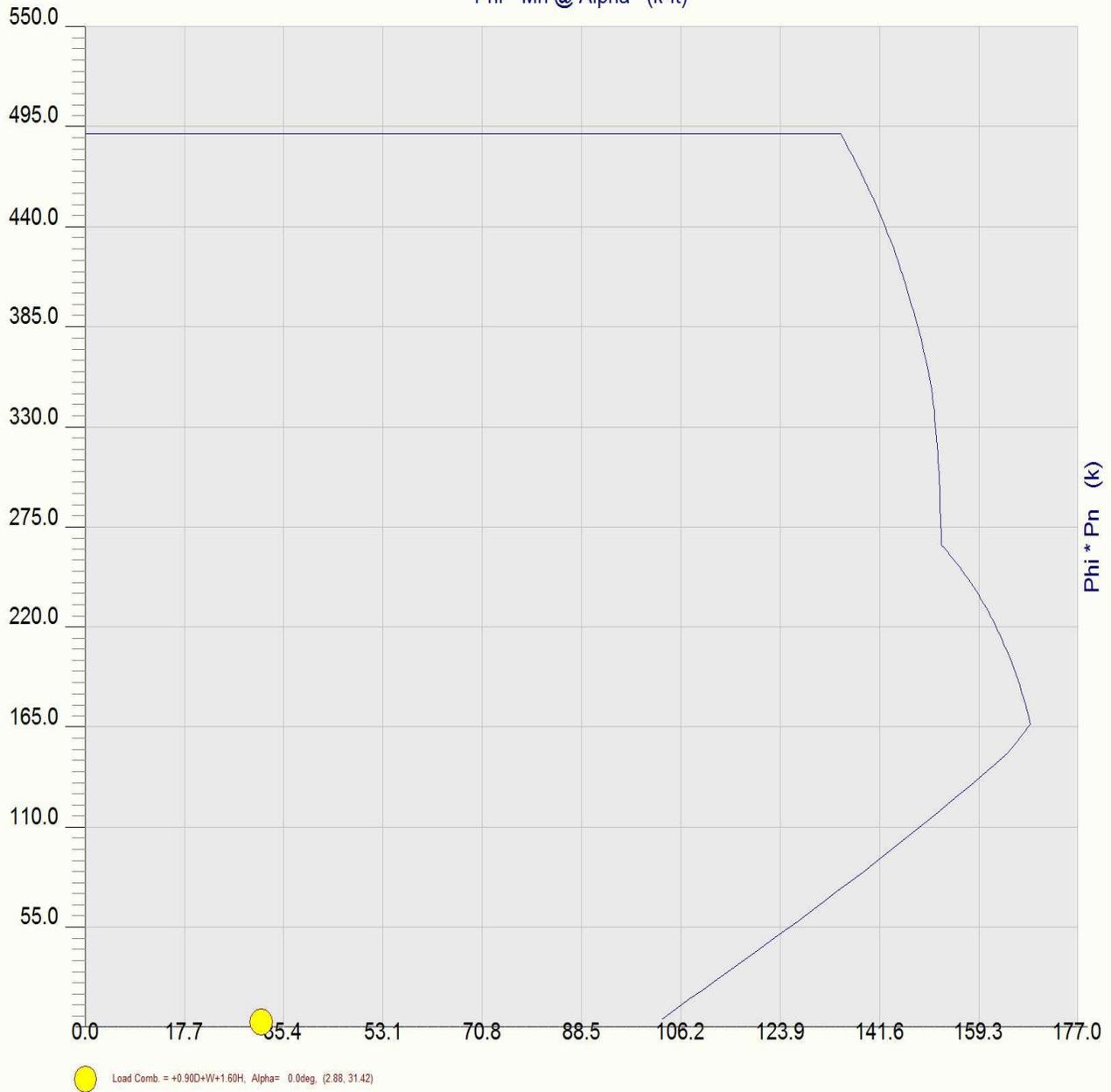
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DESCRIPTION: Building 4 Coastal Column Check - Typical 16x16

Concrete Column P-M Interaction Diagram

Phi * Mn @ Alpha (k-ft)



Concrete Column

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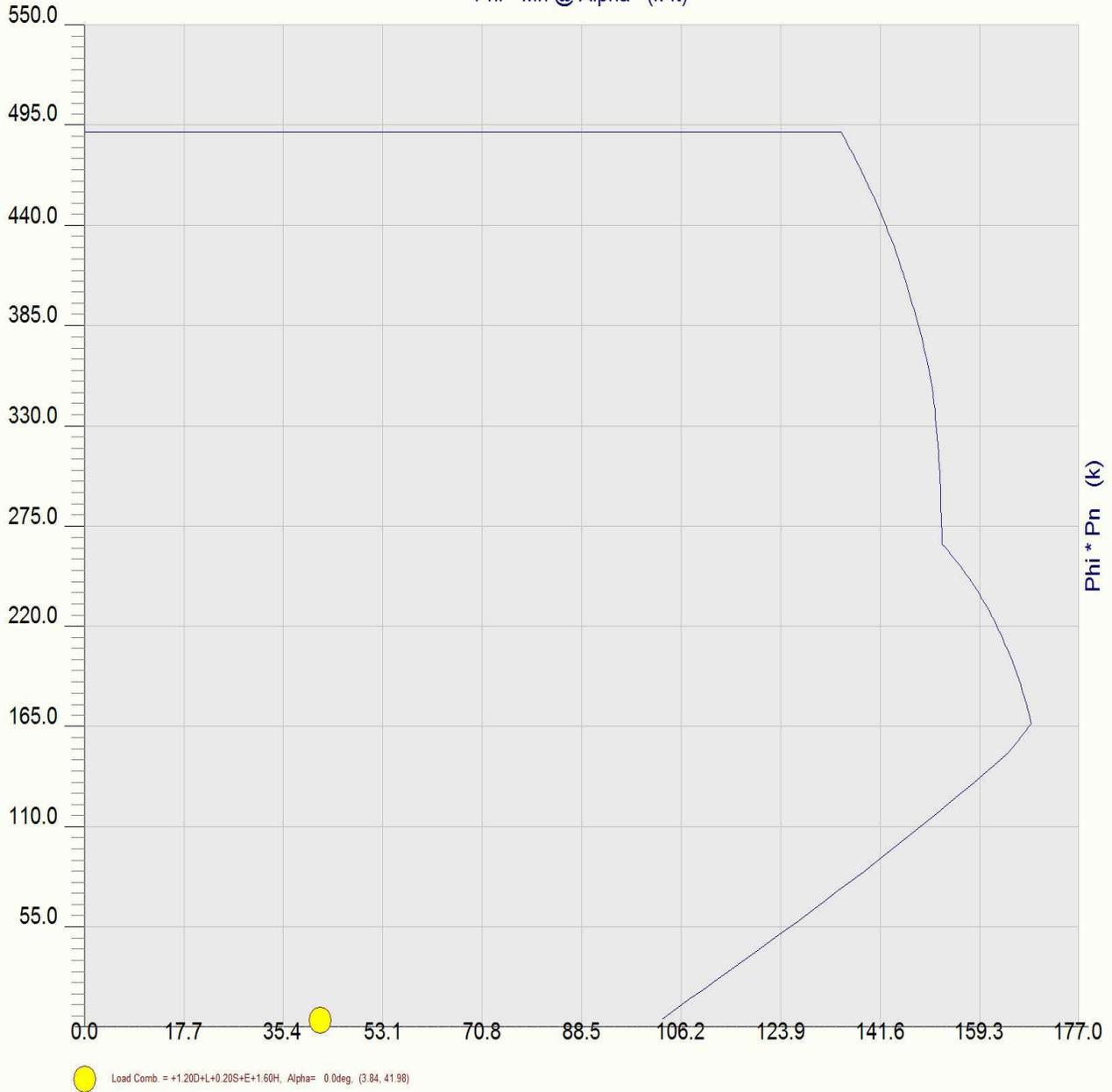
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DESCRIPTION: Building 4 Coastal Column Check - Typical 16x16

Concrete Column P-M Interaction Diagram

Phi * Mn @ Alpha (k-ft)



Concrete Column

LIC# : KW-06011269, Build:20.23.06.01

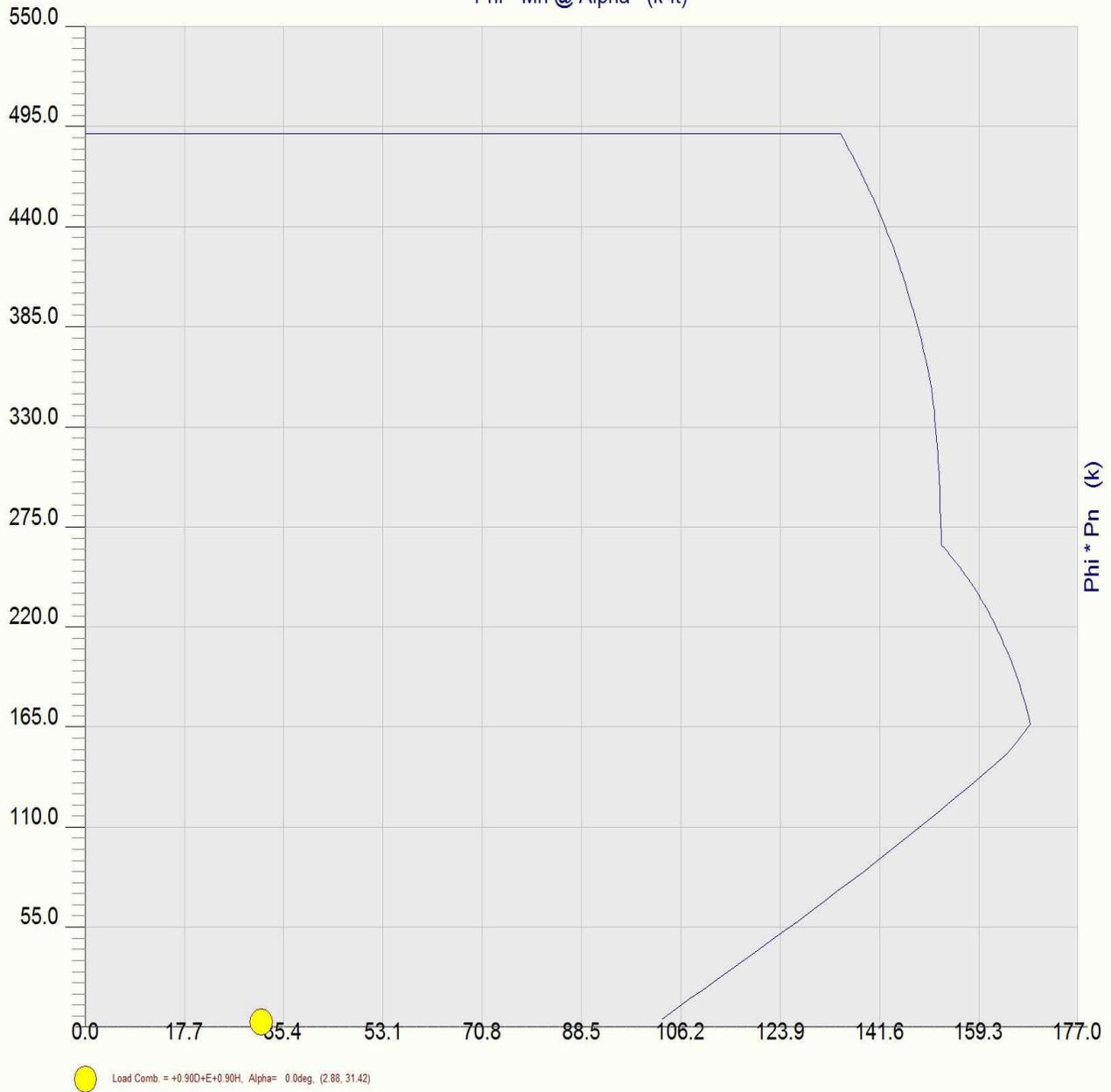
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DESCRIPTION: Building 4 Coastal Column Check - Typical 16x16

Concrete Column P-M Interaction Diagram

Phi * Mn @ Alpha (k-ft)



Concrete Slender Wall

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

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DESCRIPTION: Building 4 Wall

Code References

Calculations per ACI 318-14 Sec 11.8, IBC 2018, CBC 2019, ASCE 7-16

Load Combinations Used : ASCE 7-16

General Information

f_c : Concrete 28 day strength =	5.0 ksi	Wall Thickness	14.0 in	Temp Diff across thickness =	deg F
F_y : Rebar Yield =	60.0 ksi	Rebar at each face		Min Allow Out-of-Plane Defl Ratio =	0.0
E_c : Concrete Elastic Modulus =	3,122.0 ksi	Rebar "d" distance	2.0 in		
λ : Lt Wt Conc Fact =	1.0	Lower Level Rebar . . .		Min allow A_s/bd =	0.0020
F_r : Rupture Modulus =	353.553 psi	Bar Size #	8	Using Stiff. Reduction Factor per ACI 318-14	
Max Allow A_s/bd =	0.02125	Bar Spacing	7.0 in	Section 11.8.3	
Max $P_u/Ag = f_c *$ =	0.060				
Concrete Density =	144.0 pcf				
Width of Design Strip =	12.0 in				

One-Story Wall Dimensions

A Clear Height =	11.670 ft
B Parapet height =	1.670 ft

Wall Support Condition Top Pinned, Bottom F



Lateral Loads

Wind Loads :

Full area WIND load = 56.0 psf

Seismic Loads :

Wall Weight Seismic Load Input Method : Direct entry of Lateral Wall Weight
 Seismic Wall Lateral Load psf

$F_p = 1.0 = 0.0$ psf

	D	Lr	L	E	W	Height	(Applied to full "STRIP Width")
Point Lateral Load	8.90	4.90			k	3.90 ft	

Concrete Slender Wall

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

(c) ENERCALC INC 1983-2023

DESCRIPTION: Building 4 Wall

DESIGN SUMMARY

Results reported for "Strip Width" of 12.0 in

Governing Load Combination . . .	Actual Values . . .	Allowable Values . . .
PASS Moment Capacity Check +1.20D+2.0Lr+W	Maximum Bending Stress Ratio 0.6596 Max Mu -44.835 k-ft	Phi * Mn 67.978 k-ft
PASS Service Deflection Check +D+Lr+H	Actual Defl. Ratio L/ 2,494 Max. Deflection 0.05616 in	Allowable Defl. Ratio 150.0
PASS Axial Load Check +1.20D+2.0Lr+W	Max Pu / Ag 2.905 psi Location 0.1945 ft	Max. Allow. Defl. 0.9336 in 0.06 * f'c 300.0 psi
PASS Reinforcing Limit Check OK per ACI 318 Section 22.2	Actual As/bd 0.009405	Max Allow As/bd 0.02125
Maximum Reactions for Load Combination...		
	Top Horizontal +D+Lr+H	2.159 k
	Base Horizontal +D+Lr+H	11.641 k
	Vertical Reaction +D+H	2.241 k

Design Maximum Combinations - Moments

Results reported for "Strip Width" = 12 in.

Load Combination	Axial Load			Mu k-ft	Moment Values			As in ²	As Ratio	0.6 * rho bal	Bar 'd'
	Pu k	0.06*f'c*b*t k	Mcr k-ft		Phi	Phi Mn k-ft	As in ²				
+1.20D+2.0Lr+W at 0.00 to 0.39	0.000	50.400	11.55	44.83	0.90	67.98	1.354	0.0094	0.0213	12.00	
+0.90D+2.0Lr+W at 0.00 to 0.39	0.000	50.400	11.55	38.93	0.90	67.98	1.354	0.0094	0.0213	12.00	

Design Maximum Combinations - Deflections

Results reported for "Strip Width" = 12 in.

Load Combination	Axial Load Pu k	Moment Values			Stiffness			Deflections	
		Mcr k-ft	Mactual k-ft	I gross in ⁴	I cracked in ⁴	I effective in ⁴	Deflection in	Defl. Ratio	
+D+H at 5.45 to 5.84	1.326	11.55	9.09	2,744.00	1,163.95	2058.000	0.028	5,005.5	
+D+L+H at 5.45 to 5.84	1.326	11.55	9.09	2,744.00	1,163.95	2058.000	0.028	5,005.5	
+D+Lr+H at 5.45 to 5.84	1.326	11.55	13.02	2,744.00	1,163.95	1595.481	0.056	2,493.5	
+D+S+H at 5.45 to 5.84	1.326	11.55	9.09	2,744.00	1,163.95	2058.000	0.028	5,005.5	
+D+0.750Lr+0.750L+H at 5.06 to 5.45	1.392	11.55	12.51	2,744.00	1,164.40	1713.842	0.048	2,890.8	
+D+0.750L+0.750S+H at 5.45 to 5.84	1.326	11.55	9.09	2,744.00	1,163.95	2058.000	0.028	5,005.5	
+D+0.60W+H at 5.45 to 5.84	1.326	11.55	9.33	2,744.00	1,163.95	2058.000	0.029	4,818.1	
+D+0.750Lr+0.750L+0.450W+H at 5.06 to 5.45	1.392	11.55	12.85	2,744.00	1,164.40	1633.273	0.050	2,804.4	
+D+0.750L+0.750S+0.450W+H at 5.45 to 5.84	1.326	11.55	9.31	2,744.00	1,163.95	2058.000	0.029	4,883.6	
+0.60D+0.60W+0.60H at 5.84 to 6.22	0.756	11.55	4.77	2,744.00	1,160.25	2058.000	0.015	9,384.3	
+D+0.70E+0.60H at 5.45 to 5.84	1.326	11.55	9.09	2,744.00	1,163.95	2058.000	0.028	5,005.5	
+D+0.750L+0.750S+0.5250E+H at 5.45 to 5.84	1.326	11.55	9.09	2,744.00	1,163.95	2058.000	0.028	5,005.5	
+0.60D+0.70E+H at 5.84 to 6.22	0.756	11.55	4.50	2,744.00	1,160.25	2058.000	0.014	9,901.8	
D Only at 5.45 to 5.84	1.326	11.55	9.09	2,744.00	1,163.95	2058.000	0.028	5,005.5	
Lr Only at 5.84 to 6.22	0.000	11.55	4.11	2,744.00	1,155.24	2058.000	0.013	10,830.0	
	0.000	0.00	0.00	0.00	0.00	0.000	0.000	0.0	
	0.000	0.00	0.00	0.00	0.00	0.000	0.000	0.0	
W Only at 6.61 to 7.00	0.000	11.55	0.50	2,744.00	1,155.24	2058.000	0.001	99,371.7	
	0.000	0.00	0.00	0.00	0.00	0.000	0.000	0.0	
	0.000	0.00	0.00	0.00	0.00	0.000	0.000	0.0	

Reactions - Vertical & Horizontal

Load Combination	Base Horizontal	Top Horizontal	Vertical @ Wall Base
+D+H	7.4 k	1.51 k	2.241 k
+D+L+H	7.4 k	1.51 k	2.241 k
+D+Lr+H	11.6 k	2.16 k	2.241 k

Concrete Slender Wall

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

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DESCRIPTION: Building 4 Wall

+D+S+H	7.4 k	1.51 k	2.241 k
+D+0.750Lr+0.750L+H	10.6 k	1.95 k	2.241 k
+D+0.750L+0.750S+H	7.4 k	1.51 k	2.241 k
+D+0.60W+H	7.6 k	1.71 k	2.241 k
+D+0.750Lr+0.750L+0.450W+H	10.8 k	2.13 k	2.241 k
+D+0.750L+0.750S+0.450W+H	7.6 k	1.67 k	2.241 k
+0.60D+0.60W+0.60H	4.8 k	1.00 k	1.345 k
+D+0.70E+0.60H	7.4 k	1.51 k	2.241 k
+D+0.750L+0.750S+0.5250E+H	7.4 k	1.51 k	2.241 k
+0.60D+0.70E+H	4.5 k	0.80 k	1.345 k
D Only	7.4 k	1.51 k	2.241 k
Lr Only	4.2 k	0.73 k	0.000 k
L Only	0.0 k	0.00 k	0.000 k

Reactions - Vertical & Horizontal

Load Combination	Base Horizontal	Top Horizontal	Vertical @ Wall Base
S Only	0.0 k	0.00 k	0.000 k
W Only	0.4 k	0.35 k	0.000 k
E Only	0.0 k	0.00 k	0.000 k
H Only	0.0 k	0.00 k	0.000 k

Deflections - Service Loads

Load Combination Location	Axial Load (k)	Moments (k-ft)		Inertia (in ⁴)			Iterated Deflection (in)	
		Mcr	Mu	Igross	Icracked	Ieff	Deflection	Ratio
Overall MAXimum Envelope								
... +D+Lr+H at 11.28 to 11.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.003	999.0
... +D+Lr+H at 10.89 to 11.28	0.41	11.55	1.26	2,744.000	1,157.90	2,058.000	0.008	999.0
... +D+Lr+H at 10.50 to 10.89	0.47	11.55	2.10	2,744.000	1,158.35	2,058.000	0.012	999.0
... +D+Lr+H at 10.11 to 10.50	0.54	11.55	2.94	2,744.000	1,158.80	2,058.000	0.017	999.0
... +D+Lr+H at 9.73 to 10.11	0.61	11.55	3.78	2,744.000	1,159.25	2,058.000	0.022	999.0
... +D+Lr+H at 9.34 to 9.73	0.67	11.55	4.62	2,744.000	1,159.57	2,058.000	0.027	999.0
... +D+Lr+H at 8.95 to 9.34	0.74	11.55	5.46	2,744.000	1,160.02	2,058.000	0.031	999.0
... +D+Lr+H at 8.56 to 8.95	0.80	11.55	6.30	2,744.000	1,160.47	2,058.000	0.035	999.0
... +D+Lr+H at 8.17 to 8.56	0.87	11.55	7.14	2,744.000	1,160.92	2,058.000	0.039	999.0
... +D+Lr+H at 7.78 to 8.17	0.93	11.55	7.98	2,744.000	1,161.37	2,058.000	0.043	999.0
... +D+Lr+H at 7.39 to 7.78	1.00	11.55	8.82	2,744.000	1,161.82	2,058.000	0.046	999.0
... +D+Lr+H at 7.00 to 7.39	1.06	11.55	9.66	2,744.000	1,162.27	2,058.000	0.049	999.0
... +D+Lr+H at 6.61 to 7.00	1.13	11.55	10.50	2,744.000	1,162.59	2,058.000	0.052	999.0
... +D+Lr+H at 6.22 to 6.61	1.19	11.55	11.34	2,744.000	1,163.04	2,058.000	0.054	999.0
... +D+Lr+H at 5.84 to 6.22	1.26	11.55	12.18	2,744.000	1,163.49	1,808.950	0.055	999.0
... +D+Lr+H at 5.45 to 5.84	1.33	11.55	13.02	2,744.000	1,163.95	1,595.481	0.056	999.0
... +D+Lr+H at 5.06 to 5.45	1.39	11.55	13.86	2,744.000	1,164.40	1,454.346	0.056	999.0
... +D+Lr+H at 4.67 to 5.06	1.46	11.55	14.70	2,744.000	1,164.85	1,354.651	0.055	999.0
... +D+Lr+H at 4.28 to 4.67	1.52	11.55	15.54	2,744.000	1,165.17	1,280.759	0.053	999.0
... +D+Lr+H at 3.89 to 4.28	1.58	11.55	16.31	2,744.000	1,165.57	1,228.311	0.050	999.0
... +D+Lr+H at 3.50 to 3.89	1.64	11.55	14.40	2,744.000	1,166.00	1,387.945	0.045	999.0
... +D+Lr+H at 3.11 to 3.50	1.70	11.55	9.87	2,744.000	1,166.44	2,058.000	0.040	999.0
... +D+Lr+H at 2.72 to 3.11	1.77	11.55	5.34	2,744.000	1,166.89	2,058.000	0.034	999.0
... +D+Lr+H at 2.33 to 2.72	1.83	11.55	0.81	2,744.000	1,167.21	2,058.000	0.028	999.0
... +D+Lr+H at 1.95 to 2.33	1.90	11.55	3.72	2,744.000	1,167.66	2,058.000	0.022	999.0

Project Title:
 Engineer:
 Project ID:
 Project Descr:

Concrete Slender Wall

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

(c) ENERCALC INC 1983-2023

DESCRIPTION: Building 4 Wall

...+D+Lr+H at 1.56 to 1.95	1.97	11.55	8.25	2,744.000	1,168.11	2,058.000	0.016	999.0
...+D+Lr+H at 1.17 to 1.56	2.03	11.55	12.77	2,744.000	1,168.57	1,651.453	0.010	999.0
...+D+Lr+H at 0.78 to 1.17	2.10	11.55	17.30	2,744.000	1,169.03	1,177.994	0.006	999.0
...+D+Lr+H at 0.39 to 0.78	2.17	11.55	21.83	2,744.000	1,169.50	1,169.495	0.002	999.0
...+D+Lr+H at 0.00 to 0.39	0.00	11.55	28.62	2,744.000	1,155.24	1,155.243	0.000	999.0
+D+H								
...11.28 to 11.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.001	999.0
...10.89 to 11.28	0.41	11.55	0.88	2,744.000	1,157.90	2,058.000	0.004	999.0
...10.50 to 10.89	0.48	11.55	1.47	2,744.000	1,158.35	2,058.000	0.007	999.0
...10.11 to 10.50	0.54	11.55	2.05	2,744.000	1,158.80	2,058.000	0.009	999.0
...9.73 to 10.11	0.61	11.55	2.64	2,744.000	1,159.25	2,058.000	0.012	999.0
...9.34 to 9.73	0.67	11.55	3.23	2,744.000	1,159.58	2,058.000	0.015	999.0
...8.95 to 9.34	0.74	11.55	3.81	2,744.000	1,160.03	2,058.000	0.017	999.0
...8.56 to 8.95	0.80	11.55	4.40	2,744.000	1,160.48	2,058.000	0.019	999.0
...8.17 to 8.56	0.87	11.55	4.99	2,744.000	1,160.93	2,058.000	0.021	999.0

Deflections - Service Loads

Load Combination Location	Axial Load (k)	Moments (k-ft)		Inertia (in ⁴)			Iterated Deflection (in)	
		Mcr	Mu	I _{gross}	I _{cracked}	I _{eff}	Deflection	Ratio
...7.78 to 8.17	0.93	11.55	5.57	2,744.000	1,161.37	2,058.000	0.023	999.0
...7.39 to 7.78	1.00	11.55	6.16	2,744.000	1,161.82	2,058.000	0.024	999.0
...7.00 to 7.39	1.06	11.55	6.74	2,744.000	1,162.27	2,058.000	0.026	999.0
...6.61 to 7.00	1.13	11.55	7.33	2,744.000	1,162.60	2,058.000	0.027	999.0
...6.22 to 6.61	1.20	11.55	7.92	2,744.000	1,163.05	2,058.000	0.027	999.0
...5.84 to 6.22	1.26	11.55	8.50	2,744.000	1,163.50	2,058.000	0.028	999.0
...5.45 to 5.84	1.33	11.55	9.09	2,744.000	1,163.95	2,058.000	0.028	999.0
...5.06 to 5.45	1.39	11.55	9.68	2,744.000	1,164.40	2,058.000	0.028	999.0
...4.67 to 5.06	1.46	11.55	10.26	2,744.000	1,164.85	2,058.000	0.027	999.0
...4.28 to 4.67	1.52	11.55	10.85	2,744.000	1,165.17	2,058.000	0.026	999.0
...3.89 to 4.28	1.58	11.55	11.39	2,744.000	1,165.60	2,058.000	0.024	999.0
...3.50 to 3.89	1.65	11.55	10.20	2,744.000	1,166.05	2,058.000	0.022	999.0
...3.11 to 3.50	1.71	11.55	7.33	2,744.000	1,166.49	2,058.000	0.020	999.0
...2.72 to 3.11	1.78	11.55	4.45	2,744.000	1,166.94	2,058.000	0.017	999.0
...2.33 to 2.72	1.84	11.55	1.57	2,744.000	1,167.39	2,058.000	0.014	999.0
...1.95 to 2.33	1.91	11.55	1.30	2,744.000	1,167.71	2,058.000	0.011	999.0
...1.56 to 1.95	1.98	11.55	4.18	2,744.000	1,168.16	2,058.000	0.008	999.0
...1.17 to 1.56	2.04	11.55	7.05	2,744.000	1,168.61	2,058.000	0.006	999.0
...0.78 to 1.17	2.11	11.55	9.93	2,744.000	1,169.06	2,058.000	0.003	999.0
...0.39 to 0.78	2.17	11.55	12.81	2,744.000	1,169.52	1,644.582	0.001	999.0
...0.00 to 0.39	0.00	11.55	17.12	2,744.000	1,155.24	1,176.393	0.000	999.0
+D+L+H								
...11.28 to 11.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.001	999.0
...10.89 to 11.28	0.41	11.55	0.88	2,744.000	1,157.90	2,058.000	0.004	999.0
...10.50 to 10.89	0.48	11.55	1.47	2,744.000	1,158.35	2,058.000	0.007	999.0
...10.11 to 10.50	0.54	11.55	2.05	2,744.000	1,158.80	2,058.000	0.009	999.0
...9.73 to 10.11	0.61	11.55	2.64	2,744.000	1,159.25	2,058.000	0.012	999.0
...9.34 to 9.73	0.67	11.55	3.23	2,744.000	1,159.58	2,058.000	0.015	999.0
...8.95 to 9.34	0.74	11.55	3.81	2,744.000	1,160.03	2,058.000	0.017	999.0
...8.56 to 8.95	0.80	11.55	4.40	2,744.000	1,160.48	2,058.000	0.019	999.0
...8.17 to 8.56	0.87	11.55	4.99	2,744.000	1,160.93	2,058.000	0.021	999.0
...7.78 to 8.17	0.93	11.55	5.57	2,744.000	1,161.37	2,058.000	0.023	999.0
...7.39 to 7.78	1.00	11.55	6.16	2,744.000	1,161.82	2,058.000	0.024	999.0

Project Title:
 Engineer:
 Project ID:
 Project Descr:

Concrete Slender Wall

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

(c) ENERCALC INC 1983-2023

DESCRIPTION: Building 4 Wall

... 7.00 to 7.39	1.06	11.55	6.74	2,744.000	1,162.27	2,058.000	0.026	999.0
... 6.61 to 7.00	1.13	11.55	7.33	2,744.000	1,162.60	2,058.000	0.027	999.0
... 6.22 to 6.61	1.20	11.55	7.92	2,744.000	1,163.05	2,058.000	0.027	999.0
... 5.84 to 6.22	1.26	11.55	8.50	2,744.000	1,163.50	2,058.000	0.028	999.0
... 5.45 to 5.84	1.33	11.55	9.09	2,744.000	1,163.95	2,058.000	0.028	999.0
... 5.06 to 5.45	1.39	11.55	9.68	2,744.000	1,164.40	2,058.000	0.028	999.0
... 4.67 to 5.06	1.46	11.55	10.26	2,744.000	1,164.85	2,058.000	0.027	999.0
... 4.28 to 4.67	1.52	11.55	10.85	2,744.000	1,165.17	2,058.000	0.026	999.0
... 3.89 to 4.28	1.58	11.55	11.39	2,744.000	1,165.60	2,058.000	0.024	999.0
... 3.50 to 3.89	1.65	11.55	10.20	2,744.000	1,166.05	2,058.000	0.022	999.0
... 3.11 to 3.50	1.71	11.55	7.33	2,744.000	1,166.49	2,058.000	0.020	999.0
... 2.72 to 3.11	1.78	11.55	4.45	2,744.000	1,166.94	2,058.000	0.017	999.0
... 2.33 to 2.72	1.84	11.55	1.57	2,744.000	1,167.39	2,058.000	0.014	999.0
... 1.95 to 2.33	1.91	11.55	1.30	2,744.000	1,167.71	2,058.000	0.011	999.0
... 1.56 to 1.95	1.98	11.55	4.18	2,744.000	1,168.16	2,058.000	0.008	999.0

Deflections - Service Loads

Load Combination Location	Axial Load (k)	Moments (k-ft)		Inertia (in ⁴)			Iterated Deflection (in)	
		Mcr	Mu	I _{gross}	I _{cracked}	I _{eff}	Deflection	Ratio
... 1.17 to 1.56	2.04	11.55	7.05	2,744.000	1,168.61	2,058.000	0.006	999.0
... 0.78 to 1.17	2.11	11.55	9.93	2,744.000	1,169.06	2,058.000	0.003	999.0
... 0.39 to 0.78	2.17	11.55	12.81	2,744.000	1,169.52	1,644.582	0.001	999.0
... 0.00 to 0.39	0.00	11.55	17.12	2,744.000	1,155.24	1,176.393	0.000	999.0
+D+Lr+H								
... 11.28 to 11.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.003	999.0
... 10.89 to 11.28	0.41	11.55	1.26	2,744.000	1,157.90	2,058.000	0.008	999.0
... 10.50 to 10.89	0.47	11.55	2.10	2,744.000	1,158.35	2,058.000	0.012	999.0
... 10.11 to 10.50	0.54	11.55	2.94	2,744.000	1,158.80	2,058.000	0.017	999.0
... 9.73 to 10.11	0.61	11.55	3.78	2,744.000	1,159.25	2,058.000	0.022	999.0
... 9.34 to 9.73	0.67	11.55	4.62	2,744.000	1,159.57	2,058.000	0.027	999.0
... 8.95 to 9.34	0.74	11.55	5.46	2,744.000	1,160.02	2,058.000	0.031	999.0
... 8.56 to 8.95	0.80	11.55	6.30	2,744.000	1,160.47	2,058.000	0.035	999.0
... 8.17 to 8.56	0.87	11.55	7.14	2,744.000	1,160.92	2,058.000	0.039	999.0
... 7.78 to 8.17	0.93	11.55	7.98	2,744.000	1,161.37	2,058.000	0.043	999.0
... 7.39 to 7.78	1.00	11.55	8.82	2,744.000	1,161.82	2,058.000	0.046	999.0
... 7.00 to 7.39	1.06	11.55	9.66	2,744.000	1,162.27	2,058.000	0.049	999.0
... 6.61 to 7.00	1.13	11.55	10.50	2,744.000	1,162.59	2,058.000	0.052	999.0
... 6.22 to 6.61	1.19	11.55	11.34	2,744.000	1,163.04	2,058.000	0.054	999.0
... 5.84 to 6.22	1.26	11.55	12.18	2,744.000	1,163.49	1,808.950	0.055	999.0
... 5.45 to 5.84	1.33	11.55	13.02	2,744.000	1,163.95	1,595.481	0.056	999.0
... 5.06 to 5.45	1.39	11.55	13.86	2,744.000	1,164.40	1,454.346	0.056	999.0
... 4.67 to 5.06	1.46	11.55	14.70	2,744.000	1,164.85	1,354.651	0.055	999.0
... 4.28 to 4.67	1.52	11.55	15.54	2,744.000	1,165.17	1,280.759	0.053	999.0
... 3.89 to 4.28	1.58	11.55	16.31	2,744.000	1,165.57	1,228.311	0.050	999.0
... 3.50 to 3.89	1.64	11.55	14.40	2,744.000	1,166.00	1,387.945	0.045	999.0
... 3.11 to 3.50	1.70	11.55	9.87	2,744.000	1,166.44	2,058.000	0.040	999.0
... 2.72 to 3.11	1.77	11.55	5.34	2,744.000	1,166.89	2,058.000	0.034	999.0
... 2.33 to 2.72	1.83	11.55	0.81	2,744.000	1,167.21	2,058.000	0.028	999.0
... 1.95 to 2.33	1.90	11.55	3.72	2,744.000	1,167.66	2,058.000	0.022	999.0
... 1.56 to 1.95	1.97	11.55	8.25	2,744.000	1,168.11	2,058.000	0.016	999.0
... 1.17 to 1.56	2.03	11.55	12.77	2,744.000	1,168.57	1,651.453	0.010	999.0
... 0.78 to 1.17	2.10	11.55	17.30	2,744.000	1,169.03	1,177.994	0.006	999.0

Concrete Slender Wall

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

(c) ENERCALC INC 1983-2023

DESCRIPTION: Building 4 Wall

... 0.39 to 0.78	2.17	11.55	21.83	2,744.000	1,169.50	1,169.495	0.002	999.0
... 0.00 to 0.39	0.00	11.55	28.62	2,744.000	1,155.24	1,155.243	0.000	999.0
+D+S+H								
... 11.28 to 11.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.001	999.0
... 10.89 to 11.28	0.41	11.55	0.88	2,744.000	1,157.90	2,058.000	0.004	999.0
... 10.50 to 10.89	0.48	11.55	1.47	2,744.000	1,158.35	2,058.000	0.007	999.0
... 10.11 to 10.50	0.54	11.55	2.05	2,744.000	1,158.80	2,058.000	0.009	999.0
... 9.73 to 10.11	0.61	11.55	2.64	2,744.000	1,159.25	2,058.000	0.012	999.0
... 9.34 to 9.73	0.67	11.55	3.23	2,744.000	1,159.58	2,058.000	0.015	999.0
... 8.95 to 9.34	0.74	11.55	3.81	2,744.000	1,160.03	2,058.000	0.017	999.0
... 8.56 to 8.95	0.80	11.55	4.40	2,744.000	1,160.48	2,058.000	0.019	999.0
... 8.17 to 8.56	0.87	11.55	4.99	2,744.000	1,160.93	2,058.000	0.021	999.0
... 7.78 to 8.17	0.93	11.55	5.57	2,744.000	1,161.37	2,058.000	0.023	999.0
... 7.39 to 7.78	1.00	11.55	6.16	2,744.000	1,161.82	2,058.000	0.024	999.0
... 7.00 to 7.39	1.06	11.55	6.74	2,744.000	1,162.27	2,058.000	0.026	999.0

Deflections - Service Loads

Load Combination Location	Axial Load (k)	Moments (k-ft)		Inertia (in ⁴)			Iterated Deflection (in)	
		Mcr	Mu	I _{gross}	I _{cracked}	I _{eff}	Deflection	Ratio
... 6.61 to 7.00	1.13	11.55	7.33	2,744.000	1,162.60	2,058.000	0.027	999.0
... 6.22 to 6.61	1.20	11.55	7.92	2,744.000	1,163.05	2,058.000	0.027	999.0
... 5.84 to 6.22	1.26	11.55	8.50	2,744.000	1,163.50	2,058.000	0.028	999.0
... 5.45 to 5.84	1.33	11.55	9.09	2,744.000	1,163.95	2,058.000	0.028	999.0
... 5.06 to 5.45	1.39	11.55	9.68	2,744.000	1,164.40	2,058.000	0.028	999.0
... 4.67 to 5.06	1.46	11.55	10.26	2,744.000	1,164.85	2,058.000	0.027	999.0
... 4.28 to 4.67	1.52	11.55	10.85	2,744.000	1,165.17	2,058.000	0.026	999.0
... 3.89 to 4.28	1.58	11.55	11.39	2,744.000	1,165.60	2,058.000	0.024	999.0
... 3.50 to 3.89	1.65	11.55	10.20	2,744.000	1,166.05	2,058.000	0.022	999.0
... 3.11 to 3.50	1.71	11.55	7.33	2,744.000	1,166.49	2,058.000	0.020	999.0
... 2.72 to 3.11	1.78	11.55	4.45	2,744.000	1,166.94	2,058.000	0.017	999.0
... 2.33 to 2.72	1.84	11.55	1.57	2,744.000	1,167.39	2,058.000	0.014	999.0
... 1.95 to 2.33	1.91	11.55	1.30	2,744.000	1,167.71	2,058.000	0.011	999.0
... 1.56 to 1.95	1.98	11.55	4.18	2,744.000	1,168.16	2,058.000	0.008	999.0
... 1.17 to 1.56	2.04	11.55	7.05	2,744.000	1,168.61	2,058.000	0.006	999.0
... 0.78 to 1.17	2.11	11.55	9.93	2,744.000	1,169.06	2,058.000	0.003	999.0
... 0.39 to 0.78	2.17	11.55	12.81	2,744.000	1,169.52	1,644.582	0.001	999.0
... 0.00 to 0.39	0.00	11.55	17.12	2,744.000	1,155.24	1,176.393	0.000	999.0
+D+0.750Lr+0.750L+H								
... 11.28 to 11.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.002	999.0
... 10.89 to 11.28	0.41	11.55	1.14	2,744.000	1,157.90	2,058.000	0.007	999.0
... 10.50 to 10.89	0.47	11.55	1.90	2,744.000	1,158.35	2,058.000	0.011	999.0
... 10.11 to 10.50	0.54	11.55	2.65	2,744.000	1,158.80	2,058.000	0.015	999.0
... 9.73 to 10.11	0.61	11.55	3.41	2,744.000	1,159.25	2,058.000	0.019	999.0
... 9.34 to 9.73	0.67	11.55	4.17	2,744.000	1,159.57	2,058.000	0.023	999.0
... 8.95 to 9.34	0.74	11.55	4.93	2,744.000	1,160.02	2,058.000	0.027	999.0
... 8.56 to 8.95	0.80	11.55	5.69	2,744.000	1,160.47	2,058.000	0.031	999.0
... 8.17 to 8.56	0.87	11.55	6.45	2,744.000	1,160.92	2,058.000	0.034	999.0
... 7.78 to 8.17	0.93	11.55	7.20	2,744.000	1,161.37	2,058.000	0.037	999.0
... 7.39 to 7.78	1.00	11.55	7.96	2,744.000	1,161.82	2,058.000	0.040	999.0
... 7.00 to 7.39	1.06	11.55	8.72	2,744.000	1,162.27	2,058.000	0.042	999.0
... 6.61 to 7.00	1.13	11.55	9.48	2,744.000	1,162.59	2,058.000	0.044	999.0
... 6.22 to 6.61	1.19	11.55	10.24	2,744.000	1,163.04	2,058.000	0.046	999.0

Project Title:
 Engineer:
 Project ID:
 Project Descr:

Concrete Slender Wall

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

(c) ENERCALC INC 1983-2023

DESCRIPTION: Building 4 Wall

... 5.84 to 6.22	1.26	11.55	11.00	2,744.000	1,163.49	2,058.000	0.048	999.0
... 5.45 to 5.84	1.33	11.55	11.75	2,744.000	1,163.94	1,965.740	0.048	999.0
... 5.06 to 5.45	1.39	11.55	12.51	2,744.000	1,164.40	1,713.842	0.048	999.0
... 4.67 to 5.06	1.46	11.55	13.27	2,744.000	1,164.85	1,548.690	0.048	999.0
... 4.28 to 4.67	1.52	11.55	14.03	2,744.000	1,165.17	1,432.536	0.046	999.0
... 3.89 to 4.28	1.58	11.55	14.72	2,744.000	1,165.58	1,353.105	0.043	999.0
... 3.50 to 3.89	1.64	11.55	12.97	2,744.000	1,166.02	1,607.014	0.039	999.0
... 3.11 to 3.50	1.71	11.55	8.84	2,744.000	1,166.46	2,058.000	0.035	999.0
... 2.72 to 3.11	1.77	11.55	4.70	2,744.000	1,166.90	2,058.000	0.030	999.0
... 2.33 to 2.72	1.84	11.55	0.57	2,744.000	1,167.22	2,058.000	0.025	999.0
... 1.95 to 2.33	1.90	11.55	3.56	2,744.000	1,167.67	2,058.000	0.019	999.0
... 1.56 to 1.95	1.97	11.55	7.70	2,744.000	1,168.13	2,058.000	0.014	999.0
... 1.17 to 1.56	2.03	11.55	11.83	2,744.000	1,168.58	1,934.443	0.009	999.0
... 0.78 to 1.17	2.10	11.55	15.97	2,744.000	1,169.04	1,253.059	0.005	999.0
... 0.39 to 0.78	2.17	11.55	20.10	2,744.000	1,169.50	1,169.501	0.002	999.0

Deflections - Service Loads

Load Combination Location	Axial Load (k)	Moments (k-ft)		Inertia (in ⁴)			Iterated Deflection (in)	
		Mcr	Mu	I _{gross}	I _{cracked}	I _{eff}	Deflection	Ratio
... 0.00 to 0.39	0.00	11.55	26.30	2,744.000	1,155.24	1,155.243	0.000	999.0
+D+0.750L+0.750S+H								
... 11.28 to 11.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.001	999.0
... 10.89 to 11.28	0.41	11.55	0.88	2,744.000	1,157.90	2,058.000	0.004	999.0
... 10.50 to 10.89	0.48	11.55	1.47	2,744.000	1,158.35	2,058.000	0.007	999.0
... 10.11 to 10.50	0.54	11.55	2.05	2,744.000	1,158.80	2,058.000	0.009	999.0
... 9.73 to 10.11	0.61	11.55	2.64	2,744.000	1,159.25	2,058.000	0.012	999.0
... 9.34 to 9.73	0.67	11.55	3.23	2,744.000	1,159.58	2,058.000	0.015	999.0
... 8.95 to 9.34	0.74	11.55	3.81	2,744.000	1,160.03	2,058.000	0.017	999.0
... 8.56 to 8.95	0.80	11.55	4.40	2,744.000	1,160.48	2,058.000	0.019	999.0
... 8.17 to 8.56	0.87	11.55	4.99	2,744.000	1,160.93	2,058.000	0.021	999.0
... 7.78 to 8.17	0.93	11.55	5.57	2,744.000	1,161.37	2,058.000	0.023	999.0
... 7.39 to 7.78	1.00	11.55	6.16	2,744.000	1,161.82	2,058.000	0.024	999.0
... 7.00 to 7.39	1.06	11.55	6.74	2,744.000	1,162.27	2,058.000	0.026	999.0
... 6.61 to 7.00	1.13	11.55	7.33	2,744.000	1,162.60	2,058.000	0.027	999.0
... 6.22 to 6.61	1.20	11.55	7.92	2,744.000	1,163.05	2,058.000	0.027	999.0
... 5.84 to 6.22	1.26	11.55	8.50	2,744.000	1,163.50	2,058.000	0.028	999.0
... 5.45 to 5.84	1.33	11.55	9.09	2,744.000	1,163.95	2,058.000	0.028	999.0
... 5.06 to 5.45	1.39	11.55	9.68	2,744.000	1,164.40	2,058.000	0.028	999.0
... 4.67 to 5.06	1.46	11.55	10.26	2,744.000	1,164.85	2,058.000	0.027	999.0
... 4.28 to 4.67	1.52	11.55	10.85	2,744.000	1,165.17	2,058.000	0.026	999.0
... 3.89 to 4.28	1.58	11.55	11.39	2,744.000	1,165.60	2,058.000	0.024	999.0
... 3.50 to 3.89	1.65	11.55	10.20	2,744.000	1,166.05	2,058.000	0.022	999.0
... 3.11 to 3.50	1.71	11.55	7.33	2,744.000	1,166.49	2,058.000	0.020	999.0
... 2.72 to 3.11	1.78	11.55	4.45	2,744.000	1,166.94	2,058.000	0.017	999.0
... 2.33 to 2.72	1.84	11.55	1.57	2,744.000	1,167.39	2,058.000	0.014	999.0
... 1.95 to 2.33	1.91	11.55	1.30	2,744.000	1,167.71	2,058.000	0.011	999.0
... 1.56 to 1.95	1.98	11.55	4.18	2,744.000	1,168.16	2,058.000	0.008	999.0
... 1.17 to 1.56	2.04	11.55	7.05	2,744.000	1,168.61	2,058.000	0.006	999.0
... 0.78 to 1.17	2.11	11.55	9.93	2,744.000	1,169.06	2,058.000	0.003	999.0
... 0.39 to 0.78	2.17	11.55	12.81	2,744.000	1,169.52	1,644.582	0.001	999.0
... 0.00 to 0.39	0.00	11.55	17.12	2,744.000	1,155.24	1,176.393	0.000	999.0
+D+0.60W+H								

Project Title:
 Engineer:
 Project ID:
 Project Descr:

Concrete Slender Wall

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

(c) ENERCALC INC 1983-2023

DESCRIPTION: Building 4 Wall

... 11.28 to 11.67	0.00	11.55	0.05	2,744.000	1,155.24	2,058.000	0.001	999.0
... 10.89 to 11.28	0.41	11.55	0.91	2,744.000	1,157.90	2,058.000	0.004	999.0
... 10.50 to 10.89	0.48	11.55	1.55	2,744.000	1,158.35	2,058.000	0.007	999.0
... 10.11 to 10.50	0.54	11.55	2.18	2,744.000	1,158.80	2,058.000	0.010	999.0
... 9.73 to 10.11	0.61	11.55	2.80	2,744.000	1,159.25	2,058.000	0.013	999.0
... 9.34 to 9.73	0.67	11.55	3.42	2,744.000	1,159.58	2,058.000	0.015	999.0
... 8.95 to 9.34	0.74	11.55	4.04	2,744.000	1,160.03	2,058.000	0.018	999.0
... 8.56 to 8.95	0.80	11.55	4.64	2,744.000	1,160.47	2,058.000	0.020	999.0
... 8.17 to 8.56	0.87	11.55	5.25	2,744.000	1,160.92	2,058.000	0.022	999.0
... 7.78 to 8.17	0.93	11.55	5.85	2,744.000	1,161.37	2,058.000	0.024	999.0
... 7.39 to 7.78	1.00	11.55	6.44	2,744.000	1,161.82	2,058.000	0.025	999.0
... 7.00 to 7.39	1.06	11.55	7.03	2,744.000	1,162.27	2,058.000	0.027	999.0
... 6.61 to 7.00	1.13	11.55	7.61	2,744.000	1,162.60	2,058.000	0.028	999.0
... 6.22 to 6.61	1.20	11.55	8.19	2,744.000	1,163.05	2,058.000	0.029	999.0
... 5.84 to 6.22	1.26	11.55	8.77	2,744.000	1,163.50	2,058.000	0.029	999.0

Deflections - Service Loads

Load Combination Location	Axial Load (k)	Moments (k-ft)		Inertia (in ⁴)			Iterated Deflection (in)	
		Mcr	Mu	Igross	Icracked	Ieff	Deflection	Ratio
... 5.45 to 5.84	1.33	11.55	9.33	2,744.000	1,163.95	2,058.000	0.029	999.0
... 5.06 to 5.45	1.39	11.55	9.90	2,744.000	1,164.40	2,058.000	0.029	999.0
... 4.67 to 5.06	1.46	11.55	10.45	2,744.000	1,164.85	2,058.000	0.028	999.0
... 4.28 to 4.67	1.52	11.55	11.01	2,744.000	1,165.17	2,058.000	0.027	999.0
... 3.89 to 4.28	1.58	11.55	11.51	2,744.000	1,165.60	2,058.000	0.025	999.0
... 3.50 to 3.89	1.65	11.55	10.28	2,744.000	1,166.05	2,058.000	0.023	999.0
... 3.11 to 3.50	1.71	11.55	7.35	2,744.000	1,166.49	2,058.000	0.021	999.0
... 2.72 to 3.11	1.78	11.55	4.42	2,744.000	1,166.94	2,058.000	0.018	999.0
... 2.33 to 2.72	1.84	11.55	1.49	2,744.000	1,167.39	2,058.000	0.015	999.0
... 1.95 to 2.33	1.91	11.55	1.45	2,744.000	1,167.71	2,058.000	0.012	999.0
... 1.56 to 1.95	1.97	11.55	4.40	2,744.000	1,168.16	2,058.000	0.009	999.0
... 1.17 to 1.56	2.04	11.55	7.35	2,744.000	1,168.61	2,058.000	0.006	999.0
... 0.78 to 1.17	2.11	11.55	10.30	2,744.000	1,169.06	2,058.000	0.003	999.0
... 0.39 to 0.78	2.17	11.55	13.26	2,744.000	1,169.51	1,552.836	0.001	999.0
... 0.00 to 0.39	0.00	11.55	17.71	2,744.000	1,155.24	1,155.243	0.000	999.0
+D+0.750Lr+0.750L+0.450W+H								
... 11.28 to 11.67	0.00	11.55	0.04	2,744.000	1,155.24	2,058.000	0.002	999.0
... 10.89 to 11.28	0.41	11.55	1.18	2,744.000	1,157.90	2,058.000	0.007	999.0
... 10.50 to 10.89	0.47	11.55	1.98	2,744.000	1,158.35	2,058.000	0.011	999.0
... 10.11 to 10.50	0.54	11.55	2.78	2,744.000	1,158.80	2,058.000	0.016	999.0
... 9.73 to 10.11	0.61	11.55	3.58	2,744.000	1,159.25	2,058.000	0.020	999.0
... 9.34 to 9.73	0.67	11.55	4.37	2,744.000	1,159.57	2,058.000	0.024	999.0
... 8.95 to 9.34	0.74	11.55	5.16	2,744.000	1,160.02	2,058.000	0.028	999.0
... 8.56 to 8.95	0.80	11.55	5.95	2,744.000	1,160.47	2,058.000	0.032	999.0
... 8.17 to 8.56	0.87	11.55	6.73	2,744.000	1,160.92	2,058.000	0.035	999.0
... 7.78 to 8.17	0.93	11.55	7.51	2,744.000	1,161.37	2,058.000	0.038	999.0
... 7.39 to 7.78	1.00	11.55	8.28	2,744.000	1,161.82	2,058.000	0.041	999.0
... 7.00 to 7.39	1.06	11.55	9.05	2,744.000	1,162.27	2,058.000	0.044	999.0
... 6.61 to 7.00	1.13	11.55	9.82	2,744.000	1,162.59	2,058.000	0.046	999.0
... 6.22 to 6.61	1.19	11.55	10.58	2,744.000	1,163.04	2,058.000	0.048	999.0
... 5.84 to 6.22	1.26	11.55	11.34	2,744.000	1,163.49	2,058.000	0.049	999.0
... 5.45 to 5.84	1.33	11.55	12.10	2,744.000	1,163.95	1,837.943	0.050	999.0
... 5.06 to 5.45	1.39	11.55	12.85	2,744.000	1,164.40	1,633.273	0.050	999.0

Project Title:
 Engineer:
 Project ID:
 Project Descr:

Concrete Slender Wall

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

(c) ENERCALC INC 1983-2023

DESCRIPTION: Building 4 Wall

... 4.67 to 5.06	1.46	11.55	13.59	2,744.000	1,164.85	1,494.541	0.049	999.0
... 4.28 to 4.67	1.52	11.55	14.34	2,744.000	1,165.17	1,394.675	0.047	999.0
... 3.89 to 4.28	1.58	11.55	15.01	2,744.000	1,165.58	1,325.411	0.044	999.0
... 3.50 to 3.89	1.64	11.55	13.24	2,744.000	1,166.01	1,555.082	0.041	999.0
... 3.11 to 3.50	1.71	11.55	9.08	2,744.000	1,166.46	2,058.000	0.036	999.0
... 2.72 to 3.11	1.77	11.55	4.91	2,744.000	1,166.90	2,058.000	0.031	999.0
... 2.33 to 2.72	1.84	11.55	0.75	2,744.000	1,167.22	2,058.000	0.025	999.0
... 1.95 to 2.33	1.90	11.55	3.43	2,744.000	1,167.67	2,058.000	0.020	999.0
... 1.56 to 1.95	1.97	11.55	7.60	2,744.000	1,168.12	2,058.000	0.015	999.0
... 1.17 to 1.56	2.03	11.55	11.78	2,744.000	1,168.58	1,955.243	0.010	999.0
... 0.78 to 1.17	2.10	11.55	15.96	2,744.000	1,169.04	1,253.237	0.005	999.0
... 0.39 to 0.78	2.17	11.55	20.15	2,744.000	1,169.50	1,169.500	0.002	999.0
... 0.00 to 0.39	0.00	11.55	26.44	2,744.000	1,155.24	1,155.243	0.000	999.0
+D+0.750L+0.750S+0.450W+H								
... 11.28 to 11.67	0.00	11.55	0.04	2,744.000	1,155.24	2,058.000	0.001	999.0

Deflections - Service Loads

Load Combination Location	Axial Load (k)	Moments (k-ft)		Inertia (in ⁴)			Iterated Deflection (in)	
		Mcr	Mu	Igross	Icracked	Ieff	Deflection	Ratio
... 10.89 to 11.28	0.41	11.55	0.91	2,744.000	1,157.90	2,058.000	0.004	999.0
... 10.50 to 10.89	0.48	11.55	1.53	2,744.000	1,158.35	2,058.000	0.007	999.0
... 10.11 to 10.50	0.54	11.55	2.16	2,744.000	1,158.80	2,058.000	0.010	999.0
... 9.73 to 10.11	0.61	11.55	2.77	2,744.000	1,159.25	2,058.000	0.012	999.0
... 9.34 to 9.73	0.67	11.55	3.39	2,744.000	1,159.58	2,058.000	0.015	999.0
... 8.95 to 9.34	0.74	11.55	4.00	2,744.000	1,160.03	2,058.000	0.017	999.0
... 8.56 to 8.95	0.80	11.55	4.60	2,744.000	1,160.48	2,058.000	0.020	999.0
... 8.17 to 8.56	0.87	11.55	5.20	2,744.000	1,160.92	2,058.000	0.022	999.0
... 7.78 to 8.17	0.93	11.55	5.80	2,744.000	1,161.37	2,058.000	0.023	999.0
... 7.39 to 7.78	1.00	11.55	6.40	2,744.000	1,161.82	2,058.000	0.025	999.0
... 7.00 to 7.39	1.06	11.55	6.99	2,744.000	1,162.27	2,058.000	0.026	999.0
... 6.61 to 7.00	1.13	11.55	7.57	2,744.000	1,162.60	2,058.000	0.027	999.0
... 6.22 to 6.61	1.20	11.55	8.16	2,744.000	1,163.05	2,058.000	0.028	999.0
... 5.84 to 6.22	1.26	11.55	8.74	2,744.000	1,163.50	2,058.000	0.029	999.0
... 5.45 to 5.84	1.33	11.55	9.31	2,744.000	1,163.95	2,058.000	0.029	999.0
... 5.06 to 5.45	1.39	11.55	9.88	2,744.000	1,164.40	2,058.000	0.028	999.0
... 4.67 to 5.06	1.46	11.55	10.45	2,744.000	1,164.85	2,058.000	0.028	999.0
... 4.28 to 4.67	1.52	11.55	11.02	2,744.000	1,165.17	2,058.000	0.026	999.0
... 3.89 to 4.28	1.58	11.55	11.53	2,744.000	1,165.60	2,058.000	0.025	999.0
... 3.50 to 3.89	1.65	11.55	10.31	2,744.000	1,166.05	2,058.000	0.023	999.0
... 3.11 to 3.50	1.71	11.55	7.40	2,744.000	1,166.49	2,058.000	0.020	999.0
... 2.72 to 3.11	1.78	11.55	4.49	2,744.000	1,166.94	2,058.000	0.018	999.0
... 2.33 to 2.72	1.84	11.55	1.57	2,744.000	1,167.39	2,058.000	0.015	999.0
... 1.95 to 2.33	1.91	11.55	1.35	2,744.000	1,167.71	2,058.000	0.012	999.0
... 1.56 to 1.95	1.98	11.55	4.28	2,744.000	1,168.16	2,058.000	0.009	999.0
... 1.17 to 1.56	2.04	11.55	7.21	2,744.000	1,168.61	2,058.000	0.006	999.0
... 0.78 to 1.17	2.11	11.55	10.14	2,744.000	1,169.06	2,058.000	0.003	999.0
... 0.39 to 0.78	2.17	11.55	13.08	2,744.000	1,169.52	1,587.983	0.001	999.0
... 0.00 to 0.39	0.00	11.55	17.49	2,744.000	1,155.24	1,159.183	0.000	999.0
+0.60D+0.60W+0.60H								
... 11.28 to 11.67	0.00	11.55	0.05	2,744.000	1,155.24	2,058.000	0.001	999.0
... 10.89 to 11.28	0.25	11.55	0.50	2,744.000	1,156.84	2,058.000	0.002	999.0
... 10.50 to 10.89	0.29	11.55	0.86	2,744.000	1,157.03	2,058.000	0.004	999.0

Project Title:
 Engineer:
 Project ID:
 Project Descr:

Concrete Slender Wall

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

(c) ENERCALC INC 1983-2023

DESCRIPTION: Building 4 Wall

... 10.11 to 10.50	0.32	11.55	1.21	2,744.000	1,157.36	2,058.000	0.005	999.0
... 9.73 to 10.11	0.36	11.55	1.56	2,744.000	1,157.55	2,058.000	0.007	999.0
... 9.34 to 9.73	0.40	11.55	1.90	2,744.000	1,157.87	2,058.000	0.008	999.0
... 8.95 to 9.34	0.44	11.55	2.24	2,744.000	1,158.06	2,058.000	0.009	999.0
... 8.56 to 8.95	0.48	11.55	2.58	2,744.000	1,158.38	2,058.000	0.010	999.0
... 8.17 to 8.56	0.52	11.55	2.90	2,744.000	1,158.70	2,058.000	0.011	999.0
... 7.78 to 8.17	0.56	11.55	3.23	2,744.000	1,158.90	2,058.000	0.012	999.0
... 7.39 to 7.78	0.60	11.55	3.54	2,744.000	1,159.22	2,058.000	0.013	999.0
... 7.00 to 7.39	0.64	11.55	3.86	2,744.000	1,159.41	2,058.000	0.014	999.0
... 6.61 to 7.00	0.68	11.55	4.17	2,744.000	1,159.73	2,058.000	0.014	999.0
... 6.22 to 6.61	0.72	11.55	4.47	2,744.000	1,159.93	2,058.000	0.015	999.0
... 5.84 to 6.22	0.76	11.55	4.77	2,744.000	1,160.25	2,058.000	0.015	999.0
... 5.45 to 5.84	0.80	11.55	5.06	2,744.000	1,160.44	2,058.000	0.015	999.0
... 5.06 to 5.45	0.83	11.55	5.35	2,744.000	1,160.76	2,058.000	0.015	999.0
... 4.67 to 5.06	0.87	11.55	5.63	2,744.000	1,160.96	2,058.000	0.014	999.0

Deflections - Service Loads

Load Combination Location	Axial Load (k)	Moments (k-ft)		Inertia (in ⁴)			Iterated Deflection (in)	
		Mcr	Mu	Igross	Icracked	Ieff	Deflection	Ratio
... 4.28 to 4.67	0.91	11.55	5.90	2,744.000	1,161.28	2,058.000	0.014	999.0
... 3.89 to 4.28	0.95	11.55	6.15	2,744.000	1,161.46	2,058.000	0.013	999.0
... 3.50 to 3.89	0.99	11.55	5.35	2,744.000	1,161.78	2,058.000	0.011	999.0
... 3.11 to 3.50	1.03	11.55	3.54	2,744.000	1,161.98	2,058.000	0.010	999.0
... 2.72 to 3.11	1.07	11.55	1.72	2,744.000	1,162.30	2,058.000	0.009	999.0
... 2.33 to 2.72	1.11	11.55	0.11	2,744.000	1,162.49	2,058.000	0.007	999.0
... 1.95 to 2.33	1.15	11.55	1.94	2,744.000	1,162.81	2,058.000	0.005	999.0
... 1.56 to 1.95	1.19	11.55	3.78	2,744.000	1,163.00	2,058.000	0.004	999.0
... 1.17 to 1.56	1.23	11.55	5.62	2,744.000	1,163.32	2,058.000	0.003	999.0
... 0.78 to 1.17	1.27	11.55	7.46	2,744.000	1,163.52	2,058.000	0.001	999.0
... 0.39 to 0.78	1.30	11.55	9.31	2,744.000	1,163.84	2,058.000	0.001	999.0
... 0.00 to 0.39	0.00	11.55	12.10	2,744.000	1,155.24	1,834.073	0.000	999.0
+D+0.70E+0.60H								
... 11.28 to 11.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.001	999.0
... 10.89 to 11.28	0.41	11.55	0.88	2,744.000	1,157.90	2,058.000	0.004	999.0
... 10.50 to 10.89	0.48	11.55	1.47	2,744.000	1,158.35	2,058.000	0.007	999.0
... 10.11 to 10.50	0.54	11.55	2.05	2,744.000	1,158.80	2,058.000	0.009	999.0
... 9.73 to 10.11	0.61	11.55	2.64	2,744.000	1,159.25	2,058.000	0.012	999.0
... 9.34 to 9.73	0.67	11.55	3.23	2,744.000	1,159.58	2,058.000	0.015	999.0
... 8.95 to 9.34	0.74	11.55	3.81	2,744.000	1,160.03	2,058.000	0.017	999.0
... 8.56 to 8.95	0.80	11.55	4.40	2,744.000	1,160.48	2,058.000	0.019	999.0
... 8.17 to 8.56	0.87	11.55	4.99	2,744.000	1,160.93	2,058.000	0.021	999.0
... 7.78 to 8.17	0.93	11.55	5.57	2,744.000	1,161.37	2,058.000	0.023	999.0
... 7.39 to 7.78	1.00	11.55	6.16	2,744.000	1,161.82	2,058.000	0.024	999.0
... 7.00 to 7.39	1.06	11.55	6.74	2,744.000	1,162.27	2,058.000	0.026	999.0
... 6.61 to 7.00	1.13	11.55	7.33	2,744.000	1,162.60	2,058.000	0.027	999.0
... 6.22 to 6.61	1.20	11.55	7.92	2,744.000	1,163.05	2,058.000	0.027	999.0
... 5.84 to 6.22	1.26	11.55	8.50	2,744.000	1,163.50	2,058.000	0.028	999.0
... 5.45 to 5.84	1.33	11.55	9.09	2,744.000	1,163.95	2,058.000	0.028	999.0
... 5.06 to 5.45	1.39	11.55	9.68	2,744.000	1,164.40	2,058.000	0.028	999.0
... 4.67 to 5.06	1.46	11.55	10.26	2,744.000	1,164.85	2,058.000	0.027	999.0
... 4.28 to 4.67	1.52	11.55	10.85	2,744.000	1,165.17	2,058.000	0.026	999.0
... 3.89 to 4.28	1.58	11.55	11.39	2,744.000	1,165.60	2,058.000	0.024	999.0

Project Title:
 Engineer:
 Project ID:
 Project Descr:

Concrete Slender Wall

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

(c) ENERCALC INC 1983-2023

DESCRIPTION: Building 4 Wall

... 3.50 to 3.89	1.65	11.55	10.20	2,744.000	1,166.05	2,058.000	0.022	999.0
... 3.11 to 3.50	1.71	11.55	7.33	2,744.000	1,166.49	2,058.000	0.020	999.0
... 2.72 to 3.11	1.78	11.55	4.45	2,744.000	1,166.94	2,058.000	0.017	999.0
... 2.33 to 2.72	1.84	11.55	1.57	2,744.000	1,167.39	2,058.000	0.014	999.0
... 1.95 to 2.33	1.91	11.55	1.30	2,744.000	1,167.71	2,058.000	0.011	999.0
... 1.56 to 1.95	1.98	11.55	4.18	2,744.000	1,168.16	2,058.000	0.008	999.0
... 1.17 to 1.56	2.04	11.55	7.05	2,744.000	1,168.61	2,058.000	0.006	999.0
... 0.78 to 1.17	2.11	11.55	9.93	2,744.000	1,169.06	2,058.000	0.003	999.0
... 0.39 to 0.78	2.17	11.55	12.81	2,744.000	1,169.52	1,644.582	0.001	999.0
... 0.00 to 0.39	0.00	11.55	17.12	2,744.000	1,155.24	1,176.393	0.000	999.0
+D+0.750L+0.750S+0.5250E+H								
... 11.28 to 11.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.001	999.0
... 10.89 to 11.28	0.41	11.55	0.88	2,744.000	1,157.90	2,058.000	0.004	999.0
... 10.50 to 10.89	0.48	11.55	1.47	2,744.000	1,158.35	2,058.000	0.007	999.0
... 10.11 to 10.50	0.54	11.55	2.05	2,744.000	1,158.80	2,058.000	0.009	999.0

Deflections - Service Loads

Load Combination Location	Axial Load (k)	Moments (k-ft)		Inertia (in ⁴)			Iterated Deflection (in)	
		Mcr	Mu	Igross	Icracked	Ieff	Deflection	Ratio
... 9.73 to 10.11	0.61	11.55	2.64	2,744.000	1,159.25	2,058.000	0.012	999.0
... 9.34 to 9.73	0.67	11.55	3.23	2,744.000	1,159.58	2,058.000	0.015	999.0
... 8.95 to 9.34	0.74	11.55	3.81	2,744.000	1,160.03	2,058.000	0.017	999.0
... 8.56 to 8.95	0.80	11.55	4.40	2,744.000	1,160.48	2,058.000	0.019	999.0
... 8.17 to 8.56	0.87	11.55	4.99	2,744.000	1,160.93	2,058.000	0.021	999.0
... 7.78 to 8.17	0.93	11.55	5.57	2,744.000	1,161.37	2,058.000	0.023	999.0
... 7.39 to 7.78	1.00	11.55	6.16	2,744.000	1,161.82	2,058.000	0.024	999.0
... 7.00 to 7.39	1.06	11.55	6.74	2,744.000	1,162.27	2,058.000	0.026	999.0
... 6.61 to 7.00	1.13	11.55	7.33	2,744.000	1,162.60	2,058.000	0.027	999.0
... 6.22 to 6.61	1.20	11.55	7.92	2,744.000	1,163.05	2,058.000	0.027	999.0
... 5.84 to 6.22	1.26	11.55	8.50	2,744.000	1,163.50	2,058.000	0.028	999.0
... 5.45 to 5.84	1.33	11.55	9.09	2,744.000	1,163.95	2,058.000	0.028	999.0
... 5.06 to 5.45	1.39	11.55	9.68	2,744.000	1,164.40	2,058.000	0.028	999.0
... 4.67 to 5.06	1.46	11.55	10.26	2,744.000	1,164.85	2,058.000	0.027	999.0
... 4.28 to 4.67	1.52	11.55	10.85	2,744.000	1,165.17	2,058.000	0.026	999.0
... 3.89 to 4.28	1.58	11.55	11.39	2,744.000	1,165.60	2,058.000	0.024	999.0
... 3.50 to 3.89	1.65	11.55	10.20	2,744.000	1,166.05	2,058.000	0.022	999.0
... 3.11 to 3.50	1.71	11.55	7.33	2,744.000	1,166.49	2,058.000	0.020	999.0
... 2.72 to 3.11	1.78	11.55	4.45	2,744.000	1,166.94	2,058.000	0.017	999.0
... 2.33 to 2.72	1.84	11.55	1.57	2,744.000	1,167.39	2,058.000	0.014	999.0
... 1.95 to 2.33	1.91	11.55	1.30	2,744.000	1,167.71	2,058.000	0.011	999.0
... 1.56 to 1.95	1.98	11.55	4.18	2,744.000	1,168.16	2,058.000	0.008	999.0
... 1.17 to 1.56	2.04	11.55	7.05	2,744.000	1,168.61	2,058.000	0.006	999.0
... 0.78 to 1.17	2.11	11.55	9.93	2,744.000	1,169.06	2,058.000	0.003	999.0
... 0.39 to 0.78	2.17	11.55	12.81	2,744.000	1,169.52	1,644.582	0.001	999.0
... 0.00 to 0.39	0.00	11.55	17.12	2,744.000	1,155.24	1,176.393	0.000	999.0
+0.60D+0.70E+H								
... 11.28 to 11.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.001	999.0
... 10.89 to 11.28	0.25	11.55	0.47	2,744.000	1,156.84	2,058.000	0.002	999.0
... 10.50 to 10.89	0.29	11.55	0.78	2,744.000	1,157.03	2,058.000	0.004	999.0
... 10.11 to 10.50	0.32	11.55	1.09	2,744.000	1,157.36	2,058.000	0.005	999.0
... 9.73 to 10.11	0.36	11.55	1.40	2,744.000	1,157.55	2,058.000	0.006	999.0
... 9.34 to 9.73	0.40	11.55	1.71	2,744.000	1,157.87	2,058.000	0.007	999.0

Project Title:
 Engineer:
 Project ID:
 Project Descr:

Concrete Slender Wall

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

(c) ENERCALC INC 1983-2023

DESCRIPTION: Building 4 Wall

... 8.95 to 9.34	0.44	11.55	2.02	2,744.000	1,158.06	2,058.000	0.009	999.0
... 8.56 to 8.95	0.48	11.55	2.33	2,744.000	1,158.38	2,058.000	0.010	999.0
... 8.17 to 8.56	0.52	11.55	2.64	2,744.000	1,158.71	2,058.000	0.011	999.0
... 7.78 to 8.17	0.56	11.55	2.95	2,744.000	1,158.90	2,058.000	0.012	999.0
... 7.39 to 7.78	0.60	11.55	3.26	2,744.000	1,159.22	2,058.000	0.012	999.0
... 7.00 to 7.39	0.64	11.55	3.57	2,744.000	1,159.41	2,058.000	0.013	999.0
... 6.61 to 7.00	0.68	11.55	3.88	2,744.000	1,159.73	2,058.000	0.014	999.0
... 6.22 to 6.61	0.72	11.55	4.19	2,744.000	1,159.93	2,058.000	0.014	999.0
... 5.84 to 6.22	0.76	11.55	4.50	2,744.000	1,160.25	2,058.000	0.014	999.0
... 5.45 to 5.84	0.80	11.55	4.81	2,744.000	1,160.44	2,058.000	0.014	999.0
... 5.06 to 5.45	0.83	11.55	5.12	2,744.000	1,160.76	2,058.000	0.014	999.0
... 4.67 to 5.06	0.87	11.55	5.43	2,744.000	1,160.96	2,058.000	0.014	999.0
... 4.28 to 4.67	0.91	11.55	5.74	2,744.000	1,161.28	2,058.000	0.013	999.0
... 3.89 to 4.28	0.95	11.55	6.02	2,744.000	1,161.46	2,058.000	0.012	999.0
... 3.50 to 3.89	0.99	11.55	5.26	2,744.000	1,161.78	2,058.000	0.011	999.0

Deflections - Service Loads

Load Combination Location	Axial Load (k)	Moments (k-ft)		Inertia (in ⁴)			Iterated Deflection (in)	
		Mcr	Mu	I _{gross}	I _{cracked}	I _{eff}	Deflection	Ratio
... 3.11 to 3.50	1.03	11.55	3.50	2,744.000	1,161.98	2,058.000	0.010	999.0
... 2.72 to 3.11	1.07	11.55	1.73	2,744.000	1,162.30	2,058.000	0.008	999.0
... 2.33 to 2.72	1.11	11.55	0.04	2,744.000	1,162.49	2,058.000	0.007	999.0
... 1.95 to 2.33	1.15	11.55	1.81	2,744.000	1,162.81	2,058.000	0.005	999.0
... 1.56 to 1.95	1.19	11.55	3.57	2,744.000	1,163.00	2,058.000	0.004	999.0
... 1.17 to 1.56	1.23	11.55	5.34	2,744.000	1,163.32	2,058.000	0.002	999.0
... 0.78 to 1.17	1.27	11.55	7.11	2,744.000	1,163.52	2,058.000	0.001	999.0
... 0.39 to 0.78	1.30	11.55	8.88	2,744.000	1,163.84	2,058.000	0.001	999.0
... 0.00 to 0.39	0.00	11.55	11.53	2,744.000	1,155.24	2,058.000	0.000	999.0
D Only								
... 11.28 to 11.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.001	999.0
... 10.89 to 11.28	0.41	11.55	0.88	2,744.000	1,157.90	2,058.000	0.004	999.0
... 10.50 to 10.89	0.48	11.55	1.47	2,744.000	1,158.35	2,058.000	0.007	999.0
... 10.11 to 10.50	0.54	11.55	2.05	2,744.000	1,158.80	2,058.000	0.009	999.0
... 9.73 to 10.11	0.61	11.55	2.64	2,744.000	1,159.25	2,058.000	0.012	999.0
... 9.34 to 9.73	0.67	11.55	3.23	2,744.000	1,159.58	2,058.000	0.015	999.0
... 8.95 to 9.34	0.74	11.55	3.81	2,744.000	1,160.03	2,058.000	0.017	999.0
... 8.56 to 8.95	0.80	11.55	4.40	2,744.000	1,160.48	2,058.000	0.019	999.0
... 8.17 to 8.56	0.87	11.55	4.99	2,744.000	1,160.93	2,058.000	0.021	999.0
... 7.78 to 8.17	0.93	11.55	5.57	2,744.000	1,161.37	2,058.000	0.023	999.0
... 7.39 to 7.78	1.00	11.55	6.16	2,744.000	1,161.82	2,058.000	0.024	999.0
... 7.00 to 7.39	1.06	11.55	6.74	2,744.000	1,162.27	2,058.000	0.026	999.0
... 6.61 to 7.00	1.13	11.55	7.33	2,744.000	1,162.60	2,058.000	0.027	999.0
... 6.22 to 6.61	1.20	11.55	7.92	2,744.000	1,163.05	2,058.000	0.027	999.0
... 5.84 to 6.22	1.26	11.55	8.50	2,744.000	1,163.50	2,058.000	0.028	999.0
... 5.45 to 5.84	1.33	11.55	9.09	2,744.000	1,163.95	2,058.000	0.028	999.0
... 5.06 to 5.45	1.39	11.55	9.68	2,744.000	1,164.40	2,058.000	0.028	999.0
... 4.67 to 5.06	1.46	11.55	10.26	2,744.000	1,164.85	2,058.000	0.027	999.0
... 4.28 to 4.67	1.52	11.55	10.85	2,744.000	1,165.17	2,058.000	0.026	999.0
... 3.89 to 4.28	1.58	11.55	11.39	2,744.000	1,165.60	2,058.000	0.024	999.0
... 3.50 to 3.89	1.65	11.55	10.20	2,744.000	1,166.05	2,058.000	0.022	999.0
... 3.11 to 3.50	1.71	11.55	7.33	2,744.000	1,166.49	2,058.000	0.020	999.0
... 2.72 to 3.11	1.78	11.55	4.45	2,744.000	1,166.94	2,058.000	0.017	999.0

Project Title:
 Engineer:
 Project ID:
 Project Descr:

Concrete Slender Wall

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

(c) ENERCALC INC 1983-2023

DESCRIPTION: Building 4 Wall

... 2.33 to 2.72	1.84	11.55	1.57	2,744.000	1,167.39	2,058.000	0.014	999.0
... 1.95 to 2.33	1.91	11.55	1.30	2,744.000	1,167.71	2,058.000	0.011	999.0
... 1.56 to 1.95	1.98	11.55	4.18	2,744.000	1,168.16	2,058.000	0.008	999.0
... 1.17 to 1.56	2.04	11.55	7.05	2,744.000	1,168.61	2,058.000	0.006	999.0
... 0.78 to 1.17	2.11	11.55	9.93	2,744.000	1,169.06	2,058.000	0.003	999.0
... 0.39 to 0.78	2.17	11.55	12.81	2,744.000	1,169.52	1,644.582	0.001	999.0
... 0.00 to 0.39	0.00	11.55	17.12	2,744.000	1,155.24	1,176.393	0.000	999.0
Lr Only								
... 11.28 to 11.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.001	999.0
... 10.89 to 11.28	0.00	11.55	0.43	2,744.000	1,155.24	2,058.000	0.002	999.0
... 10.50 to 10.89	0.00	11.55	0.71	2,744.000	1,155.24	2,058.000	0.003	999.0
... 10.11 to 10.50	0.00	11.55	0.99	2,744.000	1,155.24	2,058.000	0.004	999.0
... 9.73 to 10.11	0.00	11.55	1.28	2,744.000	1,155.24	2,058.000	0.006	999.0
... 9.34 to 9.73	0.00	11.55	1.56	2,744.000	1,155.24	2,058.000	0.007	999.0
... 8.95 to 9.34	0.00	11.55	1.84	2,744.000	1,155.24	2,058.000	0.008	999.0

Deflections - Service Loads

Load Combination Location	Axial Load (k)	Moments (k-ft)		Inertia (in ⁴)			Iterated Deflection (in)	
		Mcr	Mu	Igross	Icracked	Ieff	Deflection	Ratio
... 8.56 to 8.95	0.00	11.55	2.13	2,744.000	1,155.24	2,058.000	0.009	999.0
... 8.17 to 8.56	0.00	11.55	2.41	2,744.000	1,155.24	2,058.000	0.010	999.0
... 7.78 to 8.17	0.00	11.55	2.70	2,744.000	1,155.24	2,058.000	0.011	999.0
... 7.39 to 7.78	0.00	11.55	2.98	2,744.000	1,155.24	2,058.000	0.011	999.0
... 7.00 to 7.39	0.00	11.55	3.26	2,744.000	1,155.24	2,058.000	0.012	999.0
... 6.61 to 7.00	0.00	11.55	3.55	2,744.000	1,155.24	2,058.000	0.012	999.0
... 6.22 to 6.61	0.00	11.55	3.83	2,744.000	1,155.24	2,058.000	0.013	999.0
... 5.84 to 6.22	0.00	11.55	4.11	2,744.000	1,155.24	2,058.000	0.013	999.0
... 5.45 to 5.84	0.00	11.55	4.40	2,744.000	1,155.24	2,058.000	0.013	999.0
... 5.06 to 5.45	0.00	11.55	4.68	2,744.000	1,155.24	2,058.000	0.013	999.0
... 4.67 to 5.06	0.00	11.55	4.97	2,744.000	1,155.24	2,058.000	0.012	999.0
... 4.28 to 4.67	0.00	11.55	5.25	2,744.000	1,155.24	2,058.000	0.012	999.0
... 3.89 to 4.28	0.00	11.55	5.51	2,744.000	1,155.24	2,058.000	0.011	999.0
... 3.50 to 3.89	0.00	11.55	4.81	2,744.000	1,155.24	2,058.000	0.010	999.0
... 3.11 to 3.50	0.00	11.55	3.19	2,744.000	1,155.24	2,058.000	0.009	999.0
... 2.72 to 3.11	0.00	11.55	1.57	2,744.000	1,155.24	2,058.000	0.007	999.0
... 2.33 to 2.72	0.00	11.55	0.05	2,744.000	1,155.24	2,058.000	0.006	999.0
... 1.95 to 2.33	0.00	11.55	1.67	2,744.000	1,155.24	2,058.000	0.005	999.0
... 1.56 to 1.95	0.00	11.55	3.30	2,744.000	1,155.24	2,058.000	0.003	999.0
... 1.17 to 1.56	0.00	11.55	4.92	2,744.000	1,155.24	2,058.000	0.002	999.0
... 0.78 to 1.17	0.00	11.55	6.54	2,744.000	1,155.24	2,058.000	0.001	999.0
... 0.39 to 0.78	0.00	11.55	8.16	2,744.000	1,155.24	2,058.000	0.000	999.0
... 0.00 to 0.39	0.00	11.55	10.60	2,744.000	1,155.24	2,058.000	0.000	999.0
L Only								
... 11.28 to 11.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 10.89 to 11.28	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 10.50 to 10.89	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 10.11 to 10.50	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 9.73 to 10.11	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 9.34 to 9.73	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 8.95 to 9.34	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 8.56 to 8.95	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 8.17 to 8.56	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0

Project Title:
 Engineer:
 Project ID:
 Project Descr:

Concrete Slender Wall

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

(c) ENERCALC INC 1983-2023

DESCRIPTION: Building 4 Wall

... 7.78 to 8.17	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 7.39 to 7.78	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 7.00 to 7.39	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 6.61 to 7.00	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 6.22 to 6.61	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 5.84 to 6.22	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 5.45 to 5.84	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 5.06 to 5.45	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 4.67 to 5.06	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 4.28 to 4.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 3.89 to 4.28	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 3.50 to 3.89	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 3.11 to 3.50	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 2.72 to 3.11	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 2.33 to 2.72	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0

Deflections - Service Loads

Load Combination Location	Axial Load (k)	Moments (k-ft)		Inertia (in^4)			Iterated Deflection (in)	
		Mcr	Mu	Igross	Icracked	Ieff	Deflection	Ratio
... 1.95 to 2.33	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 1.56 to 1.95	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 1.17 to 1.56	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 0.78 to 1.17	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 0.39 to 0.78	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 0.00 to 0.39	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
S Only								
... 11.28 to 11.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 10.89 to 11.28	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 10.50 to 10.89	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 10.11 to 10.50	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 9.73 to 10.11	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 9.34 to 9.73	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 8.95 to 9.34	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 8.56 to 8.95	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 8.17 to 8.56	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 7.78 to 8.17	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 7.39 to 7.78	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 7.00 to 7.39	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 6.61 to 7.00	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 6.22 to 6.61	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 5.84 to 6.22	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 5.45 to 5.84	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 5.06 to 5.45	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 4.67 to 5.06	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 4.28 to 4.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 3.89 to 4.28	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 3.50 to 3.89	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 3.11 to 3.50	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 2.72 to 3.11	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 2.33 to 2.72	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 1.95 to 2.33	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 1.56 to 1.95	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0

Project Title:
 Engineer:
 Project ID:
 Project Descr:

Concrete Slender Wall

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

(c) ENERCALC INC 1983-2023

DESCRIPTION: Building 4 Wall

... 1.17 to 1.56	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 0.78 to 1.17	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 0.39 to 0.78	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 0.00 to 0.39	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
W Only								
... 11.28 to 11.67	0.00	11.55	0.08	2,744.000	1,155.24	2,058.000	0.000	999.0
... 10.89 to 11.28	0.00	11.55	0.06	2,744.000	1,155.24	2,058.000	0.000	999.0
... 10.50 to 10.89	0.00	11.55	0.14	2,744.000	1,155.24	2,058.000	0.000	999.0
... 10.11 to 10.50	0.00	11.55	0.22	2,744.000	1,155.24	2,058.000	0.001	999.0
... 9.73 to 10.11	0.00	11.55	0.28	2,744.000	1,155.24	2,058.000	0.001	999.0
... 9.34 to 9.73	0.00	11.55	0.34	2,744.000	1,155.24	2,058.000	0.001	999.0
... 8.95 to 9.34	0.00	11.55	0.39	2,744.000	1,155.24	2,058.000	0.001	999.0
... 8.56 to 8.95	0.00	11.55	0.43	2,744.000	1,155.24	2,058.000	0.001	999.0
... 8.17 to 8.56	0.00	11.55	0.46	2,744.000	1,155.24	2,058.000	0.001	999.0
... 7.78 to 8.17	0.00	11.55	0.48	2,744.000	1,155.24	2,058.000	0.001	999.0

Deflections - Service Loads

Load Combination Location	Axial Load (k)	Moments (k-ft)		Inertia (in ⁴)			Iterated Deflection (in)	
		Mcr	Mu	Igross	Icracked	Ieff	Deflection	Ratio
... 7.39 to 7.78	0.00	11.55	0.50	2,744.000	1,155.24	2,058.000	0.001	999.0
... 7.00 to 7.39	0.00	11.55	0.50	2,744.000	1,155.24	2,058.000	0.001	999.0
... 6.61 to 7.00	0.00	11.55	0.50	2,744.000	1,155.24	2,058.000	0.001	999.0
... 6.22 to 6.61	0.00	11.55	0.49	2,744.000	1,155.24	2,058.000	0.001	999.0
... 5.84 to 6.22	0.00	11.55	0.47	2,744.000	1,155.24	2,058.000	0.001	999.0
... 5.45 to 5.84	0.00	11.55	0.44	2,744.000	1,155.24	2,058.000	0.001	999.0
... 5.06 to 5.45	0.00	11.55	0.40	2,744.000	1,155.24	2,058.000	0.001	999.0
... 4.67 to 5.06	0.00	11.55	0.36	2,744.000	1,155.24	2,058.000	0.001	999.0
... 4.28 to 4.67	0.00	11.55	0.31	2,744.000	1,155.24	2,058.000	0.001	999.0
... 3.89 to 4.28	0.00	11.55	0.24	2,744.000	1,155.24	2,058.000	0.001	999.0
... 3.50 to 3.89	0.00	11.55	0.17	2,744.000	1,155.24	2,058.000	0.001	999.0
... 3.11 to 3.50	0.00	11.55	0.10	2,744.000	1,155.24	2,058.000	0.001	999.0
... 2.72 to 3.11	0.00	11.55	0.01	2,744.000	1,155.24	2,058.000	0.001	999.0
... 2.33 to 2.72	0.00	11.55	0.09	2,744.000	1,155.24	2,058.000	0.001	999.0
... 1.95 to 2.33	0.00	11.55	0.19	2,744.000	1,155.24	2,058.000	0.000	999.0
... 1.56 to 1.95	0.00	11.55	0.30	2,744.000	1,155.24	2,058.000	0.000	999.0
... 1.17 to 1.56	0.00	11.55	0.43	2,744.000	1,155.24	2,058.000	0.000	999.0
... 0.78 to 1.17	0.00	11.55	0.55	2,744.000	1,155.24	2,058.000	0.000	999.0
... 0.39 to 0.78	0.00	11.55	0.69	2,744.000	1,155.24	2,058.000	0.000	999.0
... 0.00 to 0.39	0.00	11.55	0.91	2,744.000	1,155.24	2,058.000	0.000	999.0
E Only								
... 11.28 to 11.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 10.89 to 11.28	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 10.50 to 10.89	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 10.11 to 10.50	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 9.73 to 10.11	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 9.34 to 9.73	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 8.95 to 9.34	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 8.56 to 8.95	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 8.17 to 8.56	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 7.78 to 8.17	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 7.39 to 7.78	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 7.00 to 7.39	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0

Project Title:
 Engineer:
 Project ID:
 Project Descr:

Concrete Slender Wall

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

(c) ENERCALC INC 1983-2023

DESCRIPTION: Building 4 Wall

... 6.61 to 7.00	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 6.22 to 6.61	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 5.84 to 6.22	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 5.45 to 5.84	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 5.06 to 5.45	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 4.67 to 5.06	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 4.28 to 4.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 3.89 to 4.28	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 3.50 to 3.89	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 3.11 to 3.50	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 2.72 to 3.11	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 2.33 to 2.72	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 1.95 to 2.33	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 1.56 to 1.95	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 1.17 to 1.56	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0

Deflections - Service Loads

Load Combination Location	Axial Load (k)	Moments (k-ft)		Inertia (in ⁴)			Iterated Deflection (in)	
		Mcr	Mu	Igross	Icracked	Ieff	Deflection	Ratio
... 0.78 to 1.17	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 0.39 to 0.78	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 0.00 to 0.39	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
H Only								
... 11.28 to 11.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 10.89 to 11.28	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 10.50 to 10.89	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 10.11 to 10.50	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 9.73 to 10.11	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 9.34 to 9.73	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 8.95 to 9.34	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 8.56 to 8.95	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 8.17 to 8.56	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 7.78 to 8.17	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 7.39 to 7.78	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 7.00 to 7.39	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 6.61 to 7.00	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 6.22 to 6.61	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 5.84 to 6.22	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 5.45 to 5.84	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 5.06 to 5.45	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 4.67 to 5.06	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 4.28 to 4.67	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 3.89 to 4.28	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 3.50 to 3.89	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 3.11 to 3.50	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 2.72 to 3.11	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 2.33 to 2.72	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 1.95 to 2.33	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 1.56 to 1.95	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 1.17 to 1.56	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 0.78 to 1.17	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
... 0.39 to 0.78	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0

Project Title:
Engineer:
Project ID:
Project Descr:

Concrete Slender Wall

LIC# : KW-06011269, Build:20.23.06.01

Ramaker & Associates

(c) ENERCALC INC 1983-2023

DESCRIPTION: Building 4 Wall

... .0.00 to 0.39	0.00	11.55	0.00	2,744.000	1,155.24	2,058.000	0.000	0.0
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Building 4 Foundation Design

TABLE 1 – SUMMARY OF DRIVEN PILE CAPACITIES (Concrete)				
Pile Size (inches square)	Estimated Pile Embedment Depth ⁽¹⁾ (Feet)	Allowable Compression Capacity (tons)	Allowable Tension Capacity ⁽³⁾ (tons)	Allowable Lateral Capacity ⁽⁴⁾ (kips)
10	13-15	20	5.5 ⁽³⁾	5
12	13-15	28	6 ⁽³⁾	5
<p>(1) Embedment depth is based upon the ground surface elevation at the time of this field exploration program. If any fill material is placed at the site, the pile embedment depth must be increased to achieve the desired pile tip elevation.</p> <p>(2) The above tonnages are based upon the piles achieving tonnage within the fine sand layer that extend to a depth of approximately 15ft BGS. It is possible that some piles may not achieve the design capacity at the above provided depths, in which case these piles should be spliced and driven to deeper depths and/or helper piles may have to be installed. The actual final pile depths can be determined following completion of the test pile program.</p> <p>(3) The provided tonnages for tension support are based on full length or mechanically spliced piles.</p> <p>(4) For our analysis we assume the piles will be vertically aligned with at-grade pile head (Fixed Head Condition). The provided lateral loads will yield a deflection of less than 0.5 inches.</p> <p>(5) The impact of storm surge, wave impact forces and scour were not taken into account for our analysis.</p> <p>(6) Due to the proximity of surrounding structures, it may be necessary to pre-drill piling locations to limit vibration impacts.</p> <p>(7) To perform the above analysis boring B-12 was utilized, it was not performed within the footprint of the proposed structure, thus field conditions may vary.</p>				

All sitework and fill placement operations should be completed prior to the installation of piles to avoid adverse impacts such as damage to the piles and/or negative skin friction resulting in increased pile settlement. It is recommended that a minimum center-to-center pile spacing of 3 times the nominal pile diameter (e.g., 36 inch minimum spacing for 12 inch piles) be maintained. We estimate settlement of a single pile to be ½-inch or less, most of it due to elastic shortening of the pile.

UES should be retained to monitor the installation of the driven pile foundation system for this project. UES’s pile installation monitoring services will consist of monitoring the installation of each pile, documenting the number of hammer blows required to drive each pile for each linear foot, and evaluation of the pile driving records by a geotechnical engineer.

Once the pile size and pile driving equipment to be used for this project have been selected, a pile driving formula should be used to establish the pile driving criteria for the allowable pile load based on the pile driving hammer used. Each pile shall be driven until the established driving criteria have been achieved.

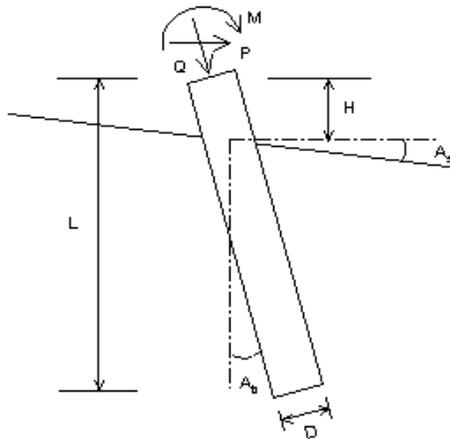
Pile load testing is not required for this project, in lieu of that, a minimum of five test piles should be driven at locations throughout the structure footprint to confirm the required production pile lengths. Test piles can be located at production pile locations and incorporated into the foundation system of the residential structure. Following the monitoring and evaluation of the test pile program by UES, production pile lengths and driving criteria can be finalized.

Piles should be driven with a hammer having a minimum energy proportionate to the size of the pile being driven. All pile driving operations should be performed in accordance with industry standards, applicable building codes, and the guidelines published by the Deep Foundations Institute (DFI).

12-inch square driven concrete piles, 15 feet embedment, Lateral load – 5 kips, Max. Moment – (-50.8 Kips-ft), Deflection – (-0.23 inch), 2 feet of unbraced length (assumed scour depth)

LATERAL ANALYSIS

Figure 2



Driving Concrete Pile

Loads:

Load Factor for Vertical Loads= 1.0
 Load Factor for Lateral Loads= 1.0
 Loads Supported by Pile Cap= 0 %
 Shear Condition: Static

(with Load Factor)

Vertical Load, Q= 36.0 -kp
 Shear Load, P= 5.0 -kp
 Moment, M= -50.8 -kp-f

Profile:

Pile Length, L= 15.0 -ft
 Top Height, H= 2 -ft
 Slope Angle, As= 0
 Batter Angle, Ab= 0

Soil Data:

Depth -ft	Gamma -lb/f3	Phi	C -kp/f2	K -lb/i3	e50 or Dr %	Nspt
0	114.9	33.0	0.00	45.0	34.78	10
2.5	52.5	33.0	0.00	32.5	34.78	10
4	59.1	36.5	0.00	68.5	54.49	20
6	59.1	36.5	0.00	68.2	54.35	20
15	36.5	26.5	0.00	2.7	6.19	1

Pile Data:

Depth -ft	Width -in	Area -in2	Per. -in	I -in4	E -kp/i2	Weight -kp/f
0.0	12	144.0	48.0	1728.0	3000	0.150
15.0	12	144.0	48.0	1728.0	3000	0.150

Single Pile Lateral Analysis:

Top Deflection, $y_t = -0.23400$ -in
 Max. Moment, $M = -50.75$ -kp-f
 Top Deflection Slope, $S_t = 0.00677$
 OK! Top Deflection, -0.2340 -in is less than the Allowable Deflection= 1.00-in

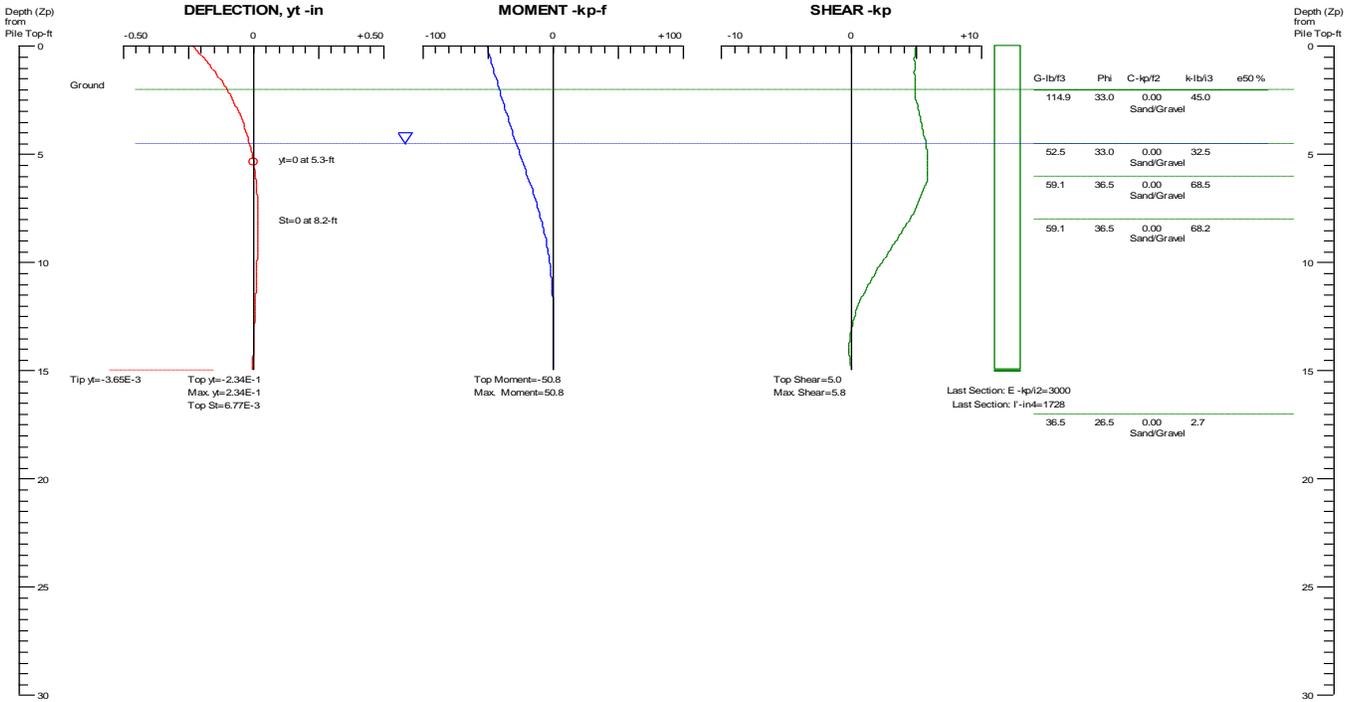
Note: If the program cannot find a result or the result exceeds the upper limit. The result will be displayed as 99999.
 The Max. Moment calculated by program is an internal force from the applied load conditions. Structural engineer has to check whether the pile has enough capacity to resist the moment with adequate factor of safety. If not, the pile may fail under the load conditions.



**CivilTech
Software**

**Margaritaville Resort
18-6322 (B-12)**

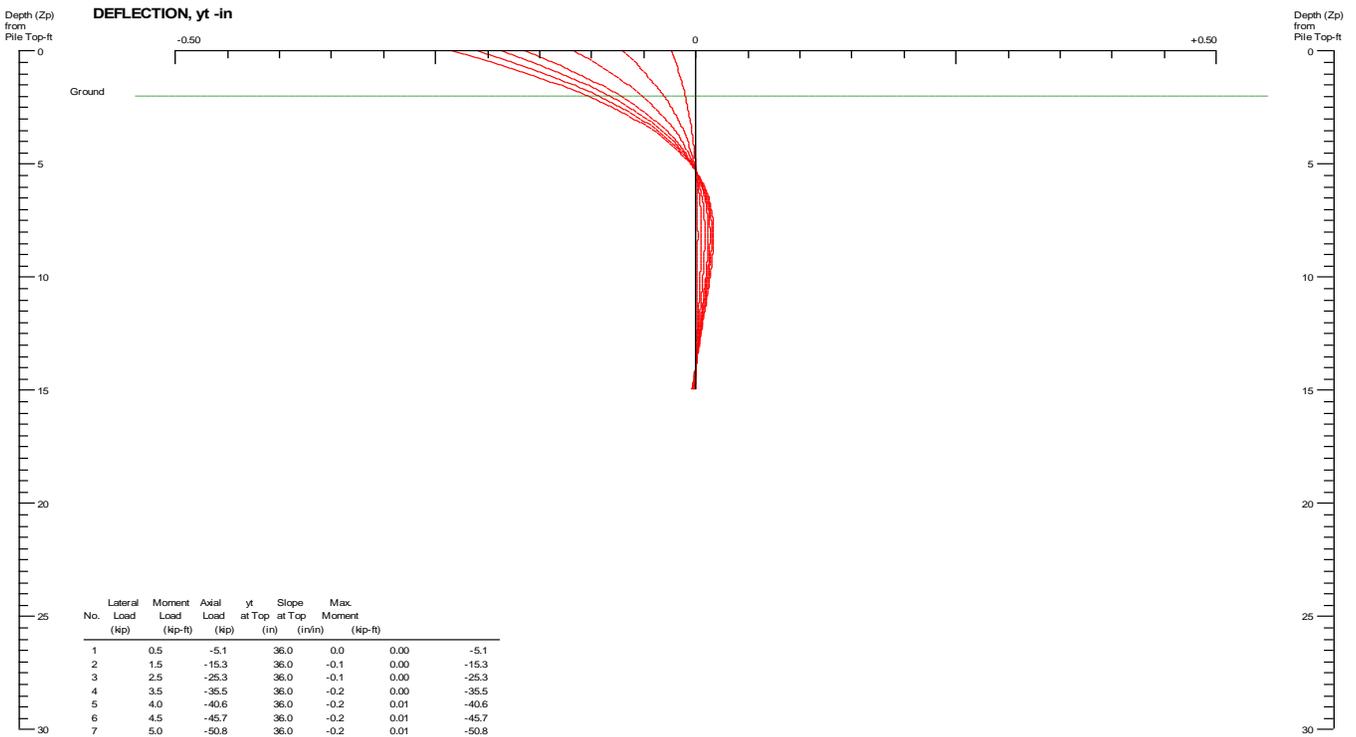
PILE DEFLECTION & FORCE vs DEPTH
Single Pile, Khead=1, Kbc=1



Margaritaville Resort
18-6322 (B-12)

Figure 2

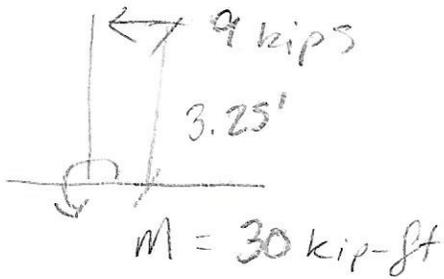
PILE DEFLECTION vs LOADING
Single Pile, Khead=1, Kbc=1



Margaritaville Resort
18-6322 (B-12)

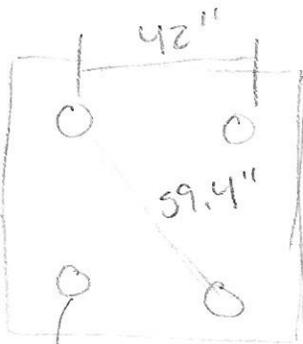
Figure 2

PILE CAP CAPACITIES DUE TO WAVE & DEBRIS HIT

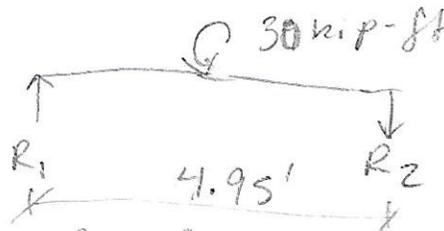


WAVE = .864 kips

DEBRIS = 8.2 kips



6.06 kips



$$\sum F_y = R_1 + R_2 = 0$$

$$\sum M_{R_1} = 30 \text{ k-ft} - R_2(4.95) = 0$$

$$R_2 = 6.06 \text{ kips}$$

FROM GFA 12" SQUARE PILE

COMP = 28 tons = 61.73 kips

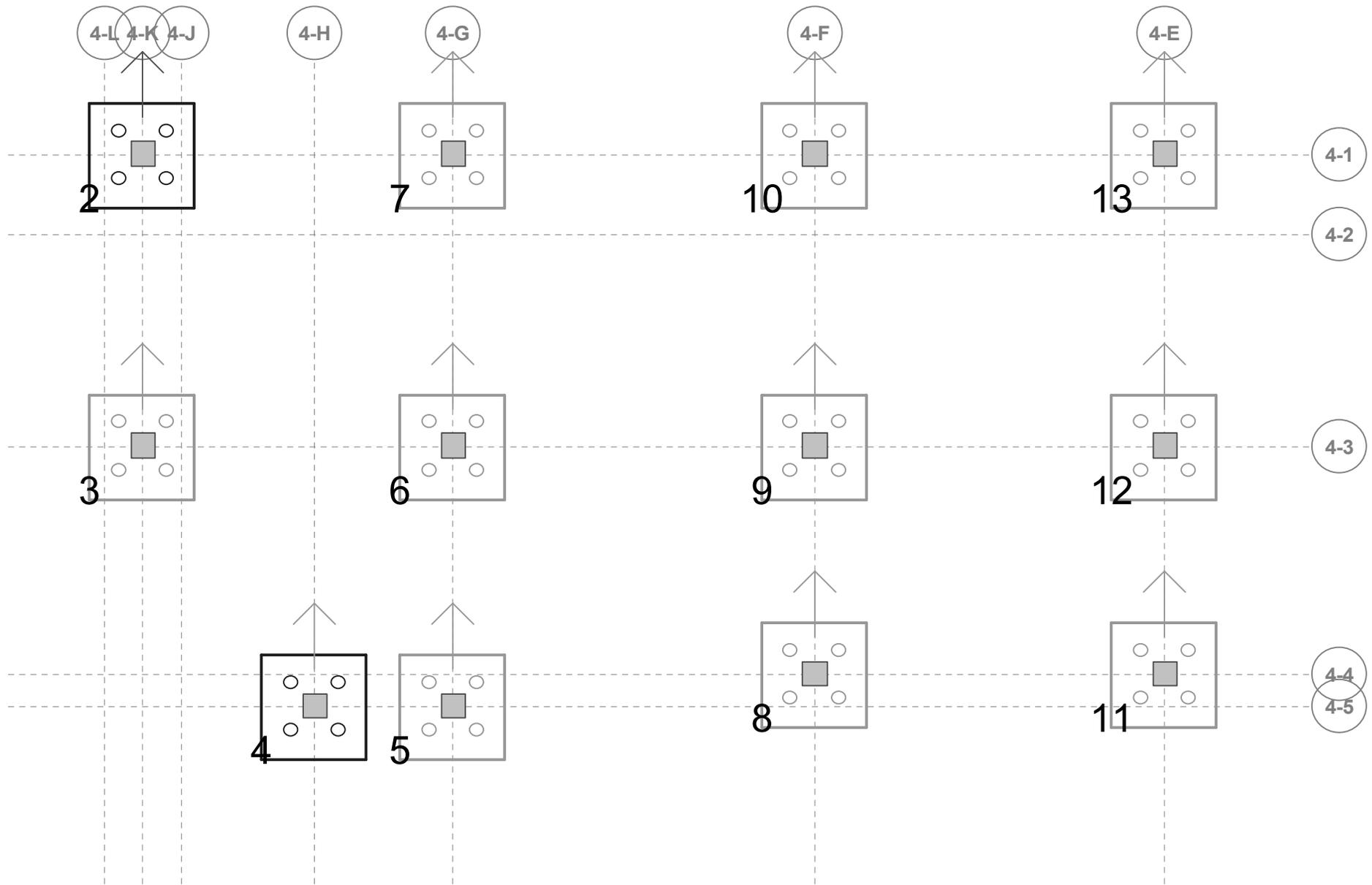
TEN = 6 tons = 13.23 kips

LATERAL = 5 kips

$$\text{LATERAL} = 5 \text{ kips} - \frac{9 \text{ kips}}{4 \text{ piles}} = 2.75 \text{ kips}$$

$$\text{COMP} = 61.73 - 6.06 \text{ kips} = 55.67 \text{ kips}$$

$$\text{TEN} = 13.23 - 6.06 \text{ kips} = 7.17 \text{ kips}$$





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PILE CAP DESIGN

Footing # 3 Footing Column Location: _____ (-2.50 - -18.33)
 Footing Orientation (deg): _____ 90.00 Column Orientation (deg): _____ 0.00
 Length (ft): _____ 6.50
 Width (ft): _____ 6.50
 Thickness (ft): _____ 2.50
 Bottom Reinf. Parallel to Length: 8 - #7 Width: 8 - #7
 Concrete f_c (ksi): 4.00 f_{ct} (ksi): CODE Density (pcf): 150.00 E_c (ksi): 3834.00
 Reinf. f_y (ksi): 60.00
 Pile Label: 12" 13-15ft - 4pile Pile Diameter: (in) 12.00 Pile Cap Label: 4 Pile Group
 Pile Spacing: (in) 36.00 Edge Spacing: (in) 21.00
 Column Size: 16x16

LOADS

Surcharge (ksf)	Dead Load:	0.400	Live Load:	0.000
Axial (kip)	Dead Load:	18.00		
	Pos. Live:	0.00	Neg. Live:	N/A
	Pos. Roof:	2.15	Neg. Roof:	N/A

CONCRETE CAPACITY

	Major	Ld Co/Code Ref.	Minor	Ld Co/Code Ref.
Required Shear (kip)	29.80	44	22.94	39
Provided Shear: (kip)	834.78	CRSI-02 Eq 13-2	802.41	CRSI-02 Eq 13-2
Required Moment: (kip-ft)	25.12	44	17.69	39
Provided Moment: (kip-ft)	475.62	N/A	456.72	N/A
Req. Col. Punching Shear: (kip)	56.81	45		
Prv. Col Punching Shear: (kip)	708.20	CRSI-02 Eq 13-1		

REINFORCEMENT

	Bottom Bars Parallel to		Top Bars Parallel to	
	Length	Width	Length	Width
Bar Quantity/Bar Size:	8-#7	8-#7	None	None
Required Steel/Provided Steel (in ²)	4.21/ 4.80	4.21/ 4.80	None	None
Required Steel Code Ref.	Sec. 24.4.3.2	Sec. 24.4.3.2	None	None
Bar Spacing (in)	10.16	10.16	None	None
Bar Depth (in)	22.56	21.69	None	None
Cover (in)	Top 2.00	Bottom: 3.00	Side: 3.00	

PILE FORCES

Pile Capacity: Compression (kip): 53.86 Tension(kip): -5.36 Shear(kip): 2.50					
	Ld Co	Pile #	H (in)	V (in)	
Max Unfactored Pile Axial (kip) _____	19.09	292	3	-18.00	18.00
Min Unfactored Pile Axial (kip) _____	2.95	316	2	18.00	-18.00
Max Unfactored Pile Shear (kip) _____	0.85	287	3	-18.00	18.00
Max Factored Pile Axial (kip) _____	24.81	45	3	-18.00	18.00
Min Factored Pile Axial (kip) _____	3.99	93	2	18.00	-18.00
Max Factored Pile Shear (kip) _____	1.18	40	3	-18.00	18.00



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PILE CAP DESIGN

Footing # 5 Footing Column Location: _____ (17.00 - -34.67)
 Footing Orientation (deg): _____ 90.00 Column Orientation (deg): _____ 0.00
 Length (ft): _____ 6.50
 Width (ft): _____ 6.50
 Thickness (ft): _____ 2.75
 Bottom Reinf. Parallel to Length: 8 - #7 Width: 8 - #7
 Concrete f_c (ksi): 4.00 f_{ct} (ksi): CODE Density (pcf): 150.00 E_c (ksi): 3834.00
 Reinf. f_y (ksi): 60.00
 Pile Label: 12" 13-15ft - 4pile Pile Diameter: (in) 12.00 Pile Cap Label: 4 Pile Group
 Pile Spacing: (in) 36.00 Edge Spacing: (in) 21.00
 Column Size: 16x16

LOADS

Surcharge (ksf)	Dead Load:	0.400	Live Load:	0.000
Axial (kip)	Dead Load:	7.86	Pos. Live:	0.00
	Pos. Roof:	0.55	Neg. Live:	N/A
			Neg. Roof:	N/A

CONCRETE CAPACITY

	Major	Ld Co/Code Ref.	Minor	Ld Co/Code Ref.
Required Shear (kip)	17.27	40	19.20	27
Provided Shear: (kip)	945.78	CRSI-02 Eq 13-2	913.40	CRSI-02 Eq 13-2
Required Moment: (kip-ft)	169.75	93	377.70	45
Provided Moment: (kip-ft)	540.42	N/A	521.52	N/A
Req. Col. Punching Shear: (kip)	31.84	45		
Prv. Col Punching Shear: (kip)	985.14	CRSI-02 Eq 13-1		

REINFORCEMENT

	Bottom Bars Parallel to		Top Bars Parallel to	
	Length	Width	Length	Width
Bar Quantity/Bar Size:	8-#7	8-#7	None	None
Required Steel/Provided Steel (in ²)	4.63/ 4.80	4.63/ 4.80	None	None
Required Steel Code Ref.	Sec. 24.4.3.2	Sec. 24.4.3.2	None	None
Bar Spacing (in)	10.16	10.16	None	None
Bar Depth (in)	25.56	24.69	None	None
Cover (in) Top 2.00	Bottom: 3.00	Side: 3.00		

PILE FORCES

Pile Capacity: Compression (kip): 53.86 Tension(kip): -5.36 Shear(kip): 2.50					
		Ld Co	Pile #	H (in)	V (in)
Max Unfactored Pile Axial (kip) _____	14.76	268	3	-18.00	18.00
Min Unfactored Pile Axial (kip) _____	1.68	316	2	18.00	-18.00
Max Unfactored Pile Shear (kip) _____	0.44	268	3	-18.00	18.00
Max Factored Pile Axial (kip) _____	19.47	45	3	-18.00	18.00
Min Factored Pile Axial (kip) _____	1.82	93	2	18.00	-18.00
Max Factored Pile Shear (kip) _____	0.70	45	3	-18.00	18.00



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PILE CAP DESIGN

Footing # 6 Footing Column Location: _____ (17.00 - -18.33)
 Footing Orientation (deg): _____ 90.00 Column Orientation (deg): _____ 0.00
 Length (ft): _____ 6.50
 Width (ft): _____ 6.50
 Thickness (ft): _____ 2.50
 Bottom Reinf. Parallel to Length: 8 - #7 Width: 8 - #7
 Concrete f_c (ksi): 4.00 f_{ct} (ksi): CODE Density (pcf): 150.00 E_c (ksi): 3834.00
 Reinf. f_y (ksi): 60.00
 Pile Label: 12" 13-15ft - 4pile Pile Diameter: (in) 12.00 Pile Cap Label: 4 Pile Group
 Pile Spacing: (in) 36.00 Edge Spacing: (in) 21.00
 Column Size: 16x16

LOADS

Surcharge (ksf)	Dead Load:	0.400	Live Load:	0.000
Axial (kip)	Dead Load:	28.37	Pos. Live:	0.00
	Pos. Roof:	3.72	Neg. Live:	N/A
			Neg. Roof:	N/A

CONCRETE CAPACITY

	Major	Ld Co/Code Ref.	Minor	Ld Co/Code Ref.
Required Shear (kip)	37.12	40	31.31	27
Provided Shear: (kip)	834.78	CRSI-02 Eq 13-2	802.41	CRSI-02 Eq 13-2
Required Moment: (kip-ft)	33.05	40	26.76	27
Provided Moment: (kip-ft)	475.62	N/A	456.72	N/A
Req. Col. Punching Shear: (kip)	71.61	34		
Prv. Col Punching Shear: (kip)	708.20	CRSI-02 Eq 13-1		

REINFORCEMENT

	Bottom Bars Parallel to		Top Bars Parallel to	
	Length	Width	Length	Width
Bar Quantity/Bar Size:	8-#7	8-#7	None	None
Required Steel/Provided Steel (in ²)	4.21/ 4.80	4.21/ 4.80	None	None
Required Steel Code Ref.	Sec. 24.4.3.2	Sec. 24.4.3.2	None	None
Bar Spacing (in)	10.16	10.16	None	None
Bar Depth (in)	22.56	21.69	None	None
Cover (in) Top 2.00	Bottom: 3.00	Side: 3.00		

PILE FORCES

Pile Capacity: Compression (kip): 53.86 Tension(kip): -5.36 Shear(kip): 2.50					
		Ld Co	Pile #	H (in)	V (in)
Max Unfactored Pile Axial (kip) _____	21.85	281	1	-18.00	-18.00
Min Unfactored Pile Axial (kip) _____	3.86	316	2	18.00	-18.00
Max Unfactored Pile Shear (kip) _____	0.86	263	4	18.00	18.00
Max Factored Pile Axial (kip) _____	28.56	34	1	-18.00	-18.00
Min Factored Pile Axial (kip) _____	5.10	93	2	18.00	-18.00
Max Factored Pile Shear (kip) _____	1.26	40	4	18.00	18.00



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PILE CAP DESIGN

Footing # 7 Footing Column Location: _____ (17.00 - 0.00)
 Footing Orientation (deg): _____ 90.00 Column Orientation (deg): _____ 0.00
 Length (ft): _____ 6.50
 Width (ft): _____ 6.50
 Thickness (ft): _____ 2.50
 Bottom Reinf. Parallel to Length: 8 - #7 Width: 8 - #7
 Concrete f_c (ksi): 4.00 f_{ct} (ksi): CODE Density (pcf): 150.00 E_c (ksi): 3834.00
 Reinf. f_y (ksi): 60.00
 Pile Label: 12" 13-15ft - 4pile Pile Diameter: (in) 12.00 Pile Cap Label: 4 Pile Group
 Pile Spacing: (in) 36.00 Edge Spacing: (in) 21.00
 Column Size: 16x16

LOADS

Surcharge (ksf) Dead Load: 0.400 Live Load: 0.000
 Axial (kip) Dead Load: 23.92
 Pos. Live: 0.00 Neg. Live: N/A
 Pos. Roof: 3.05 Neg. Roof: N/A

CONCRETE CAPACITY

	Major	Ld Co/Code Ref.	Minor	Ld Co/Code Ref.
Required Shear (kip)	34.33	28	27.88	39
Provided Shear: (kip)	834.78	CRSI-02 Eq 13-2	802.41	CRSI-02 Eq 13-2
Required Moment: (kip-ft)	30.03	28	23.04	39
Provided Moment: (kip-ft)	475.62	N/A	456.72	N/A
Req. Col. Punching Shear: (kip)	68.31	46		
Prv. Col Punching Shear: (kip)	708.20	CRSI-02 Eq 13-1		

REINFORCEMENT

	Bottom Bars Parallel to		Top Bars Parallel to	
	Length	Width	Length	Width
Bar Quantity/Bar Size:	8-#7	8-#7	None	None
Required Steel/Provided Steel (in ²)	4.21/ 4.80	4.21/ 4.80	None	None
Required Steel Code Ref.	Sec. 24.4.3.2	Sec. 24.4.3.2	None	None
Bar Spacing (in)	10.16	10.16	None	None
Bar Depth (in)	22.56	21.69	None	None
Cover (in) Top 2.00 Bottom: 3.00 Side: 3.00				

PILE FORCES

Pile Capacity: Compression (kip): 53.86 Tension(kip): -5.36 Shear(kip): 2.50

	Ld Co	Pile #	H (in)	V (in)
Max Unfactored Pile Axial (kip) _____	21.08	269	4	18.00
Min Unfactored Pile Axial (kip) _____	3.00	317	1	-18.00
Max Unfactored Pile Shear (kip) _____	0.92	251	4	18.00
Max Factored Pile Axial (kip) _____	27.79	46	4	18.00
Min Factored Pile Axial (kip) _____	3.88	94	1	-18.00
Max Factored Pile Shear (kip) _____	1.30	28	4	18.00



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PILE CAP DESIGN

Footing # 8 Footing Column Location: _____ (39.67 - -32.67)
 Footing Orientation (deg): _____ 90.00 Column Orientation (deg): _____ 0.00
 Length (ft): _____ 6.50
 Width (ft): _____ 6.50
 Thickness (ft): _____ 2.50
 Bottom Reinf. Parallel to Length: 8 - #7 Width: 8 - #7
 Concrete f_c (ksi): 4.00 f_{ct} (ksi): CODE Density (pcf): 150.00 E_c (ksi): 3834.00
 Reinf. f_y (ksi): 60.00
 Pile Label: 12" 13-15ft - 4pile Pile Diameter: (in) 12.00 Pile Cap Label: 4 Pile Group
 Pile Spacing: (in) 36.00 Edge Spacing: (in) 21.00
 Column Size: 16x16

LOADS

Surcharge (ksf)	Dead Load:	0.400	Live Load:	0.000
Axial (kip)	Dead Load:	12.80	Pos. Live:	0.00
	Pos. Roof:	1.29	Neg. Live:	N/A
			Neg. Roof:	N/A

CONCRETE CAPACITY

	Major	Ld Co/Code Ref.	Minor	Ld Co/Code Ref.
Required Shear (kip)	23.62	40	20.78	39
Provided Shear: (kip)	834.78	CRSI-02 Eq 13-2	802.41	CRSI-02 Eq 13-2
Required Moment: (kip-ft)	93.77	88	15.35	39
Provided Moment: (kip-ft)	475.62	N/A	456.72	N/A
Req. Col. Punching Shear: (kip)	45.42	45		
Prv. Col Punching Shear: (kip)	708.20	CRSI-02 Eq 13-1		

REINFORCEMENT

	Bottom Bars Parallel to		Top Bars Parallel to	
	Length	Width	Length	Width
Bar Quantity/Bar Size:	8-#7	8-#7	None	None
Required Steel/Provided Steel (in ²)	4.21/ 4.80	4.21/ 4.80	None	None
Required Steel Code Ref.	Sec. 24.4.3.2	Sec. 24.4.3.2	None	None
Bar Spacing (in)	10.16	10.16	None	None
Bar Depth (in)	22.56	21.69	None	None
Cover (in)	Top 2.00	Bottom: 3.00	Side: 3.00	

PILE FORCES

Pile Capacity: Compression (kip): 53.86 Tension(kip): -5.36 Shear(kip): 2.50					
	Ld Co	Pile #	H (in)	V (in)	
Max Unfactored Pile Axial (kip) _____	16.53	268	3	-18.00	18.00
Min Unfactored Pile Axial (kip) _____	2.72	316	2	18.00	-18.00
Max Unfactored Pile Shear (kip) _____	0.51	271	3	-18.00	18.00
Max Factored Pile Axial (kip) _____	21.84	45	3	-18.00	18.00
Min Factored Pile Axial (kip) _____	3.53	93	2	18.00	-18.00
Max Factored Pile Shear (kip) _____	0.78	48	3	-18.00	18.00



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PILE CAP DESIGN

Footing # 9 Footing Column Location: _____ (39.67 - -18.33)
 Footing Orientation (deg): _____ 90.00 Column Orientation (deg): _____ 0.00
 Length (ft): _____ 6.50
 Width (ft): _____ 6.50
 Thickness (ft): _____ 2.50
 Bottom Reinf. Parallel to Length: 8 - #7 Width: 8 - #7
 Concrete f_c (ksi): 4.00 fct (ksi): CODE Density (pcf): 150.00 E_c (ksi): 3834.00
 Reinf. f_y (ksi): 60.00
 Pile Label: 12" 13-15ft - 4pile Pile Diameter: (in) 12.00 Pile Cap Label: 4 Pile Group
 Pile Spacing: (in) 36.00 Edge Spacing: (in) 21.00
 Column Size: 16x16

LOADS

Surcharge (ksf)	Dead Load:	0.400	Live Load:	0.000
Axial (kip)	Dead Load:	33.25		
	Pos. Live:	0.00	Neg. Live:	N/A
	Pos. Roof:	4.59	Neg. Roof:	N/A

CONCRETE CAPACITY

	Major	Ld Co/Code Ref.	Minor	Ld Co/Code Ref.
Required Shear (kip)	40.54	40	35.09	39
Provided Shear: (kip)	834.78	CRSI-02 Eq 13-2	802.41	CRSI-02 Eq 13-2
Required Moment: (kip-ft)	36.76	40	30.85	39
Provided Moment: (kip-ft)	475.62	N/A	456.72	N/A
Req. Col. Punching Shear: (kip)	79.26	45		
Prv. Col Punching Shear: (kip)	708.20	CRSI-02 Eq 13-1		

REINFORCEMENT

	Bottom Bars Parallel to		Top Bars Parallel to	
	Length	Width	Length	Width
Bar Quantity/Bar Size:	8-#7	8-#7	None	None
Required Steel/Provided Steel (in ²)	4.21/ 4.80	4.21/ 4.80	None	None
Required Steel Code Ref.	Sec. 24.4.3.2	Sec. 24.4.3.2	None	None
Bar Spacing (in)	10.16	10.16	None	None
Bar Depth (in)	22.56	21.69	None	None
Cover (in) Top 2.00 Bottom: 3.00 Side: 3.00				

PILE FORCES

Pile Capacity: Compression (kip): 53.86 Tension(kip): -5.36 Shear(kip): 2.50					
		Ld Co	Pile #	H (in)	V (in)
Max Unfactored Pile Axial (kip) _____	23.23	292	3	-18.00	18.00
Min Unfactored Pile Axial (kip) _____	4.42	316	2	18.00	-18.00
Max Unfactored Pile Shear (kip) _____	0.78	263	3	-18.00	18.00
Max Factored Pile Axial (kip) _____	30.51	45	3	-18.00	18.00
Min Factored Pile Axial (kip) _____	5.96	93	2	18.00	-18.00
Max Factored Pile Shear (kip) _____	1.18	40	3	-18.00	18.00



Pile Cap Footing Design

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PILE CAP DESIGN

Footing # 10 Footing Column Location: _____ (39.67 - 0.00)
 Footing Orientation (deg): _____ 90.00 Column Orientation (deg): _____ 0.00
 Length (ft): _____ 6.50
 Width (ft): _____ 6.50
 Thickness (ft): _____ 2.50
 Bottom Reinf. Parallel to Length: 8 - #7 Width: 8 - #7
 Concrete f_c (ksi): 4.00 f_{ct} (ksi): CODE Density (pcf): 150.00 E_c (ksi): 3834.00
 Reinf. f_y (ksi): 60.00
 Pile Label: 12" 13-15ft - 4pile Pile Diameter: (in) 12.00 Pile Cap Label: 4 Pile Group
 Pile Spacing: (in) 36.00 Edge Spacing: (in) 21.00
 Column Size: 16x16

LOADS

Surcharge (ksf) Dead Load: 0.400 Live Load: 0.000
 Axial (kip) Dead Load: 24.99
 Pos. Live: 0.00 Neg. Live: N/A
 Pos. Roof: 3.20 Neg. Roof: N/A

CONCRETE CAPACITY

	Major	Ld Co/Code Ref.	Minor	Ld Co/Code Ref.
Required Shear (kip)	36.65	28	28.09	39
Provided Shear: (kip)	834.78	CRSI-02 Eq 13-2	802.41	CRSI-02 Eq 13-2
Required Moment: (kip-ft)	32.55	28	23.27	39
Provided Moment: (kip-ft)	475.62	N/A	456.72	N/A
Req. Col. Punching Shear: (kip)	70.62	46		
Prv. Col Punching Shear: (kip)	708.20	CRSI-02 Eq 13-1		

REINFORCEMENT

	Bottom Bars Parallel to		Top Bars Parallel to	
	Length	Width	Length	Width
Bar Quantity/Bar Size:	8-#7	8-#7	None	None
Required Steel/Provided Steel (in ²)	4.21/ 4.80	4.21/ 4.80	None	None
Required Steel Code Ref.	Sec. 24.4.3.2	Sec. 24.4.3.2	None	None
Bar Spacing (in)	10.16	10.16	None	None
Bar Depth (in)	22.56	21.69	None	None
Cover (in) Top 2.00 Bottom: 3.00 Side: 3.00				

PILE FORCES

Pile Capacity: Compression (kip): 53.86 Tension(kip): -5.36 Shear(kip): 2.50

	Ld Co	Pile #	H (in)	V (in)
Max Unfactored Pile Axial (kip) _____	21.50	269	4	18.00
Min Unfactored Pile Axial (kip) _____	2.96	317	1	-18.00
Max Unfactored Pile Shear (kip) _____	0.95	251	4	18.00
Max Factored Pile Axial (kip) _____	28.39	46	4	18.00
Min Factored Pile Axial (kip) _____	3.78	94	1	-18.00
Max Factored Pile Shear (kip) _____	1.35	28	4	18.00



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PILE CAP DESIGN

Footing # 11 Footing Column Location: _____ (61.67 - -32.67)
 Footing Orientation (deg): _____ 90.00 Column Orientation (deg): _____ 0.00
 Length (ft): _____ 6.50
 Width (ft): _____ 6.50
 Thickness (ft): _____ 2.75
 Bottom Reinf. Parallel to Length: 8 - #7 Width: 8 - #7
 Concrete f_c (ksi): 4.00 f_{ct} (ksi): CODE Density (pcf): 150.00 E_c (ksi): 3834.00
 Reinf. f_y (ksi): 60.00
 Pile Label: 12" 13-15ft - 4pile Pile Diameter: (in) 12.00 Pile Cap Label: 4 Pile Group
 Pile Spacing: (in) 36.00 Edge Spacing: (in) 21.00
 Column Size: 16x16

LOADS

Surcharge (ksf) Dead Load: 0.400 Live Load: 0.000
 Axial (kip) Dead Load: 14.07
 Pos. Live: 0.00 Neg. Live: N/A
 Pos. Roof: 1.35 Neg. Roof: N/A

CONCRETE CAPACITY

	Major	Ld Co/Code Ref.	Minor	Ld Co/Code Ref.
Required Shear (kip)	25.72	43	22.06	27
Provided Shear: (kip)	945.78	CRSI-02 Eq 13-2	913.40	CRSI-02 Eq 13-2
Required Moment: (kip-ft)	140.09	88	16.40	27
Provided Moment: (kip-ft)	540.42	N/A	521.52	N/A
Req. Col. Punching Shear: (kip)	46.67	34		
Prv. Col Punching Shear: (kip)	985.14	CRSI-02 Eq 13-1		

REINFORCEMENT

	Bottom Bars Parallel to		Top Bars Parallel to	
	Length	Width	Length	Width
Bar Quantity/Bar Size:	8-#7	8-#7	None	None
Required Steel/Provided Steel (in ²)	4.63/ 4.80	4.63/ 4.80	None	None
Required Steel Code Ref.	Sec. 24.4.3.2	Sec. 24.4.3.2	None	None
Bar Spacing (in)	10.16	10.16	None	None
Bar Depth (in)	25.56	24.69	None	None
Cover (in) Top 2.00 Bottom: 3.00 Side: 3.00				

PILE FORCES

Pile Capacity: Compression (kip): 53.86 Tension(kip): -5.36 Shear(kip): 2.50

	Ld Co	Pile #	H (in)	V (in)
Max Unfactored Pile Axial (kip) _____	17.69	257	1	-18.00
Min Unfactored Pile Axial (kip) _____	2.82	305	4	18.00
Max Unfactored Pile Shear (kip) _____	0.56	266	4	18.00
Max Factored Pile Axial (kip) _____	23.33	34	1	-18.00
Min Factored Pile Axial (kip) _____	3.66	82	4	18.00
Max Factored Pile Shear (kip) _____	0.85	43	4	18.00



Pile Cap Footing Design

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PILE CAP DESIGN

Footing # 12 Footing Column Location: _____ (61.67 - -18.33)
 Footing Orientation (deg): _____ 90.00 Column Orientation (deg): _____ 0.00
 Length (ft): _____ 6.50
 Width (ft): _____ 6.50
 Thickness (ft): _____ 2.50
 Bottom Reinf. Parallel to Length: 8 - #7 Width: 8 - #7
 Concrete f_c (ksi): 4.00 f_{ct} (ksi): CODE Density (pcf): 150.00 E_c (ksi): 3834.00
 Reinf. f_y (ksi): 60.00
 Pile Label: 12" 13-15ft - 4pile Pile Diameter: (in) 12.00 Pile Cap Label: 4 Pile Group
 Pile Spacing: (in) 36.00 Edge Spacing: (in) 21.00
 Column Size: 16x16

LOADS

Surcharge (ksf) Dead Load: 0.400 Live Load: 0.000
 Axial (kip) Dead Load: 32.45
 Pos. Live: 0.00 Neg. Live: N/A
 Pos. Roof: 4.27 Neg. Roof: N/A

CONCRETE CAPACITY

	Major	Ld Co/Code Ref.	Minor	Ld Co/Code Ref.
Required Shear (kip)	39.22	43	34.48	27
Provided Shear: (kip)	834.78	CRSI-02 Eq 13-2	802.41	CRSI-02 Eq 13-2
Required Moment: (kip-ft)	35.33	43	30.20	27
Provided Moment: (kip-ft)	475.62	N/A	456.72	N/A
Req. Col. Punching Shear: (kip)	76.69	34		
Prv. Col Punching Shear: (kip)	708.20	CRSI-02 Eq 13-1		

REINFORCEMENT

	Bottom Bars Parallel to		Top Bars Parallel to	
	Length	Width	Length	Width
Bar Quantity/Bar Size:	8-#7	8-#7	None	None
Required Steel/Provided Steel (in ²)	4.21/ 4.80	4.21/ 4.80	None	None
Required Steel Code Ref.	Sec. 24.4.3.2	Sec. 24.4.3.2	None	None
Bar Spacing (in)	10.16	10.16	None	None
Bar Depth (in)	22.56	21.69	None	None
Cover (in) Top 2.00 Bottom: 3.00 Side: 3.00				

PILE FORCES

Pile Capacity: Compression (kip): 53.86 Tension(kip): -5.36 Shear(kip): 2.50

	Ld Co	Pile #	H (in)	V (in)
Max Unfactored Pile Axial (kip) _____	22.63	257	1	-18.00
Min Unfactored Pile Axial (kip) _____	4.45	305	4	18.00
Max Unfactored Pile Shear (kip) _____	0.75	266	4	18.00
Max Factored Pile Axial (kip) _____	29.83	34	1	-18.00
Min Factored Pile Axial (kip) _____	5.99	82	4	18.00
Max Factored Pile Shear (kip) _____	1.14	43	4	18.00



Pile Cap Footing Design

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PILE CAP DESIGN

Footing # 13 Footing Column Location: _____ (61.67 - 0.00)
 Footing Orientation (deg): _____ 90.00 Column Orientation (deg): _____ 0.00
 Length (ft): _____ 6.50
 Width (ft): _____ 6.50
 Thickness (ft): _____ 2.50
 Bottom Reinf. Parallel to Length: 8 - #7 Width: 8 - #7
 Concrete f_c (ksi): 4.00 f_{ct} (ksi): CODE Density (pcf): 150.00 E_c (ksi): 3834.00
 Reinf. f_y (ksi): 60.00
 Pile Label: 12" 13-15ft - 4pile Pile Diameter: (in) 12.00 Pile Cap Label: 4 Pile Group
 Pile Spacing: (in) 36.00 Edge Spacing: (in) 21.00
 Column Size: 16x16

LOADS

Surcharge (ksf)	Dead Load:	0.400	Live Load:	0.000
Axial (kip)	Dead Load:	17.22		
	Pos. Live:	0.00	Neg. Live:	N/A
	Pos. Roof:	1.87	Neg. Roof:	N/A

CONCRETE CAPACITY

	Major	Ld Co/Code Ref.	Minor	Ld Co/Code Ref.
Required Shear (kip)	28.84	31	21.64	27
Provided Shear: (kip)	834.78	CRSI-02 Eq 13-2	802.41	CRSI-02 Eq 13-2
Required Moment: (kip-ft)	130.30	76	16.28	27
Provided Moment: (kip-ft)	475.62	N/A	456.72	N/A
Req. Col. Punching Shear: (kip)	51.83	49		
Prv. Col Punching Shear: (kip)	708.20	CRSI-02 Eq 13-1		

REINFORCEMENT

	Bottom Bars Parallel to		Top Bars Parallel to	
	Length	Width	Length	Width
Bar Quantity/Bar Size:	8-#7	8-#7	None	None
Required Steel/Provided Steel (in ²)	4.21/ 4.80	4.21/ 4.80	None	None
Required Steel Code Ref.	Sec. 24.4.3.2	Sec. 24.4.3.2	None	None
Bar Spacing (in)	10.16	10.16	None	None
Bar Depth (in)	22.56	21.69	None	None
Cover (in) Top 2.00 Bottom: 3.00 Side: 3.00				

PILE FORCES

Pile Capacity: Compression (kip): 53.86 Tension(kip): -5.36 Shear(kip): 2.50					
	Ld Co	Pile #	H (in)	V (in)	
Max Unfactored Pile Axial (kip) _____	17.87	272	4	18.00	18.00
Min Unfactored Pile Axial (kip) _____	2.96	320	1	-18.00	-18.00
Max Unfactored Pile Shear (kip) _____	0.74	254	4	18.00	18.00
Max Factored Pile Axial (kip) _____	23.49	49	4	18.00	18.00
Min Factored Pile Axial (kip) _____	3.86	97	1	-18.00	-18.00
Max Factored Pile Shear (kip) _____	1.07	31	4	18.00	18.00

BOUYANCY CALCS ON DRIVEN PILES

SEE FOLLOWING PAGES FOR LOADING ON SLAB/PILES.

FROM RAM CONCEPT BOUYANCY UPLIFT ON
PILES = 33.9 kips

FROM GEOTECH (12" SQUARE PILE)

ALLOWABLE TENSION CAPACITY OF 6 TONS

6 TONS = 12,000 lbs

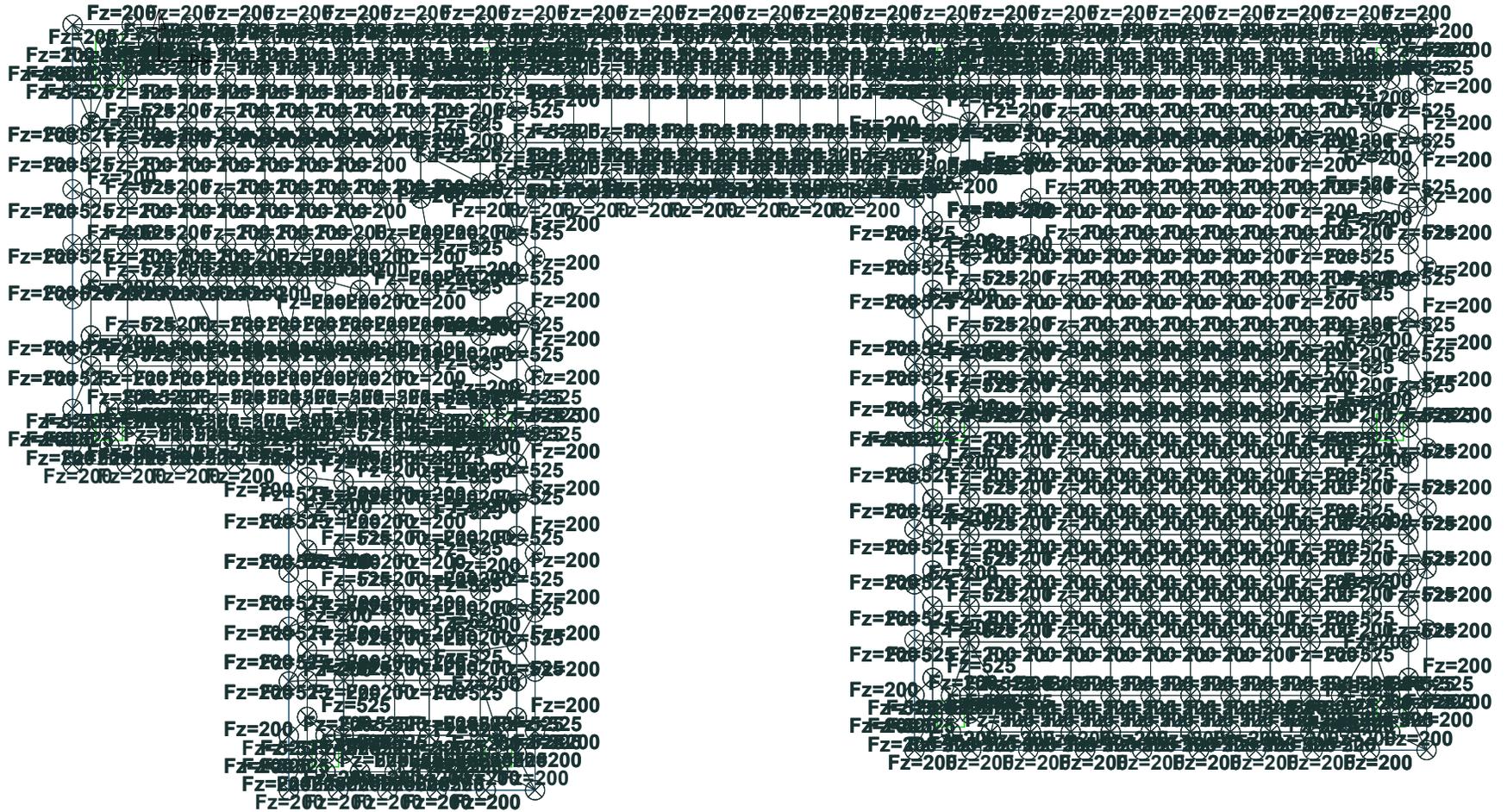
4 PILES PER PILE CAP $(12,000 \times 4) = 48,000$ lbs

48 kips > 33.9 kips OK

PILES W/ HELP OF SLAB WEIGHT
WILL BE ABLE TO COUNTER THE
BOUYANCY FORCE

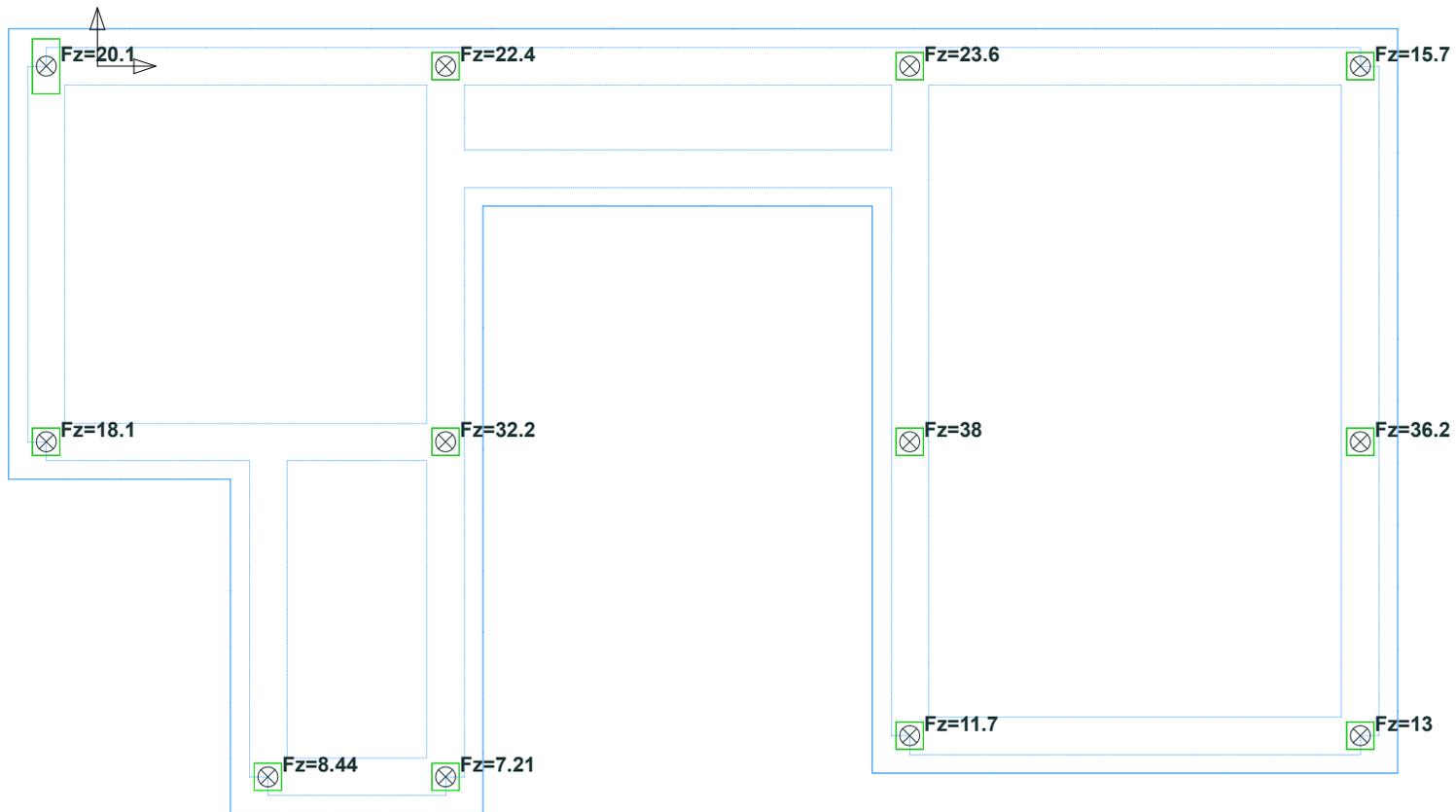
Self-Dead Loading: All Loads Plan

Self-Dead Loading: User Lines; User Notes; User Dimensions; Point Loads; Point Load Icons; Point Load Values; Line Loads; Line Load Icons; Line Load Values; All Element: Wall Elements Below; Wall Elements Above; Wall Element Outline Only; Column Elements Below; Column Elements Above; Slab Elements; Slab Element C
Scale = 1:99



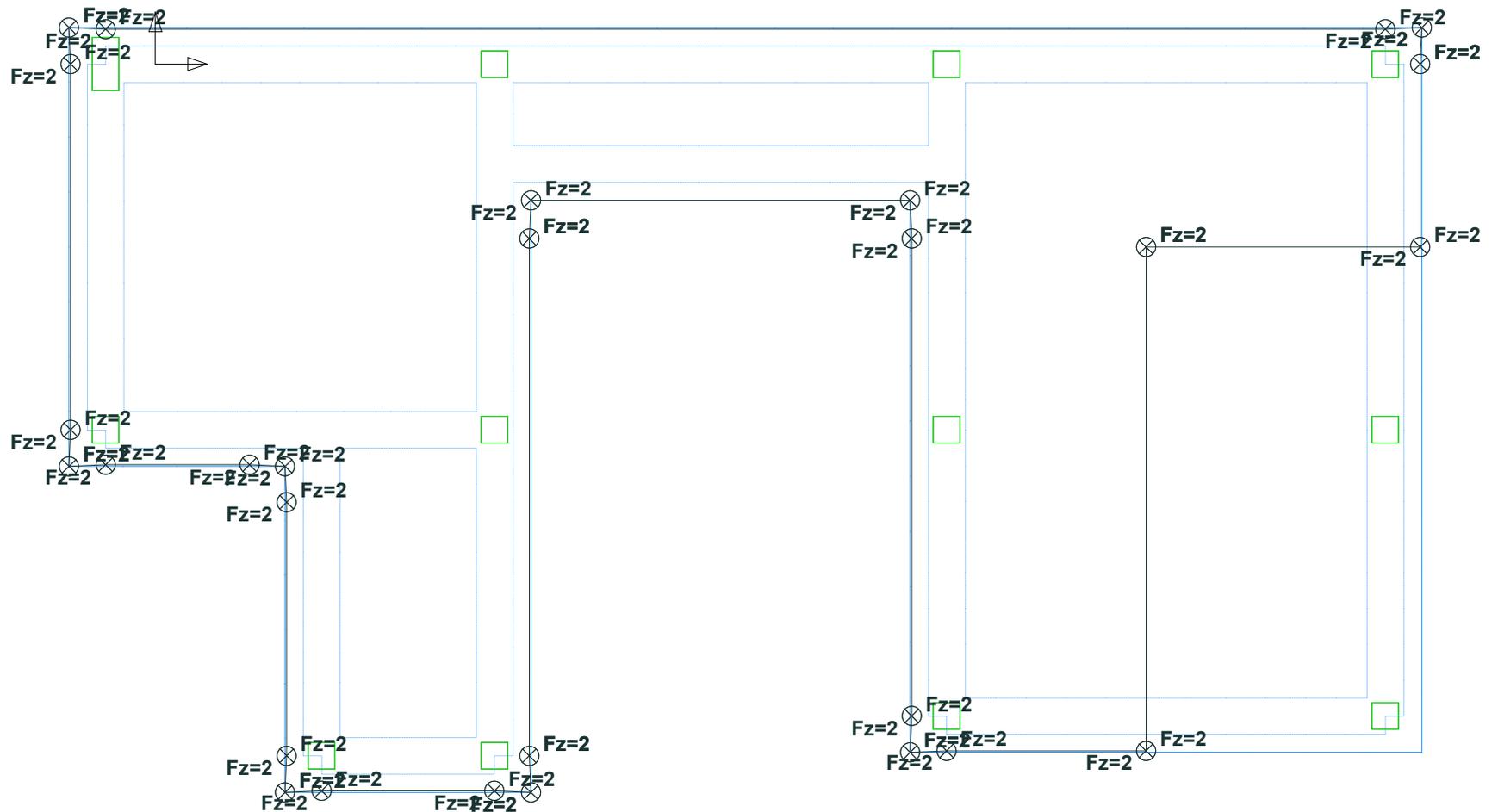
Dead Load (transfer): All Loads Plan

Dead Load (transfer): User Lines; User Notes; User Dimensions; Point Loads; Point Load Icons; Point Load Values; Line Loads; Line Load Icons; Line Load Values; Area Loads; Area Load Icons; Area Load Values; Wall Elements Below; Wall Elements Above; Wall Element Outline Only; Column Elements Below; Column Elements Above; Slab Elements; Slab Element Outline Only; Scale = 1:109



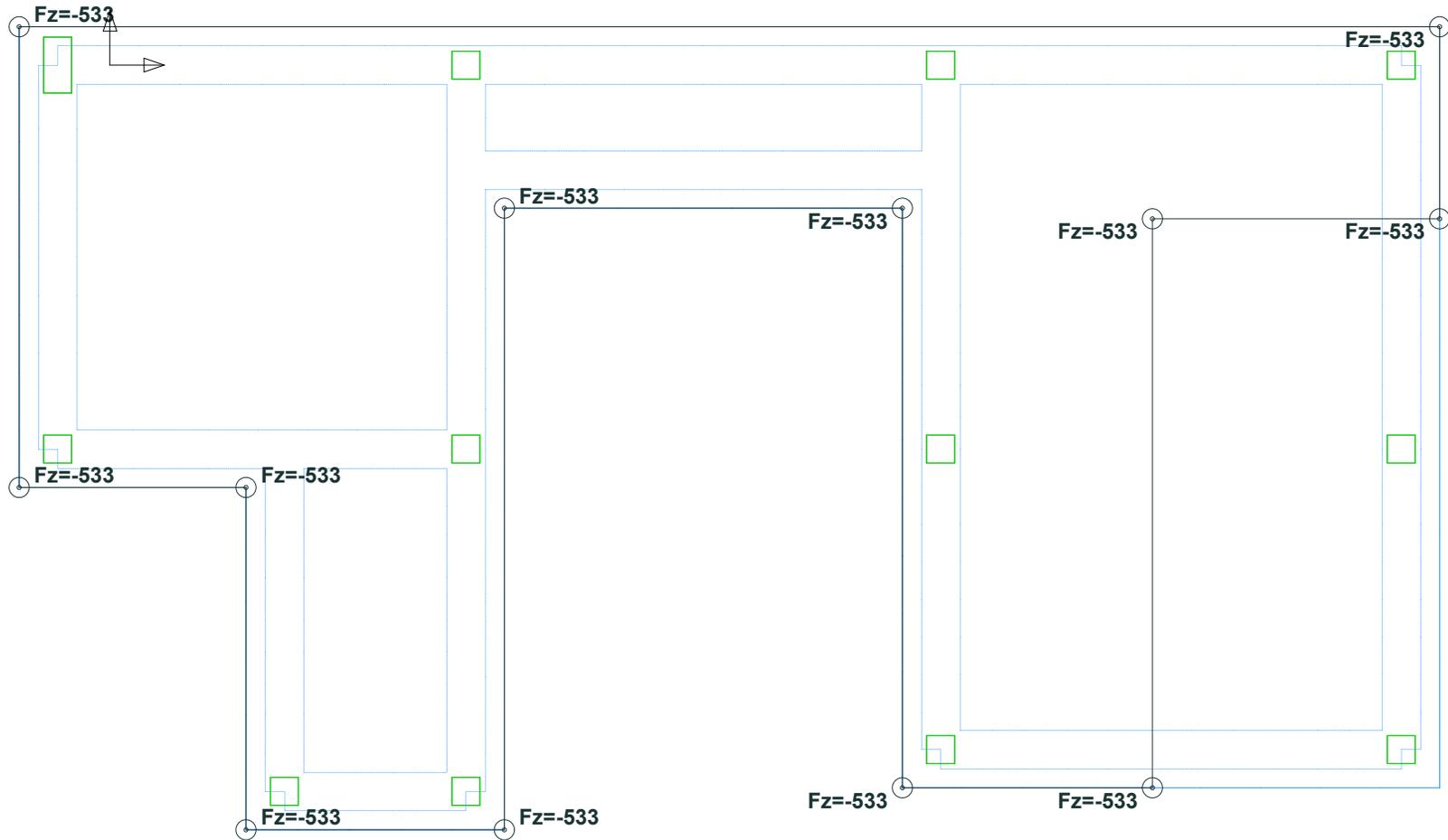
Dead Load (Wall Loading): All Loads Plan

Dead Load (Wall Loading): User Lines; User Notes; User Dimensions; Point Loads; Point Load Icons; Point Load Values; Line Loads; Line Load Icons; Line Load Va
 Element: Wall Elements Above; Wall Elements Below; Wall Element Outline Only; Column Elements Below; Column Elements Above; Slab Elements; Slab Element C
 Scale = 1:99



Hydrostatic Pressure: All Loads Plan

Hydrostatic Pressure: User Lines; User Notes; User Dimensions; Point Loads; Point Load Icons; Point Load Values; Line Loads; Line Load Icons; Line Load Values; Element: Wall Elements Below; Wall Elements Above; Wall Element Outline Only; Column Elements Below; Column Elements Above; Slab Elements; Slab Element C
 Scale = 1:99



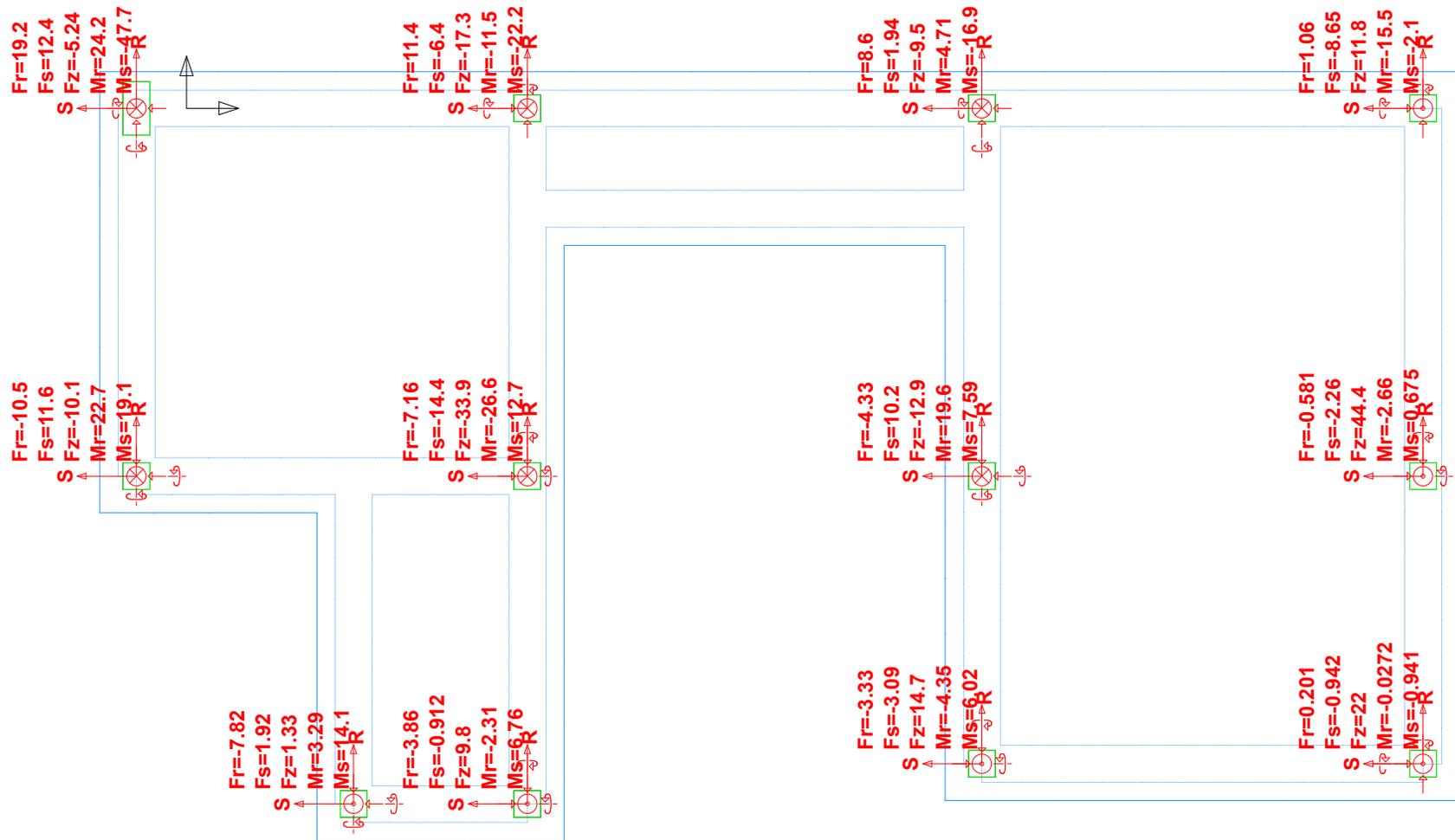
.6DL+1.0H: Max Reactions Plan

.6DL+1.0H: User Lines; User Notes; User Dimensions;

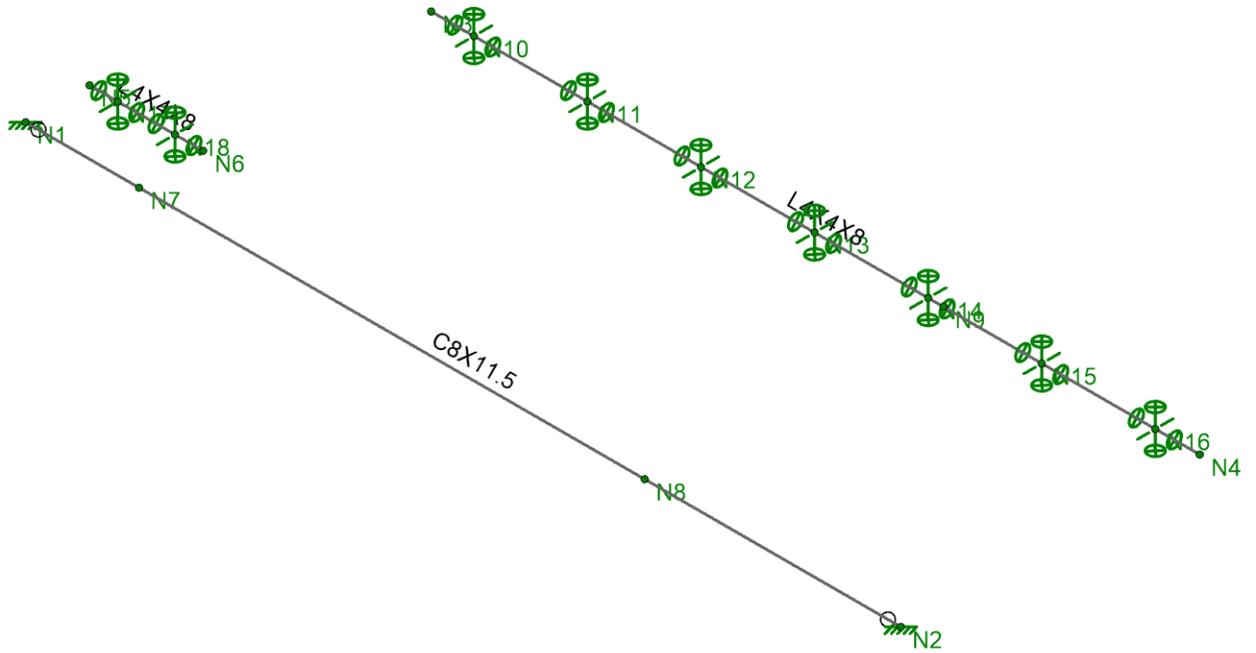
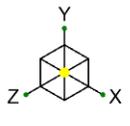
Element: Wall Elements Below; Wall Elements Above; Wall Element Outline Only; Column Elements Below; Column Elements Above; Slab Elements; Slab Element C

Scale = 1:99

.6DL+1.0H - Reaction Plot: (Column Below)(Fr,Fs,Fz,Mr,Ms,Mz)(Max Fz Context)



Building 4 Miscellaneous Calcs



Envelope Only Solution

Ramaker	Building 4 Equipment Platform	SK-2
KLM		Jan 24, 2023
30479		30479 Building 4 Equipment Platfo...

Hot Rolled Steel Properties

	Label	E [ksi]	G [ksi]	Nu	Therm. Coeff. [1e ⁵ F ⁻¹]	Density [k/ft ³]	Yield [ksi]	Ry	Fu [ksi]	Rt
1	A992	29000	11154	0.3	0.65	0.49	50	1.1	65	1.1
2	A36 Gr.36	29000	11154	0.3	0.65	0.49	36	1.5	58	1.2
3	A572 Gr.50	29000	11154	0.3	0.65	0.49	50	1.1	65	1.1
4	A500 Gr.B RND	29000	11154	0.3	0.65	0.527	42	1.4	58	1.3
5	A500 Gr.B RECT	29000	11154	0.3	0.65	0.527	46	1.4	58	1.3
6	A500 Gr.C RND	29000	11154	0.3	0.65	0.527	46	1.4	62	1.3
7	A500 Gr.C RECT	29000	11154	0.3	0.65	0.527	50	1.4	62	1.3
8	A53 Gr.B	29000	11154	0.3	0.65	0.49	35	1.6	60	1.2
9	A1085	29000	11154	0.3	0.65	0.49	50	1.4	65	1.3
10	A913 Gr.65	29000	11154	0.3	0.65	0.49	65	1.1	80	1.1

Hot Rolled Steel Section Sets

	Label	Shape	Type	Design List	Material	Design Rule	Area [in ²]	Iyy [in ⁴]	Izz [in ⁴]	J [in ⁴]
1	L4x4x1/2	L4X4X8	Beam	Single Angle	A36 Gr.36	Typical	3.75	5.52	5.52	0.322
2	C6x8.2	C8X11.5	Beam	Channel	A36 Gr.36	Typical	3.37	1.31	32.5	0.13

Member Primary Data

	Label	I Node	J Node	Rotate(deg)	Section/Shape	Type	Design List	Material	Design Rule
1	M1	N3	N4	90	L4x4x1/2	Beam	Single Angle	A36 Gr.36	Typical
2	M2	N5	N6	90	L4x4x1/2	Beam	Single Angle	A36 Gr.36	Typical
3	M3	N1	N2	180	C6x8.2	Beam	Channel	A36 Gr.36	Typical

Member Advanced Data

	Label	I Release	J Release	Physical	Deflection Ratio Options	Seismic DR
1	M1			Yes	Default	None
2	M2			Yes	Default	None
3	M3	BenPIN	BenPIN	Yes	Default	None

Hot Rolled Steel Design Parameters

	Label	Shape	Length [ft]	Lcomp top [ft]	Channel Conn.	a [ft]	Function
1	M1	L4x4x1/2	9	Lbyy	N/A	N/A	Lateral
2	M2	L4x4x1/2	1.33	Lbyy	N/A	N/A	Lateral
3	M3	C6x8.2	10.25	Lbyy	N/A	N/A	Lateral

Basic Load Cases

	BLC Description	Category	Y Gravity	Distributed	Area(Member)
1	DL	DL	-1		3
2	LL	LL			2
3	BLC 1 Transient Area Loads	None		14	
4	BLC 2 Transient Area Loads	None		12	

Load Combinations

	Description	Solve	P-Delta	BLC	Factor	BLC	Factor	BLC	Factor
1	Deflection 1	Yes	Y	DL	1				
2	Deflection 2	Yes	Y	LL	1				
3	Deflection 3	Yes	Y	DL	1	LL	1		

Load Combinations (Continued)

	Description	Solve	P-Delta	BLC	Factor	BLC	Factor	BLC	Factor
4	IBC 16-1	Yes	Y	DL	1.4				
5	IBC 16-2 (a)	Yes	Y	DL	1.2	LL	1.6	LLS	1.6

Envelope Node Reactions

	Node Label		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [lb-ft]	LC	MY [lb-ft]	LC	MZ [lb-ft]	LC
1	N17	max	0	5	37.115	5	0	5	0	5	-0.166	1	0	5
2		min	0	1	10.979	1	0	1	0	1	-0.562	5	0	1
3	N18	max	0	5	37.115	5	0	3	0	5	0.562	5	0	5
4		min	0	1	10.979	1	0	5	0	1	0.166	1	0	1
5	N1	max	0	5	863.674	5	0	5	0	5	0	5	0	5
6		min	0	1	173.186	1	0	1	0	1	0	1	0	1
7	N2	max	0	5	1398.899	5	0	5	0	5	0	5	0	5
8		min	0	1	420.792	1	0	1	0	1	0	1	0	1
9	N12	max	0	5	239.151	5	0.758	4	0	5	0.182	5	0	5
10		min	0	1	38.402	1	-0.612	2	0	1	0.056	2	0	1
11	N10	max	0	5	303.555	5	1.709	5	0	5	0.076	4	0	5
12		min	0	1	41.123	1	0.062	1	0	1	-0.892	5	0	1
13	N11	max	0	5	254.088	5	-0.059	1	0	5	-0.256	1	0	5
14		min	0	1	38.662	1	-0.895	5	0	1	-2.509	5	0	1
15	N14	max	0	5	299.51	5	-0.156	1	0	5	10.41	4	0	5
16		min	0	1	88.219	1	-0.884	5	0	1	-0.038	2	0	1
17	N13	max	0	5	231.61	5	0.188	2	0	5	-0.003	2	0	5
18		min	0	1	29.933	1	-5.026	4	0	1	-0.492	4	0	1
19	N15	max	0	5	427.6	5	5.542	4	0	5	1.973	5	0	5
20		min	0	1	127.639	2	-1.352	2	0	1	-0.01	4	0	1
21	N16	max	0	5	457.518	5	1.82	5	0	5	1.778	5	0	5
22		min	0	1	162.568	2	-1.06	4	0	1	-0.645	4	0	1
23	Totals:	max	0	5	4549.837	5	0	3						
24		min	0	1	1202.931	1	0	5						

Envelope AISC 15TH (360-16): LRFD Member Steel Code Checks

	Member	Shape	Code	Check	Loc[ft]	LC	Shear	Check	Loc[ft]	Dir	LC	phi*Pnc [lb]	phi*Pnt [lb]	phi*Mn y-y [lb-ft]	phi*Mn z-z [lb-ft]	Cb	Eqn
1	M1	L4X4X8	0.009	8.531	5	0.006	8.438	z	5			43736.804	121500	5480.406	12057.021	1.5	H2-1
2	M2	L4X4X8	0.001	1.011	5	0	0.998	z	5			118824.257	121500	5480.406	12574.63	1.385	H2-1
3	M3	C8X11.5	0.162	5.445	5	0.041	10.25	y	5			19561.444	109188	3352.607	17772.653	1.138	H1-1b

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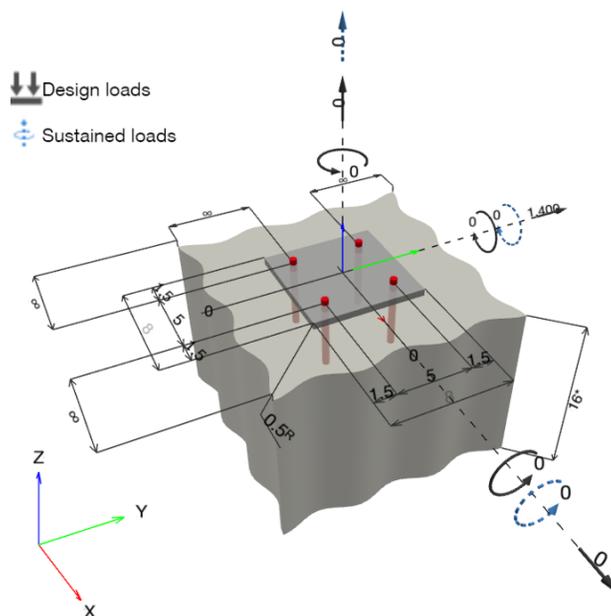
Specifier's comments:

1 Input data

Anchor type and diameter:	HIT-HY 200 V3 + HAS-V-36 (ASTM F1554 Gr.36) 1/2	
Item number:	2198022 HAS-V-36 1/2"x6-1/2" (element) / 2334276 HIT-HY 200-R V3 (adhesive)	
Effective embedment depth:	$h_{ef,act} = 4.500$ in. ($h_{ef,limit} = -$ in.)	
Material:	ASTM F1554 Grade 36	
Evaluation Service Report:	ESR-4868	
Issued Valid:	11/1/2022 11/1/2024	
Proof:	Design Method ACI 318-14 / Chem	
Stand-off installation:	$e_b = 0.000$ in. (no stand-off); $t = 0.500$ in.	
Anchor plate ^R :	$l_x \times l_y \times t = 8.000$ in. x 8.000 in. x 0.500 in.; (Recommended plate thickness: not calculated)	
Profile:	no profile	
Base material:	cracked concrete, 5000, $f'_c = 5,000$ psi; $h = 16.000$ in., Temp. short/long: 32/32 °F	
Installation:	hammer drilled hole, Installation condition: Dry	
Reinforcement:	tension: condition B, shear: condition B; no supplemental splitting reinforcement present edge reinforcement: none or < No. 4 bar	

^R - The anchor calculation is based on a rigid anchor plate assumption.

Geometry [in.] & Loading [lb, in.lb]



Input data and results must be checked for conformity with the existing conditions and for plausibility!
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1.1 Design results

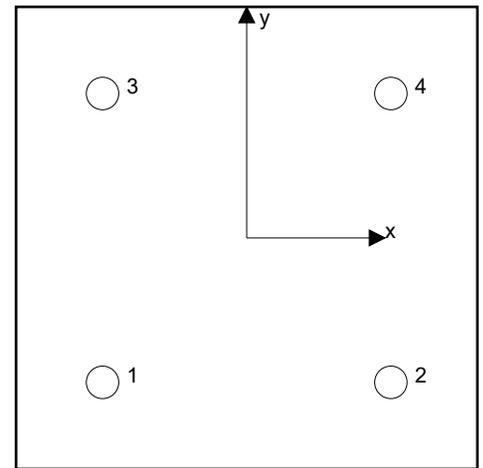
Case	Description	Forces [lb] / Moments [in.lb]	Seismic	Max. Util. Anchor [%]
1	Combination 1	$N = 0; V_x = 0; V_y = 1,400;$ $M_x = 0; M_y = 0; M_z = 0;$ $N_{sus} = 0; M_{x,sus} = 0; M_{y,sus} = 0;$	no	11

2 Load case/Resulting anchor forces

Anchor reactions [lb]

Tension force: (+Tension, -Compression)

Anchor	Tension force	Shear force	Shear force x	Shear force y
1	0	350	0	350
2	0	350	0	350
3	0	350	0	350
4	0	350	0	350



max. concrete compressive strain: - [%]
 max. concrete compressive stress: - [psi]
 resulting tension force in (x/y)=(0.000/0.000): 0 [lb]
 resulting compression force in (x/y)=(0.000/0.000): 0 [lb]

Anchor forces are calculated based on the assumption of a rigid anchor plate.

3 Tension load

	Load N_{ua} [lb]	Capacity ϕN_n [lb]	Utilization $\beta_N = N_{ua}/\phi N_n$	Status
Steel Strength*	N/A	N/A	N/A	N/A
Bond Strength**	N/A	N/A	N/A	N/A
Sustained Tension Load Bond Strength*	N/A	N/A	N/A	N/A
Concrete Breakout Failure**	N/A	N/A	N/A	N/A

* highest loaded anchor **anchor group (anchors in tension)



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4 Shear load

	Load V_{ua} [lb]	Capacity ϕV_n [lb]	Utilization $\beta_v = V_{ua} / \phi V_n$	Status
Steel Strength*	350	3,211	11	OK
Steel failure (with lever arm)*	N/A	N/A	N/A	N/A
Pryout Strength (Bond Strength controls)**	1,400	21,664	7	OK
Concrete edge failure in direction **	N/A	N/A	N/A	N/A

* highest loaded anchor **anchor group (relevant anchors)

4.1 Steel Strength

V_{sa} = ESR value refer to ICC-ES ESR-4868
 $\phi V_{steel} \geq V_{ua}$ ACI 318-14 Table 17.3.1.1

Variables

$A_{se,V}$ [in. ²]	f_{uta} [psi]
0.14	58,000

Calculations

V_{sa} [lb]
4,940

Results

V_{sa} [lb]	ϕ_{steel}	ϕV_{sa} [lb]	V_{ua} [lb]
4,940	0.650	3,211	350



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4.2 Pryout Strength (Bond Strength controls)

$$V_{cpq} = k_{cp} \left[\left(\frac{A_{Na}}{A_{Na0}} \right) \Psi_{ec1,Na} \Psi_{ec2,Na} \Psi_{ed,Na} \Psi_{cp,Na} N_{ba} \right] \quad \text{ACI 318-14 Eq. (17.5.3.1b)}$$

$$\phi V_{cpq} \geq V_{ua} \quad \text{ACI 318-14 Table 17.3.1.1}$$

A_{Na} see ACI 318-14, Section 17.4.5.1, Fig. R 17.4.5.1(b)

$$A_{Na0} = (2 c_{Na})^2 \quad \text{ACI 318-14 Eq. (17.4.5.1c)}$$

$$c_{Na} = 10 d_a \sqrt{\frac{\tau_{uncr}}{1100}} \quad \text{ACI 318-14 Eq. (17.4.5.1d)}$$

$$\Psi_{ec,Na} = \left(\frac{1}{1 + \frac{e_N}{c_{Na}}} \right) \leq 1.0 \quad \text{ACI 318-14 Eq. (17.4.5.3)}$$

$$\Psi_{ed,Na} = 0.7 + 0.3 \left(\frac{c_{a,min}}{c_{Na}} \right) \leq 1.0 \quad \text{ACI 318-14 Eq. (17.4.5.4b)}$$

$$\Psi_{cp,Na} = \text{MAX} \left(\frac{c_{a,min}}{c_{ac}}, \frac{c_{Na}}{c_{ac}} \right) \leq 1.0 \quad \text{ACI 318-14 Eq. (17.4.5.5b)}$$

$$N_{ba} = \lambda_a \cdot \tau_{k,c} \cdot \pi \cdot d_a \cdot h_{ef} \quad \text{ACI 318-14 Eq. (17.4.5.2)}$$

Variables

k_{cp}	$\alpha_{overhead}$	$\tau_{k,c,uncr}$ [psi]	d_a [in.]	h_{ef} [in.]	$c_{a,min}$ [in.]	$\tau_{k,c}$ [psi]
2	1.000	2,379	0.500	4.500	∞	1,216
$e_{c1,N}$ [in.]	$e_{c2,N}$ [in.]	c_{ac} [in.]	λ_a			
0.000	0.000	8.272	1.000			

Calculations

c_{Na} [in.]	A_{Na} [in. ²]	A_{Na0} [in. ²]	$\Psi_{ed,Na}$
7.320	385.76	214.35	1.000
$\Psi_{ec1,Na}$	$\Psi_{ec2,Na}$	$\Psi_{cp,Na}$	N_{ba} [lb]
1.000	1.000	1.000	8,599

Results

V_{cpq} [lb]	$\phi_{concrete}$	ϕV_{cpq} [lb]	V_{ua} [lb]
30,949	0.700	21,664	1,400

Input data and results must be checked for conformity with the existing conditions and for plausibility!
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5 Warnings

- The anchor design methods in PROFIS Engineering require rigid anchor plates per current regulations (AS 5216:2021, ETAG 001/Annex C, EOTA TR029 etc.). This means load re-distribution on the anchors due to elastic deformations of the anchor plate are not considered - the anchor plate is assumed to be sufficiently stiff, in order not to be deformed when subjected to the design loading. PROFIS Engineering calculates the minimum required anchor plate thickness with CBFEM to limit the stress of the anchor plate based on the assumptions explained above. The proof if the rigid anchor plate assumption is valid is not carried out by PROFIS Engineering. Input data and results must be checked for agreement with the existing conditions and for plausibility!
- Condition A applies where the potential concrete failure surfaces are crossed by supplementary reinforcement proportioned to tie the potential concrete failure prism into the structural member. Condition B applies where such supplementary reinforcement is not provided, or where pullout or pryout strength governs.
- Design Strengths of adhesive anchor systems are influenced by the cleaning method. Refer to the INSTRUCTIONS FOR USE given in the Evaluation Service Report for cleaning and installation instructions.
- For additional information about ACI 318 strength design provisions, please go to <https://submittals.us.hilti.com/PROFISAnchorDesignGuide/>
- Installation of Hilti adhesive anchor systems shall be performed by personnel trained to install Hilti adhesive anchors. Reference ACI 318-14, Section 17.8.1.

Fastening meets the design criteria!

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6 Installation data

Profile: no profile

Hole diameter in the fixture: $d_f = 0.562$ in.

Plate thickness (input): 0.500 in.

Recommended plate thickness: not calculated

Drilling method: Hammer drilled

Cleaning: Compressed air cleaning of the drilled hole according to instructions for use is required

Anchor type and diameter: HIT-HY 200 V3 + HAS-V-36

(ASTM F1554 Gr.36) 1/2

Item number: 2198022 HAS-V-36 1/2"x6-1/2" (element) / 2334276 HIT-HY 200-R V3 (adhesive)

Maximum installation torque: 360 in.lb

Hole diameter in the base material: 0.562 in.

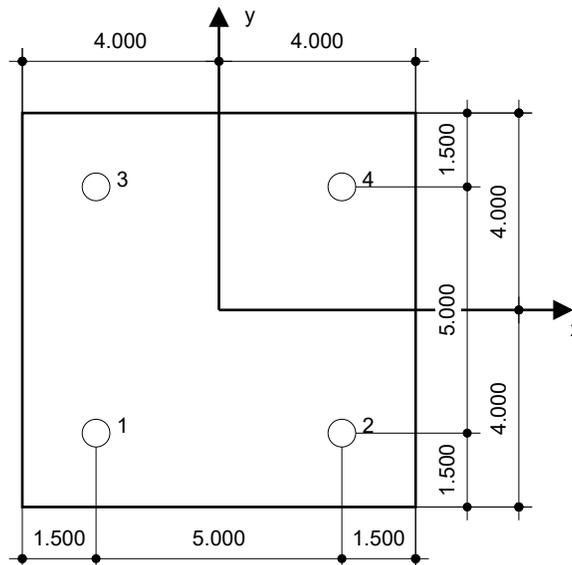
Hole depth in the base material: 4.500 in.

Minimum thickness of the base material: 5.750 in.

1/2 Hilti HAS Carbon steel threaded rod with Hilti HIT-HY 200 V3 Safe Set System

6.1 Recommended accessories

Drilling	Cleaning	Setting
<ul style="list-style-type: none"> • Suitable Rotary Hammer • Properly sized drill bit 	<ul style="list-style-type: none"> • Compressed air with required accessories to blow from the bottom of the hole • Proper diameter wire brush 	<ul style="list-style-type: none"> • Dispenser including cassette and mixer • Torque wrench



Coordinates Anchor [in.]

Anchor	x	y	C _{-x}	C _{+x}	C _{-y}	C _{+y}
1	-2.500	-2.500	-	-	-	-
2	2.500	-2.500	-	-	-	-
3	-2.500	2.500	-	-	-	-
4	2.500	2.500	-	-	-	-

Input data and results must be checked for conformity with the existing conditions and for plausibility!
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7 Remarks; Your Cooperation Duties

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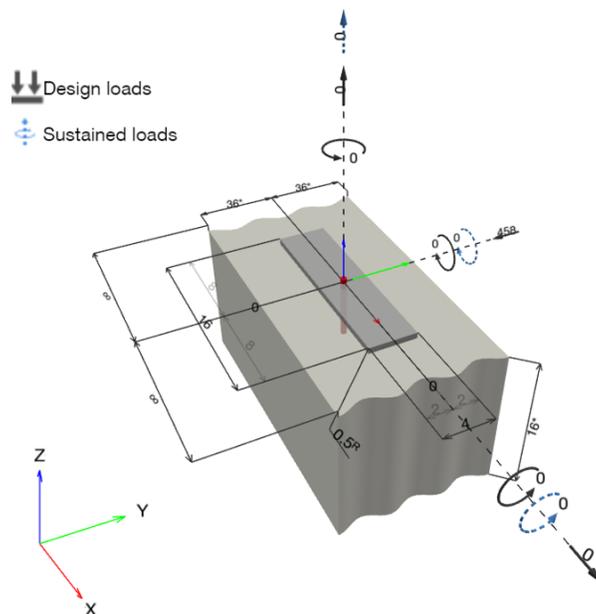
Specifier's comments:

1 Input data

Anchor type and diameter:	HIT-HY 200 V3 + HAS-V-36 (ASTM F1554 Gr.36) 1/2	
Item number:	2198022 HAS-V-36 1/2"x6-1/2" (element) / 2334276 HIT-HY 200-R V3 (adhesive)	
Effective embedment depth:	$h_{ef,act} = 4.500$ in. ($h_{ef,limit} = -$ in.)	
Material:	ASTM F1554 Grade 36	
Evaluation Service Report:	ESR-4868	
Issued Valid:	11/1/2022 11/1/2024	
Proof:	Design Method ACI 318-14 / Chem	
Stand-off installation:	$e_b = 0.000$ in. (no stand-off); $t = 0.500$ in.	
Anchor plate ^R :	$l_x \times l_y \times t = 16.000$ in. x 4.000 in. x 0.500 in.; (Recommended plate thickness: not calculated)	
Profile:	no profile	
Base material:	cracked concrete, 5000 , $f'_c = 5,000$ psi; $h = 16.000$ in., Temp. short/long: 32/32 °F	
Installation:	hammer drilled hole, Installation condition: Dry	
Reinforcement:	tension: condition B, shear: condition B; no supplemental splitting reinforcement present edge reinforcement: none or < No. 4 bar	

^R - The anchor calculation is based on a rigid anchor plate assumption.

Geometry [in.] & Loading [lb, in.lb]



Input data and results must be checked for conformity with the existing conditions and for plausibility!
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1.1 Design results

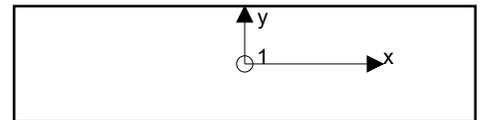
Case	Description	Forces [lb] / Moments [in.lb]	Seismic	Max. Util. Anchor [%]
1	Combination 1	N = 0; V _x = 0; V _y = -458; M _x = 0; M _y = 0; M _z = 0; N _{sus} = 0; M _{x,sus} = 0; M _{y,sus} = 0;	no	15

2 Load case/Resulting anchor forces

Anchor reactions [lb]

Tension force: (+Tension, -Compression)

Anchor	Tension force	Shear force	Shear force x	Shear force y
1	0	458	0	-458



max. concrete compressive strain: - [%]
 max. concrete compressive stress: - [psi]
 resulting tension force in (x/y)=(0.000/0.000): 0 [lb]
 resulting compression force in (x/y)=(0.000/0.000): 0 [lb]

Anchor forces are calculated based on the assumption of a rigid anchor plate.

3 Tension load

	Load N _{ua} [lb]	Capacity ϕ N _n [lb]	Utilization $\beta_N = N_{ua}/\phi N_n$	Status
Steel Strength*	N/A	N/A	N/A	N/A
Bond Strength**	N/A	N/A	N/A	N/A
Sustained Tension Load Bond Strength*	N/A	N/A	N/A	N/A
Concrete Breakout Failure**	N/A	N/A	N/A	N/A

* highest loaded anchor **anchor group (anchors in tension)



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4 Shear load

	Load V_{ua} [lb]	Capacity ϕV_n [lb]	Utilization $\beta_v = V_{ua} / \phi V_n$	Status
Steel Strength*	458	3,211	15	OK
Steel failure (with lever arm)*	N/A	N/A	N/A	N/A
Pryout Strength (Bond Strength controls)**	458	12,038	4	OK
Concrete edge failure in direction y-**	458	43,662	2	OK

* highest loaded anchor **anchor group (relevant anchors)

4.1 Steel Strength

V_{sa} = ESR value refer to ICC-ES ESR-4868
 $\phi V_{steel} \geq V_{ua}$ ACI 318-14 Table 17.3.1.1

Variables

$A_{se,V}$ [in. ²]	f_{uta} [psi]
0.14	58,000

Calculations

V_{sa} [lb]
4,940

Results

V_{sa} [lb]	ϕ_{steel}	ϕV_{sa} [lb]	V_{ua} [lb]
4,940	0.650	3,211	458



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4.2 Pryout Strength (Bond Strength controls)

$$V_{cp} = k_{cp} \left[\left(\frac{A_{Na}}{A_{Na0}} \right) \psi_{ed,Na} \psi_{cp,Na} N_{ba} \right] \quad \text{ACI 318-14 Eq. (17.5.3.1a)}$$

$$\phi V_{cp} \geq V_{ua} \quad \text{ACI 318-14 Table 17.3.1.1}$$

$$A_{Na} \text{ see ACI 318-14, Section 17.4.5.1, Fig. R 17.4.5.1(b)}$$

$$A_{Na0} = (2 c_{Na})^2 \quad \text{ACI 318-14 Eq. (17.4.5.1c)}$$

$$c_{Na} = 10 d_a \sqrt{\frac{\tau_{k,c,uncr}}{1100}} \quad \text{ACI 318-14 Eq. (17.4.5.1d)}$$

$$\psi_{ed,Na} = 0.7 + 0.3 \left(\frac{c_{a,min}}{c_{Na}} \right) \leq 1.0 \quad \text{ACI 318-14 Eq. (17.4.5.4b)}$$

$$\psi_{cp,Na} = \text{MAX} \left(\frac{c_{a,min}}{c_{ac}}, \frac{c_{Na}}{c_{ac}} \right) \leq 1.0 \quad \text{ACI 318-14 Eq. (17.4.5.5b)}$$

$$N_{ba} = \lambda_a \cdot \tau_{k,c} \cdot \pi \cdot d_a \cdot h_{ef} \quad \text{ACI 318-14 Eq. (17.4.5.2)}$$

Variables

k_{cp}	$\alpha_{overhead}$	$\tau_{k,c,uncr}$ [psi]	d_a [in.]	h_{ef} [in.]	$c_{a,min}$ [in.]	$\tau_{k,c}$ [psi]
2	1.000	2,379	0.500	4.500	36.000	1,216
c_{ac} [in.]	λ_a					
8.272	1.000					

Calculations

c_{Na} [in.]	A_{Na} [in. ²]	A_{Na0} [in. ²]	$\psi_{ed,Na}$
7.320	214.35	214.35	1.000
$\psi_{cp,Na}$	N_{ba} [lb]		
1.000	8,599		

Results

V_{cp} [lb]	$\phi_{concrete}$	ϕV_{cp} [lb]	V_{ua} [lb]
17,197	0.700	12,038	458

Input data and results must be checked for conformity with the existing conditions and for plausibility!
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4.3 Concrete edge failure in direction y-

$$V_{cb} = \left(\frac{A_{Vc}}{A_{Vc0}} \right) \Psi_{ed,V} \Psi_{c,V} \Psi_{h,V} \Psi_{parallel,V} V_b \quad \text{ACI 318-14 Eq. (17.5.2.1a)}$$

$$\phi V_{cb} \geq V_{ua} \quad \text{ACI 318-14 Table 17.3.1.1}$$

 A_{Vc} see ACI 318-14, Section 17.5.2.1, Fig. R 17.5.2.1(b)

$$A_{Vc0} = 4.5 c_{a1}^2 \quad \text{ACI 318-14 Eq. (17.5.2.1c)}$$

$$\Psi_{ed,V} = 0.7 + 0.3 \left(\frac{c_{a2}}{1.5c_{a1}} \right) \leq 1.0 \quad \text{ACI 318-14 Eq. (17.5.2.6b)}$$

$$\Psi_{h,V} = \sqrt{\frac{1.5c_{a1}}{h_a}} \geq 1.0 \quad \text{ACI 318-14 Eq. (17.5.2.8)}$$

$$V_b = \left(7 \left(\frac{l_e}{d_a} \right)^{0.2} \sqrt{d_a} \right) \lambda_a \sqrt{f'_c} c_{a1}^{1.5} \quad \text{ACI 318-14 Eq. (17.5.2.2a)}$$

Variables

c_{a1} [in.]	c_{a2} [in.]	$\Psi_{c,V}$	h_a [in.]	l_e [in.]
36.000	-	1.000	16.000	4.000
λ_a	d_a [in.]	f'_c [psi]	$\Psi_{parallel,V}$	
1.000	0.500	5,000	1.000	

Calculations

A_{Vc} [in. ²]	A_{Vc0} [in. ²]	$\Psi_{ed,V}$	$\Psi_{h,V}$	V_b [lb]
1,728.00	5,832.00	1.000	1.837	114,588

Results

V_{cb} [lb]	$\phi_{concrete}$	ϕV_{cb} [lb]	V_{ua} [lb]
62,374	0.700	43,662	458

5 Warnings

- The anchor design methods in PROFIS Engineering require rigid anchor plates per current regulations (AS 5216:2021, ETAG 001/Annex C, EOTA TR029 etc.). This means load re-distribution on the anchors due to elastic deformations of the anchor plate are not considered - the anchor plate is assumed to be sufficiently stiff, in order not to be deformed when subjected to the design loading. PROFIS Engineering calculates the minimum required anchor plate thickness with CBFEM to limit the stress of the anchor plate based on the assumptions explained above. The proof if the rigid anchor plate assumption is valid is not carried out by PROFIS Engineering. Input data and results must be checked for agreement with the existing conditions and for plausibility!
- Condition A applies where the potential concrete failure surfaces are crossed by supplementary reinforcement proportioned to tie the potential concrete failure prism into the structural member. Condition B applies where such supplementary reinforcement is not provided, or where pullout or pryout strength governs.
- Design Strengths of adhesive anchor systems are influenced by the cleaning method. Refer to the INSTRUCTIONS FOR USE given in the Evaluation Service Report for cleaning and installation instructions.
- For additional information about ACI 318 strength design provisions, please go to <https://submittals.us.hilti.com/PROFISAnchorDesignGuide/>
- Installation of Hilti adhesive anchor systems shall be performed by personnel trained to install Hilti adhesive anchors. Reference ACI 318-14, Section 17.8.1.



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Fastening meets the design criteria!

Input data and results must be checked for conformity with the existing conditions and for plausibility!
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 E-Mail:
 Date: 6/5/2023

6 Installation data

Profile: no profile

Hole diameter in the fixture: $d_f = 0.562$ in.

Plate thickness (input): 0.500 in.

Recommended plate thickness: not calculated

Drilling method: Hammer drilled

Cleaning: Compressed air cleaning of the drilled hole according to instructions for use is required

Anchor type and diameter: HIT-HY 200 V3 + HAS-V-36 (ASTM F1554 Gr.36) 1/2

Item number: 2198022 HAS-V-36 1/2"x6-1/2" (element) / 2334276 HIT-HY 200-R V3 (adhesive)

Maximum installation torque: 360 in.lb

Hole diameter in the base material: 0.562 in.

Hole depth in the base material: 4.500 in.

Minimum thickness of the base material: 5.750 in.

1/2 Hilti HAS Carbon steel threaded rod with Hilti HIT-HY 200 V3 Safe Set System

6.1 Recommended accessories

Drilling

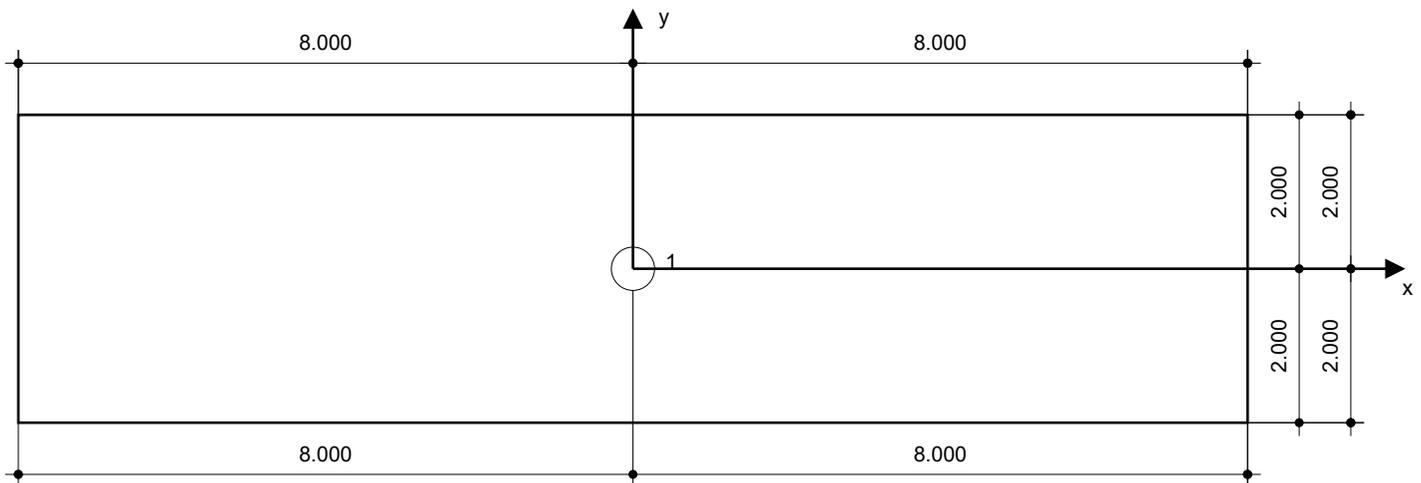
- Suitable Rotary Hammer
- Properly sized drill bit

Cleaning

- Compressed air with required accessories to blow from the bottom of the hole
- Proper diameter wire brush

Setting

- Dispenser including cassette and mixer
- Torque wrench



Coordinates Anchor [in.]

Anchor	x	y	c _{-x}	c _{+x}	c _{-y}	c _{+y}
1	0.000	0.000	-	-	36.000	36.000

Input data and results must be checked for conformity with the existing conditions and for plausibility!
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Company:		Page:	8
Address:		Specifier:	
Phone Fax:		E-Mail:	
Design:	30479 Equipment Platform Ledger Anchor	Date:	6/5/2023
Fastening point:			

7 Remarks; Your Cooperation Duties

- Any and all information and data contained in the Software concern solely the use of Hilti products and are based on the principles, formulas and security regulations in accordance with Hilti's technical directions and operating, mounting and assembly instructions, etc., that must be strictly complied with by the user. All figures contained therein are average figures, and therefore use-specific tests are to be conducted prior to using the relevant Hilti product. The results of the calculations carried out by means of the Software are based essentially on the data you put in. Therefore, you bear the sole responsibility for the absence of errors, the completeness and the relevance of the data to be put in by you. Moreover, you bear sole responsibility for having the results of the calculation checked and cleared by an expert, particularly with regard to compliance with applicable norms and permits, prior to using them for your specific facility. The Software serves only as an aid to interpret norms and permits without any guarantee as to the absence of errors, the correctness and the relevance of the results or suitability for a specific application.
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SERIES TYPE & NAME	BB HGT	BB THK	LBS./SF		LOAD/ DEFL	CLEAR SPAN																		
			19-W-4	19-W-2		12"	18"	24"	30"	36"	42"	48"	54"	60"	66"	72"	78"	84"	90"	96"	102"	108"	114"	120"
GW-75-A & GW-75-A-2	3/4"	1/8"	4.1	5.0	U	1421	631	355	227	158	116	89	70	57	47	39	34	29	25	22	20	18	16	14
					D	0.025	0.056	0.099	0.155	0.224	0.304	0.398	0.502	0.623	0.752	0.883	1.061	1.217	1.362	1.575	1.824	2.064	2.277	2.446
					C	710	474	355	284	237	203	178	158	142	129	118	109	101	95	89	84	79	75	71
					D	0.020	0.045	0.079	0.124	0.179	0.243	0.319	0.403	0.496	0.600	0.713	0.837	0.969	1.121	1.274	1.442	1.610	1.798	1.985
GW-75 & GW-75-2	3/4"	3/16"	5.8	6.7	U	2131	947	533	341	237	174	133	105	85	70	59	50	43	38	33	29	26	24	21
					D	0.025	0.056	0.099	0.155	0.224	0.304	0.397	0.502	0.619	0.746	0.891	1.040	1.203	1.401	1.575	1.764	1.987	2.277	2.446
					C	1066	710	533	426	355	304	266	237	213	194	178	164	152	142	133	125	118	112	107
					D	0.020	0.045	0.079	0.124	0.179	0.243	0.317	0.403	0.496	0.602	0.717	0.839	0.972	1.117	1.269	1.431	1.603	1.790	1.994
GW-100-A & GW-100-A-2	1"	1/8"	5.2	6.1	U	2526	1123	632	404	281	206	158	125	101	84	70	60	52	45	39	35	31	28	25
					D	0.019	0.042	0.075	0.116	0.168	0.228	0.298	0.378	0.465	0.566	0.668	0.789	0.920	1.049	1.177	1.346	1.499	1.680	1.842
					C	1263	842	632	505	421	361	316	281	253	230	211	194	180	168	158	149	140	133	126
					D	0.015	0.034	0.060	0.093	0.134	0.182	0.238	0.302	0.373	0.451	0.537	0.628	0.728	0.836	0.954	1.079	1.203	1.344	1.485
GW-100 & GW-100-2	1"	3/16"	7.5	8.4	U	3790	1684	947	606	421	309	237	187	152	125	105	90	77	67	59	52	47	42	38
					D	0.019	0.042	0.074	0.116	0.168	0.228	0.298	0.377	0.467	0.562	0.669	0.789	0.908	1.042	1.187	1.334	1.515	1.681	1.867
					C	1895	1263	947	758	632	541	474	421	379	345	316	292	271	253	237	223	211	199	189
					D	0.015	0.034	0.060	0.093	0.134	0.182	0.238	0.302	0.372	0.451	0.537	0.630	0.731	0.839	0.954	1.077	1.209	1.341	1.486
GW-125-A & GW-125-A-2	1-1/4"	1/8"	6.3	7.2	U	3947	1754	987	631	439	322	247	195	158	130	110	93	81	70	62	55	49	44	39
					D	0.015	0.034	0.060	0.093	0.134	0.182	0.239	0.302	0.373	0.449	0.538	0.626	0.734	0.836	0.958	1.083	1.213	1.352	1.472
					C	1973	1316	987	789	658	564	493	439	395	359	329	304	282	263	247	232	219	208	197
					D	0.012	0.027	0.048	0.074	0.107	0.146	0.191	0.242	0.298	0.361	0.429	0.504	0.584	0.670	0.764	0.860	0.964	1.077	1.189
GW-125 & GW-125-2	1-1/4"	3/16"	9.1	10.0	U	5921	2631	1480	947	658	483	370	292	237	196	164	140	121	105	93	82	73	66	59
					D	0.015	0.034	0.060	0.093	0.134	0.182	0.238	0.301	0.373	0.451	0.535	0.629	0.731	0.836	0.958	1.077	1.205	1.352	1.484
					C	2960	1974	1480	1184	987	846	740	658	592	538	493	455	423	395	370	348	329	312	296
					D	0.012	0.027	0.048	0.074	0.107	0.146	0.191	0.241	0.298	0.360	0.429	0.503	0.584	0.671	0.763	0.860	0.965	1.077	1.191
GW-150-A & GW-150-A-2	1-1/2"	1/8"	7.4	8.3	U	5684	2526	1421	910	632	464	355	281	227	188	158	135	116	101	89	79	70	63	57
					D	0.012	0.028	0.050	0.078	0.112	0.152	0.198	0.252	0.310	0.376	0.447	0.526	0.608	0.698	0.796	0.901	1.003	1.121	1.245
					C	2842	1895	1421	1137	947	812	711	632	568	517	474	437	406	379	355	334	316	299	284
					D	0.010	0.022	0.040	0.062	0.089	0.122	0.159	0.201	0.248	0.301	0.358	0.419	0.487	0.559	0.635	0.717	0.805	0.896	0.992
GW-150 & GW150-2	1-1/2"	3/16"	10.8	11.7	U	8526	3789	2132	1364	947	696	533	421	341	282	237	202	174	152	133	118	105	94	85
					D	0.012	0.028	0.050	0.078	0.112	0.152	0.199	0.251	0.310	0.376	0.447	0.525	0.608	0.700	0.793	0.897	1.003	1.115	1.238
					C	4263	2842	2132	1705	1421	1218	1066	947	853	775	711	656	609	568	533	502	474	449	426
					D	0.010	0.022	0.040	0.062	0.089	0.122	0.159	0.201	0.248	0.300	0.358	0.420	0.487	0.558	0.636	0.718	0.805	0.897	0.992
GW-175 & GW-175-2	1-3/4"	3/16"	12.5	13.4	U	11605	5158	2901	1857	1289	947	725	573	464	384	322	275	237	206	181	161	143	129	116
					D	0.011	0.024	0.043	0.067	0.096	0.130	0.170	0.215	0.266	0.322	0.383	0.450	0.522	0.598	0.680	0.771	0.860	0.963	1.064
					C	5803	3868	2901	2321	1934	1658	1451	1289	1161	1055	967	893	829	774	725	683	645	611	580
					D	0.009	0.019	0.034	0.053	0.077	0.104	0.136	0.172	0.213	0.257	0.306	0.360	0.417	0.479	0.545	0.615	0.690	0.768	0.851
GW-200 & GW-200-2	2"	3/16"	14.1	15.0	U	15158	6737	3790	2425	1684	1237	947	749	606	501	421	359	309	269	237	210	187	168	152
					D	0.009	0.021	0.037	0.058	0.084	0.114	0.149	0.189	0.233	0.282	0.335	0.394	0.456	0.523	0.596	0.673	0.754	0.840	0.934
					C	7579	5053	3790	3032	2526	2165	1895	1684	1516	1378	1263	1166	1083	1011	947	892	842	798	758
					D	0.007	0.017	0.030	0.047	0.067	0.091	0.119	0.151	0.186	0.225	0.268	0.315	0.365	0.419	0.476	0.538	0.603	0.672	0.745
GW-225 & GW-225-2	2-1/4"	3/16"	15.8	16.7	U	19184	8526	4796	3070	2132	1566	1199	947	767	634	533	454	392	341	300	266	237	213	192
					D	0.008	0.019	0.033	0.052	0.074	0.101	0.132	0.168	0.207	0.250	0.298	0.350	0.406	0.465	0.530	0.599	0.671	0.748	0.828
					C	9592	6395	4796	3837	3197	2741	2398	2132	1918	1744	1599	1476	1370	1279	1199	1128	1066	1010	959
					D	0.007	0.015	0.026	0.041	0.060	0.081	0.106	0.134	0.165	0.200	0.238	0.280	0.324	0.372	0.424	0.478	0.536	0.598	0.662
GW-250 & GW-250-2	2-1/2"	3/16"	17.4	18.3	U	23684	10526	5921	3790	2632	1933	1480	1170	947	783	658	561	483	421	370	328	292	262	237
					D	0.007	0.017	0.030	0.047	0.067	0.091	0.119	0.151	0.186	0.225	0.268	0.315	0.365	0.419	0.477	0.538	0.602	0.671	0.745
					C	11842	7895	5921	4737	3947	3383	2961	2632	2368	2153	1974	1822	1692	1579	1480	1393	1316	1247	1184
					D	0.006	0.013	0.024	0.037	0.054	0.073	0.095	0.121	0.149	0.180	0.215	0.252	0.292	0.335	0.381	0.430	0.483	0.538	0.596

U - Uniform Load - Lbs. per Square Foot

D - Deflection - in Inches

C - Concentrated Load - Lbs. per Square Foot of Width at Mid Span

- Span and loading values to the left of the bolded black line produce a deflection of 1/4" or less under a uniform load of 100 lbs. per square foot, allowing for safe pedestrian comfort. Span and loading values to the right of the bolded black line are applicable to other types of loads at the discretion of a licensed engineer.
- For Grating with a serrated surface (1" bearing bar height or taller), subtract 1/4" from the bearing bar height requirement and reference that loading information listed in the table. For example, a 1-1/2" x 3/16" smooth (non-serrated) bearing bar height and thickness would have the same strength and loading values as a 1-1/4" x 3/16" smooth (non-serrated) bearing bar height and thickness.
- Loading and deflection values are theoretical and based on a maximum allowable fiber stress (Fs) of 18,000 PSI, E = 29,000,000 PSI.
- Technical information provided is theoretical and for evaluation by technically skilled persons, with any use thereof to be at their independent discretion and risk. McNICHOLS shall have no responsibility or liability for results obtained or damages resulting from improper evaluation or use of Bar Grating.

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